## Irrigation: crops and water delivery

Irrigation and Drainage
CT4410

echnische Universiteit Delft




## Transforming a ditch for mines to a ditch for irrigation

- High canals
- Continuous flow
- Reservoirs
- Water measurement in NID


## The system



## Water measurement



The miners inch
Amount of water flowing through a surface of one square inch with a head of six inches.
How many liters per second??

## Controlling the canal

- What if a farmer does not needs his water?
- How to keep the constant head?






## Water requirements

- How to determine water requirements?
- How to predict water demand?



## Design problem

What cropping pattern do you take?
How correct is the ET calculation?
How correct is the ET and rainfall for the entire area?
How would you take into account "real" soil processes?

## In other words: how to take into account heterogeneity?

Lankford (2004) discusses this.
How to use remotely sensed ET in DESIGN ??


| Growth stage | Length | Crop <br> coefficient | Root depth |
| :---: | :---: | :---: | :---: |
|  | Days |  | Meter |
| Initial | 90 | 0.5 | 2 |
| Development | 90 |  | $\gg$ |
| Mid | 90 | 1.2 | 2 |
| Late | 95 | 0.8 | 2 |
|  | 365 |  |  |



## Crop water requirement calculation: example



Climate

|  | Rain | ETo |
| :---: | :---: | :---: |
|  | $\mathrm{mm} /$ stage | $\mathrm{mm} /$ day |
| Initial | 90 | 5 |
| Development | 65 | 6 |
| Mid | 40 | 7 |
| Late | 80 | 5 |

## Remarks:

Assuming all rain is effective
Simplifying development stage
Significant numbers??


CRW

|  | Rain | Eto | kc | Etg | Etn |
| :---: | ---: | :---: | ---: | ---: | ---: |
| Initial | 1.00 | 5 | 0.5 | 2.5 | $\mathbf{1 . 5 0}$ |
| Development | 0.72 | 6 | 0.85 | 5.1 | $\mathbf{4 . 3 8}$ |
| Mid | 0.44 | 7 | 1.2 | 8.4 | $\mathbf{7 . 9 6}$ |
| Late | 0.84 | 5 | 0.8 | 4 | $\mathbf{3 . 1 6}$ |

## How to distribute that?

Flow for a farm of one hectare

|  | $\mathrm{mm} / \mathrm{day}$ | $\mathrm{m} 3 / \mathrm{s}$ | $\mathrm{I} / \mathrm{s}$ |
| :--- | :---: | :---: | :---: |
| Continuous | 8 | 0.0009259 | 1 |
| Continuous during day | 8 | 0.0018519 | 2 |
| Every week for 10 hours | 8 | 0.0155556 | 16 |
| Every week for 1 hour | 8 | 0.1555556 | 156 |
| Every month for 1 hour | 8 | 0.6666667 | 667 |

1. Suppose I have 10 farms, how much should my canal carry?
2. Suppose I have $1200 \mathrm{l} / \mathrm{s}$, how many farms can irrigate at the same time?
3. In case 2 , how large would my surface area per canal become?

## Your assignment

1. Calculate total water demand for a 1000 hectare area in the NID over a year.
2. Describe how this water would be supplied within the NID water delivery philosophy.
3. Calculate required canal flows at the intake for this 1000 hectare area.
4. Design the canal and outlets for this area, assuming that 20 farmers with each 50 hectares take water. Assume the canal being 10 kilometers long, with farm intakes evenly spread on one side.

## Example information trees

| Growth stage | Length | Crop coefficient | Root depth |
| :---: | :---: | :---: | :---: |
|  | Days |  | Meter |
| Initial | 140 | 0.9 | 2 |
| Development | 30 |  | $\gg$ |
| Mid | 150 | 0.95 | 2 |
| Late | 45 | 0.9 | 2 |
|  | 365 |  |  |




## First, a little warning: physical reality



- Crop : COTTON
- Planting date : 1/10
- Calculation time step $=10$ Day(s)
- Irrigation Efficiency $=100 \%$
- Initial condition $=0 \%$ depletion

| Date | ETO <br> (mm/period) | Planted Area (\%) | $\begin{gathered} \text { Crop } \\ \text { Kc } \end{gathered}$ | CWR <br> (ETm) | Total Rain -- (mm/ | Effect. Rain eriod) | Irr. Req. | FWS (1/s/ha) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/10 | 50.76 | 100.00 | 0.35 | 17.77 | 12.17 | 11.87 | 5.90 | 0.07 |
| 11/10 | 51.83 | 100.00 | 0.35 | 18.14 | 13.82 | 13.24 | 4.90 | 0.06 |
| 21/10 | 52.63 | 100.00 | 0.35 | 18.42 | 17.10 | 15.75 | 2.67 | 0.03 |
| 31/10 | 53.11 | 100.00 | 0.44 | 23.56 | 21.59 | 19.12 | 4.44 | 0.05 |
| 10/11 | 53.24 | 100.00 | 0.61 | 32.66 | 26.63 | 22.83 | 9.84 | 0.11 |
| 20/11 | 53.01 | 100.00 | 0.78 | 41.52 | 31.49 | 26.35 | 15.18 | 0.18 |
| 30/11 | 52.41 | 100.00 | 0.95 | 49.97 | 35.52 | 29.22 | 20.75 | 0.24 |
| 10/12 | 51.49 | 100.00 | 1.12 | 57.84 | 38.32 | 31.16 | 26.68 | 0.31 |
| 20/12 | 50.29 | 100.00 | 1.20 | 60.35 | 39.75 | 32.07 | 28.28 | 0.33 |
| 30/12 | 48.54 | 100.00 | 1.20 | 58.24 | 39.84 | 32.07 | 26.17 | 0.30 |
| 9/1 | 48.03 | 100.00 | 1.20 | 57.63 | 39.86 | 32.26 | 25.38 | 0.29 |
| 19/1 | 47.50 | 100.00 | 1.20 | 57.00 | 39.51 | 32.19 | 24.81 | 0.29 |
| 29/1 | 46.75 | 100.00 | 1.20 | 56.10 | 38.52 | 31.64 | 24.46 | 0.28 |
| 8/2 | 45.80 | 100.00 | 1.20 | 54.96 | 36.75 | 30.49 | 24.47 | 0.28 |
| 18/2 | 44.70 | 100.00 | 1.14 | 50.97 | 34.22 | 28.73 | 22.24 | 0.26 |
| 28/2 | 43.48 | 100.00 | 1.03 | 44.84 | 31.01 | 26.41 | 18.43 | 0.21 |
| 10/3 | 42.21 | 100.00 | 0.92 | 38.93 | 27.33 | 23.68 | 15.25 | 0.18 |
| 20/3 | 40.94 | 100.00 | 0.81 | 33.28 | 23.45 | 20.72 | 12.56 | 0.15 |
| 30/3 | 39.71 | 100.00 | 0.70 | 27.95 | 19.68 | 17.79 | 10.16 | 0.12 |
| 9/4 | 19.42 | 100.00 | 0.62 | 12.08 | 8.55 | 7.86 | 4.22 | 0.10 |
| Total | 935.86 |  |  | 812.21 | 575.13 | 485.43 | 326.78 | [0.19] |

- Crop
: COTTON
- Planting date 1/10
- Calculation time step $=10$ Day(s)
- Irrigation Efficiency
- Initial condition $=100 \%$ depletion

| Date | ETo <br> (mm/period) | Planted Area (\%) | Crop Kc | $\begin{aligned} & \text { CWR } \\ & \text { (ETm) } \end{aligned}$ | Total Rain - (mm/ | Effect. Rain eriod) | Irr. Req. | FWS $(1 / s / h a)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/10 | 50.76 | 100.00 | 0.35 | 17.77 | 12.17 | 11.87 | 5.90 | 0.07 |
| 11/10 | 51.83 | 100.00 | 0.35 | 18.14 | 13.82 | 13.24 | 4.90 | 0.06 |
| 21/10 | 52.63 | 100.00 | 0.35 | 18.42 | 17.10 | 15.75 | 2.67 | 0.03 |
| 31/10 | 53.11 | 100.00 | 0.44 | 23.56 | 21.59 | 19.12 | 4.44 | 0.05 |
| 10/11 | 53.24 | 100.00 | 0.61 | 32.66 | 26.63 | 22.83 | 9.84 | 0.11 |
| 20/11 | 53.01 | 100.00 | 0.78 | 41.52 | 31.49 | 26.35 | 15.18 | 0.18 |
| 30/11 | 52.41 | 100.00 | 0.95 | 49.97 | 35.52 | 29.22 | 20.75 | 0.24 |
| 10/12 | 51.49 | 100.00 | 1.12 | 57.84 | 38.32 | 31.16 | 26.68 | 0.31 |
| 20/12 | 50.29 | 100.00 | 1.20 | 60.35 | 39.75 | 32.07 | 28.28 | 0.33 |
| 30/12 | 48.54 | 100.00 | 1.20 | 58.24 | 39.84 | 32.07 | 26.17 | 0.30 |
| 9/1 | 48.03 | 100.00 | 1.20 | 57.63 | 39.86 | 32.26 | 25.38 | 0.29 |
| 19/1 | 47.50 | 100.00 | 1.20 | 57.00 | 39.51 | 32.19 | 24.81 | 0.29 |
| 29/1 | 46.75 | 100.00 | 1.20 | 56.10 | 38.52 | 31.64 | 24.46 | 0.28 |
| 8/2 | 45.80 | 100.00 | 1.20 | 54.96 | 36.75 | 30.49 | 24.47 | 0.28 |
| 18/2 | 44.70 | 100.00 | 1.14 | 50.97 | 34.22 | 28.73 | 22.24 | 0.26 |
| 28/2 | 43.48 | 100.00 | 1.03 | 44.84 | 31.01 | 26.41 | 18.43 | 0.21 |
| 10/3 | 42.21 | 100.00 | 0.92 | 38.93 | 27.33 | 23.68 | 15.25 | 0.18 |
| 20/3 | 40.94 | 100.00 | 0.81 | 33.28 | 23.45 | 20.72 | 12.56 | 0.15 |
| 30/3 | 39.71 | 100.00 | 0.70 | 27.95 | 19.68 | 17.79 | 10.16 | 0.12 |
| 9/4 | 19.42 | 100.00 | 0.62 | 12.08 | 8.55 | 7.86 | 4.22 | 0.10 |
| Total | 935.86 |  |  | 812.21 | 575.13 | 485.43 | 326.78 | [0.19] |

- Planting date: $1 / 10$

Soil description : Medium
Initial soll molsture depletion: 0 \%

- Application Timing:

Irrigate when $100 \%$ of readily soil moisture depletion occurs

- Applications Depths:

Refill to $100 \%$ of readily available soil moisture.

- Start of Scheduling: 1/10

| Date | TAM (mm) | $\begin{aligned} & \text { RAM } \\ & (\mathrm{mm}) \end{aligned}$ | Total Rain (mm) | Efct. Rain <br> (mm) | ETC <br> (mm) | ETc/ETm <br> (\%) | SMD <br> (mm) | Interv. (Days) | Net <br> Irr. <br> (mm) | $\begin{aligned} & \text { Lost } \\ & \text { Irr. } \\ & (\mathrm{mm}) \end{aligned}$ | User Adj. (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5/10 | 49.7 | 29.8 | 6.1 | 6.1 | 1.8 | 100.0\% | 2.7 |  |  |  |  |
| 10/10 | 59.3 | 35.6 | 6.5 | 6.5 | 1.8 | 100.0\% | 5.1 |  |  |  |  |
| 15/10 | 69.0 | 41.4 | 7.1 | 7.1 | 1.8 | 100.0\% | 7.1 |  |  |  |  |
| 20/10 | 78.6 | 47.1 | 7.9 | 7.9 | 1.8 | 100.0\% | 8.3 |  |  |  |  |
| 25/10 | 88.2 | 52.9 | 8.8 | 8.8 | 1.8 | 100.0\% | 8.7 |  |  |  |  |
| 30/10 | 97.8 | 58.7 | 9.9 | 9.9 | 1.9 | 100.0\% | 8.0 |  |  |  |  |
| 4/11 | 107.4 | 64.5 | 11.2 | 11.2 | 2.3 | 100.0\% | 7.4 |  |  |  |  |
| 9/11 | 117.1 | 70.2 | 12.4 | 12.4 | 2.8 | 100.0\% | 7.9 |  |  |  |  |
| 14/11 | 126.7 | 76.0 | 13.7 | 13.7 | 3.2 | 100.0\% | 9.4 |  |  |  |  |
| 19/11 | 136.3 | 81.8 | 14.9 | 14.9 | 3.7 | 100.0\% | 12.0 |  |  |  |  |
| 24/11 | 145.9 | 87.6 | 16.1 | 16.1 | 4.1 | 100.0\% | 15.5 |  |  |  |  |
| 29/11 | 155.6 | 93.3 | 17.1 | 17.1 | 4.5 | 100.0\% | 20.3 |  |  |  |  |
| 4/12 | 165.2 | 99.1 | 18.0 | 18.0 | 5.0 | 100.0\% | 26.2 |  |  |  |  |
| 9/12 | 174.8 | 104.9 | 18.8 | 18.8 | 5.4 | 100.0\% | 33.4 |  |  |  |  |
| 14/12 | 184.4 | 110.7 | 19.3 | 19.3 | 5.7 | 100.0\% | 42.1 |  |  |  |  |
| 19/12 | 194.1 | 116.4 | 19.7 | 19.7 | 6.1 | 100.0\% | 52.2 |  |  |  |  |
| 24/12 | 196.0 | 117.6 | 19.9 | 19.9 | 6.0 | 100.0\% | 62.6 |  |  |  |  |
| 29/12 | 196.0 | 117.6 | 12.0 | 12.0 | 6.0 | 100.0\% | 80.6 |  |  |  |  |
| 1/1 | 196.0 | 117.6 | 19.9 | 19.9 | 5.8 | 100.0\% | 78.4 |  |  |  |  |
| 6/1 | 196.0 | 117.6 | 19.9 | 19.9 | 5.8 | 100.0\% | 87.5 |  |  |  |  |
| 11/1 | 196.0 | 117.6 | 19.9 | 19.9 | 5.8 | 100.0\% | 96.4 |  |  |  |  |
| 15/1 | 196.0 | 117.6 | 0.0 | 0.0 | 5.8 | 100.0\% | 119.5 | 106 | 119.5 | 0.0 |  |
| 16/1 | 196.0 | 117.6 | 19.9 | 0.0 | 5.8 | 100.0\% | 5.8 |  |  |  |  |
| 21/1 | 196.0 | 117.6 | 19.8 | 19.8 | 5.7 | 100.0\% | 14.6 |  |  |  |  |
| 26/1 | 196.0 | 117.6 | 19.6 | 19.6 | 5.7 | 100.0\% | 23.5 |  |  |  |  |
| 31/1 | 196.0 | 117.6 | 19.3 | 19.3 | 5.6 | 100.0\% | 32.5 |  |  |  |  |
| 5/2 | 196.0 | 117.6 | 18.9 | 18.9 | 5.6 | 100.0\% | 41.6 |  |  |  |  |
| 10/2 | 196.0 | 117.6 | 18.4 | 18.4 | 5.5 | 100.0\% | 50.9 |  |  |  |  |
| 15/2 | 196.0 | 117.6 | 17.9 | 17.9 | 5.5 | 100.0\% | 60.5 |  |  |  |  |
| 20/2 | 196.0 | 120.8 | 17.2 | 17.2 | 5.3 | 100.0\% | 70.1 |  |  |  |  |
| 25/2 | 196.0 | 126.2 | 16.4 | 16.4 | 4.9 | 100.0\% | 79.0 |  |  |  |  |
| 2/3 | 196.0 | 131.5 | 15.6 | 15.6 | 4.6 | 100.0\% | 87.2 |  |  |  |  |
| 7/3 | 196.0 | 136.8 | 14.7 | 14.7 | 4.3 | 100.0\% | 94.8 |  |  |  |  |
| 12/3 | 196.0 | 142.2 | 13.8 | 13.8 | 4.0 | 100.0\% | 101.8 |  |  |  |  |
| 17/3 | 196.0 | 147.5 | 12.8 | 12.8 | 3.7 | 100.0\% | 108.3 |  |  |  |  |
| 22/3 | 196.0 | 152.9 | 11.8 | 11.8 | 3.5 | 100.0\% | 114.4 |  |  |  |  |
| 27/3 | 196.0 | 158.2 | 10.9 | 10.9 | 3.2 | 100.0\% | 120.0 |  |  |  |  |
| 1/4 | 196.0 | 163.6 | 9.9 | 9.9 | 2.9 | 100.0\% | 125.2 |  |  |  |  |
| 6/4 | 196.0 | 168.9 | 9.0 | 9.0 | 2.7 | 100.0\% | 130.0 |  |  |  |  |
| 11/4 | 196.0 | 174.3 | 8.2 | 8.2 | 2.4 | 100.0\% | 134.4 |  |  |  |  |
| Total |  |  | 573.5 | 553.7 | 812.2 | 100.0\% |  |  | 119.5 | 0.0 | 0.0 |

Planting date: $1 / 10$

- Initial soil moisture depleti
- Application Timing:

Irrigate when $100 \%$ of readily soll moisture depletion occurs.

- Applications Depths:

Refill to $100 \%$ of readily available soil moisture.

- Start of Scheduling: 1/10

| Date | $\begin{aligned} & \text { TAM } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{aligned} & \text { RAM } \\ & (\mathrm{mm}) \end{aligned}$ | Total Rain (mm) | Efct. Rain (mm) | ETc <br> (mm) | ETc/ETm <br> (\%) | $\begin{aligned} & \text { SMD } \\ & (\mathrm{mm}) \end{aligned}$ | Interv. Net Lost  <br> (Days) Irr. Irr. <br>  (mm)  | User Adj. (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/10 | 42.0 | 25.2 | 0.0 | 0.0 | 0.0 | 0.0\% | 42.0 | 042. |  |
| 5/10 | 49.7 | 29.8 | 6.1 | 5.3 | 1.8 | 100.0\% | 1.8 |  |  |
| 10/10 | 59.3 | 35.6 | 6.5 | 6.5 | 1.8 | 100.0\% | 4.2 |  |  |
| 15/10 | 69.0 | 41.4 | 7.1 | 7.1 | 1.8 | 100.0\% | 6.2 |  |  |
| 20/10 | 78.6 | 47.1 | 7.9 | 7.9 | 1.8 | 100.0\% | 7.4 |  |  |
| 25/10 | 88.2 | 52.9 | 8.8 | 8.8 | 1.8 | 100.0\% | 7.7 |  |  |
| 30/10 | 97.8 | 58.7 | 9.9 | 9.9 | 1.9 | 100.0\% | 7.0 |  |  |
| 4/11 | 107.4 | 64.5 | 11.2 | 11.2 | 2.3 | 100.0\% | 6.5 |  |  |
| 9/11 | 117.1 | 70.2 | 12.4 | 12.4 | 2.8 | 100.0\% | 7.0 |  |  |
| 14/11 | 126.7 | 76.0 | 13.7 | 13.7 | 3.2 | 100.0\% | 8.5 |  |  |
| 19/11 | 136.3 | 81.8 | 14.9 | 14.9 | 3.7 | 100.0\% | 11.0 |  |  |
| 24/11 | 145.9 | 87.6 | 16.1 | 16.1 | 4.1 | 100.0\% | 14.6 |  |  |
| 29/11 | 155.6 | 93.3 | 17.1 | 17.1 | 4.5 | 100.0\% | 19.3 |  |  |
| 4/12 | 165.2 | 99.1 | 18.0 | 18.0 | 5.0 | 100.0\% | 25.3 |  |  |
| 9/12 | 174.8 | 104.9 | 18.8 | 18.8 | 5.4 | 100.0\% | 32.5 |  |  |
| 14/12 | 184.4 | 110.7 | 19.3 | 19.3 | 5.7 | 100.0\% | 41.1 |  |  |
| 19/12 | 194.1 | 116.4 | 19.7 | 19.7 | 6.1 | 100.0\% | 51.3 |  |  |
| 24/12 | 196.0 | 117.6 | 19.9 | 19.9 | 6.0 | 100.0\% | 61.7 |  |  |
| 29/12 | 196.0 | 117.6 | 12.0 | 12.0 | 6.0 | 100.0\% | 79.7 |  |  |
| 1/1 | 196.0 | 117.6 | 19.9 | 19.9 | 5.8 | 100.0\% | 77.5 |  |  |
| 6/1 | 196.0 | 117.6 | 19.9 | 19.9 | 5.8 | 100.0\% | 86.5 |  |  |
| 11/1 | 196.0 | 117.6 | 19.9 | 19.9 | 5.8 | 100.0\% | 95.5 | , |  |
| 15/1 | 196.0 | 117.6 | 0.0 | 0.0 | 5.8 | 100.0\% | 118.6 | 106118.6 0.0 |  |
| 16/1 | 196.0 | 117.6 | 19.9 | 0.0 | 5.8 | 100.0\% | 5.8 | ( 118.6 |  |
| 21/1 | 196.0 | 117.6 | 19.8 | 19.8 | 5.7 | 100.0\% | 14.6 |  |  |
| 26/1 | 196.0 | 117.6 | 19.6 | 19.6 | 5.7 | 100.0\% | 23.5 |  |  |
| 31/1 | 196.0 | 117.6 | 19.3 | 19.3 | 5.6 | 100.0\% | 32.5 |  |  |
| 5/2 | 196.0 | 117.6 | 18.9 | 18.9 | 5.6 | 100.0\% | 41.6 |  |  |
| 10/2 | 196.0 | 117.6 | 18.4 | 18.4 | 5.5 | 100.0\% | 50.9 |  |  |
| 15/2 | 196.0 | 117.6 | 17.9 | 17.9 | 5.5 | 100.0\% | 60.5 |  |  |
| 20/2 | 196.0 | 120.8 | 17.2 | 17.2 | 5.3 | 100.0\% | 70.1 |  |  |
| 25/2 | 196.0 | 126.2 | 16.4 | 16.4 | 4.9 | 100.0\% | 79.0 |  |  |
| 2/3 | 196.0 | 131.5 | 15.6 | 15.6 | 4.6 | 100.0\% | 87.2 |  |  |
| 7/3 | 196.0 | 136.8 | 14.7 | 14.7 | 4.3 | 100.0\% | 94.8 |  |  |
| 12/3 | 196.0 | 142.2 | 13.8 | 13.8 | 4.0 | 100.0\% | 101.8 |  |  |
| 17/3 | 196.0 | 147.5 | 12.8 | 12.8 | 3.7 | 100.0\% | 108.3 |  |  |
| 22/3 | 196.0 | 152.9 | 11.8 | 11.8 | 3.5 | 100.0\% | 114.4 |  |  |
| 27/3 | 196.0 | 158.2 | 10.9 | 10.9 | 3.2 | 100.0\% | 120.0 |  |  |
| 1/4 | 196.0 | 163.6 | 9.9 | 9.9 | 2.9 | 100.0\% | 125.2 |  |  |
| 6/4 | 196.0 | 168.9 | 9.0 | 9.0 | 2.7 | 100.0\% | 130.0 |  |  |
| 11/4 | 196.0 | 174.3 | 8.2 | 8.2 | 2.4 | 100.0\% | 134.4 |  |  |
| Total |  |  | 573.5 | 552.8 | 810.4 | 99.8\% |  | $160.6 \quad 0.0$ | 0.0 |

## What did I do? Water requirements



## Water need in I/s and miners inches/farm



## So why start per April 1??

- What if a farmer is an early vegetable grower?
- What if it does not rain in April?
- What if ... ?


## And the canal?

I know I will have fluctuating flows and that there is a need to maintain the same water level. So, one uniform flow calculation will not suffice. And I probably need some kind of water level control, and perhaps some spills.

## Canal calculation

Not that straightforward designing a fitting canal and structures

| canal | AB |
| :--- | ---: |
| $\mathbf{L}$ | 10000 |
| $\mathbf{H}$ control | 0.64 |
| $\mathbf{y}$ | 0.64 |
| $\mathbf{A}$ | 2.97 |
| $\mathbf{Q}$ | 0.66 |
| $\mathbf{m}$ | 1 |
| $\mathbf{v}$ | 0.22 |
| $\mathbf{R}$ | 0.51 |
| $\mathbf{s}$ | 35 |
| $\mathbf{k}$ | 4 |
| $\mathbf{b}$ | 6.0001 |
| $\mathbf{n}$ |  |

## Q increases:

| canal | AB |
| :--- | ---: |
| $\mathbf{L}$ | 10000 |
| H control | 0.71 |
| $\mathbf{y}$ | 0.71 |
| A | 3.34 |
| Q | 0.8 |
| $\mathbf{m}$ | 1 |
| $\mathbf{v}$ | 0.24 |
| $\mathbf{R}$ | 0.56 |
| $\mathbf{s}$ | 0.0001 |
| $\mathbf{k}$ | 35 |
| $\mathbf{b}$ | 4 |
| $\mathbf{n}$ | 5.6 |

Q decreases:

| canal | $A B$ |
| :--- | ---: |
| L | 10000 |
| $\mathbf{H}$ control | 0.47 |
| $\mathbf{y}$ | 0.47 |
| $\mathbf{A}$ | 2.10 |
| $\mathbf{Q}$ | 0.4 |
| $\mathbf{m}$ | 1 |
| $\mathbf{v}$ | 0.19 |
| $\mathbf{R}$ | 0.39 |
| $\mathbf{s}$ | 0.0001 |
| $\mathbf{k}$ | 35 |
| $\mathbf{b}$ | 4 |
| $\mathbf{n}$ | 8.5 |

## Canal calculation

## So probably we need water leı

Weirs?



## And what if I have farmers with only fuit and vegetables????



## What did I do?

Design discharge of $1 \mathrm{~m} 3 / \mathrm{s}$
Water depth of 1 meter, bed width of 2 meters
Slope of 1 in 10000
Side slope of 1
Roughness of about 45 (Strickler)


Animation time:
02Jan-1951 16:00:00


