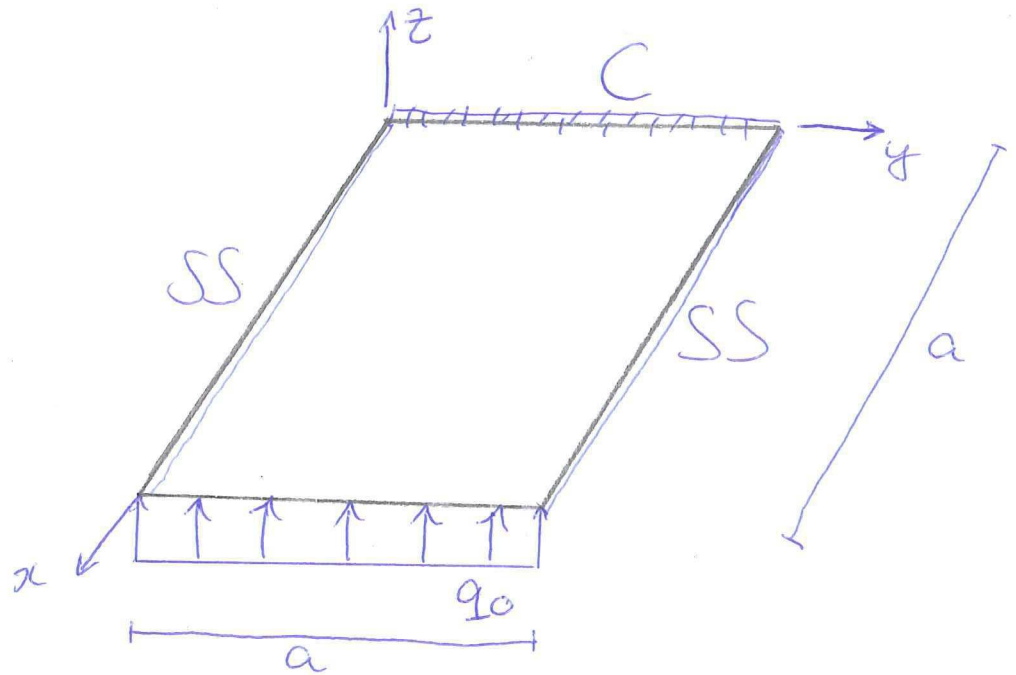


Take Home Exam

Problem 1



1a) We have: $w = \sum_n \psi_n(x) \sin \frac{n\pi y}{a} = \sum_n \psi_n(x) \sin \alpha y$ (1)
 with $\alpha = \frac{n\pi}{a}$

$$\Pi = U + V$$

with: $U = \iint_{00}^{aa} \frac{D}{2} [w_{,xx}^2 + w_{,yy}^2 + 2\nu w_{,xx} w_{,yy} + 2(1-\nu)w_{,xy}^2] dx dy$ (2)

$$V = - \iint_{00}^{aa} q(x,y) w dx dy$$
 (3)

From $w_n = \psi_n(x) \sin \alpha y$:

$$w_{n,xx} = \psi_n'' \sin \alpha y$$

$$w_{n,yy} = -\psi_n \alpha^2 \sin \alpha y$$

$$w_{n,xy} = \psi_n' \alpha \cos \alpha y$$

$$w_{n,xx}^2 = \psi_n''^2 \sin^2 \alpha y$$

$$w_{n,yy}^2 = \psi_n^2 \alpha^4 \sin^2 \alpha y$$

$$w_{n,xy}^2 = \psi_n'^2 \alpha^2 \cos^2 \alpha y$$

$$w_{n,xx} w_{n,yy} = -\psi_n \psi_n'' \alpha^2 \sin^2 \alpha y$$

(4)

Now use:

$$\int_0^a \sin^2 \alpha y \, dy = \int_0^a \cos^2 \alpha y \, dy = \frac{a}{2} \quad (5)$$

$$\int_0^a \sin \frac{n\pi y}{a} \sin \frac{m\pi y}{a} \, dy = \int_0^a \cos \frac{n\pi y}{a} \cos \frac{m\pi y}{a} \, dy = 0 \quad \text{for } m \neq n$$

Hence: $U = \sum_n U_n$, with (using (2,4,5))

$$U_n = \frac{Da}{4} \int_0^a \left(\psi_n''^2 + \psi_n^2 \alpha^4 - 2\nu \psi_n \psi_n'' \alpha^2 + 2(1-\nu) \psi_n' \alpha^2 \right) dx$$

Also for $V = \sum_n V_n$ with

$$V_n = - \int_0^a \int_0^a q(x,y) w_n \, dx \, dy, \quad \text{with } q(x,y) = q_0 \delta(x-a)$$

$$= - \int_0^a q_0 \delta(x-a) \psi_n(x) \, dx \int_0^a \sin \alpha y \, dy$$

$$= - q_0 \psi_n(a) \cdot \frac{1}{\alpha} [1 - (-1)^n]$$

$$= \begin{cases} - \frac{2q_0 \psi_n(a)}{\alpha} & \text{for } n \text{ odd} \\ 0 & \text{otherwise} \end{cases}$$

So $\pi = U + V = \sum_n U_n + V_n = \sum_n \pi_n$, with

$$\pi_n = U_n + V_n \quad (6)$$

$$= \frac{Da}{4} \int_0^a \left(\psi_n''^2 + \psi_n^2 \alpha^4 - 2\nu \psi_n \psi_n'' \alpha^2 + 2(1-\nu) \psi_n' \alpha^2 \right) dx + - \frac{2q_0}{\alpha} \psi_n(a)$$

$$1) b) \delta \Pi = 0 \Rightarrow \delta \Pi_n = 0 \quad \text{for all } n = 1, 3, 5, \dots$$

From (b) and using $\delta \varphi_n''^2 = 2 \varphi_n'' \delta \varphi_n''$, etc.:

$$\begin{aligned} \delta \Pi_n &= \frac{Dca}{u} \int_0^a \left(2 \varphi_n'' \delta \varphi_n'' + 2 \alpha^4 \varphi_n \delta \varphi_n - 2 \nu \alpha \left(\varphi_n \delta \varphi_n'' + \varphi_n'' \delta \varphi_n \right) \right. \\ &\quad \left. + 2(1-\nu) \alpha^2 \cdot 2 \varphi_n' \delta \varphi_n' \right) dx - \frac{2q_0}{d} \delta \varphi_n(a) \\ &= \frac{Dca}{2} \int_0^a \left[\underbrace{\left(\alpha^4 \varphi_n - \nu \alpha^2 \varphi_n'' \right) \delta \varphi_n}_{\text{I}} + \underbrace{\left(\varphi_n'' - \nu \alpha^2 \varphi_n \right) \delta \varphi_n''}_{\text{II}} + 2(1-\nu) \alpha^2 \varphi_n' \delta \varphi_n' \right] dx \\ &\quad - \underbrace{\frac{2q_0}{d} \delta \varphi_n(a)}_{\text{B.T.}} \end{aligned}$$

Use integration by parts: (use $\delta \varphi_n(0) = \delta \varphi_n'(0) = 0$)

$$\begin{aligned} \text{I: } \int_0^a \left(\varphi_n'' - \nu \alpha^2 \varphi_n \right) \delta \varphi_n' dx &= \left[\left(\varphi_n'' - \nu \alpha^2 \varphi_n \right) \delta \varphi_n' \right]_0^a - \int_0^a \left(\varphi_n''' - \nu \alpha^2 \varphi_n' \right) \delta \varphi_n dx \\ &= \left[\left(\varphi_n'' - \nu \alpha^2 \varphi_n \right) \delta \varphi_n' \right]_{x=a} - \left[\left(\varphi_n''' - \nu \alpha^2 \varphi_n' \right) \delta \varphi_n \right]_0^a + \int_0^a \left(\varphi_n'''' - \nu \alpha^2 \varphi_n'' \right) \delta \varphi_n dx \\ &= \underbrace{\left[\left(\varphi_n'' - \nu \alpha^2 \varphi_n \right) \delta \varphi_n' - \left(\varphi_n''' - \nu \alpha^2 \varphi_n' \right) \delta \varphi_n \right]_{x=a}}_{\text{B.T. (Boundary Terms)}} + \int_0^a \left(\varphi_n'''' - \nu \alpha^2 \varphi_n'' \right) \delta \varphi_n dx \end{aligned}$$

$$\begin{aligned} \text{II: } \int_0^a 2(1-\nu) \alpha^2 \varphi_n' \delta \varphi_n' &= \left[2(1-\nu) \alpha^2 \varphi_n' \delta \varphi_n \right]_0^a - \int_0^a 2(1-\nu) \alpha^2 \varphi_n'' \delta \varphi_n dx \\ &= \underbrace{\left[2(1-\nu) \alpha^2 \varphi_n' \delta \varphi_n \right]_{x=a}}_{\text{B.T.}} - \int_0^a 2(1-\nu) \alpha^2 \varphi_n'' \delta \varphi_n dx \end{aligned}$$

Collecting results from integration by parts and substituting these into $\delta\pi_n$:

$$\delta\pi_n = \frac{Da}{2} \int_0^a (d^4\varphi_n - 2d^2\varphi_n'' + \varphi_n'''' - \nu d^2\varphi_n'' - 2(1-\nu)d^2\varphi_n'') \delta\varphi_n dx + B.T.$$

$$= \frac{Da}{2} \int_0^a (d^4\varphi_n - 2d^2\varphi_n'' + \varphi_n''') \delta\varphi_n dx + B.T.$$

$$\Rightarrow \text{So: } \delta\pi = 0 \Rightarrow \boxed{\varphi_n'''' - 2d^2\varphi_n'' + d^4\varphi_n = 0} \quad (7)$$

Boundary conditions:

We already used the essential B.C.

$$\varphi_n(0) = 0 \quad (\text{BC 1})$$

$$\varphi_n'(0) = 0 \quad (\text{BC 2})$$

The remaining two B.C. are derived from the B.T. in the expression of $\delta\pi_n$

$$B.T. = \frac{Da}{2} \left[(\varphi_n'' - \nu d^2\varphi_n) \delta\varphi_n' + (-\varphi_n'''' + \nu d^2\varphi_n'' + 2(1-\nu)d^2\varphi_n') \delta\varphi_n \right]_{x=a}$$

$$- \frac{2q_0}{\alpha} \delta\varphi_n(a)$$

$$= \frac{Da}{2} \left[(\varphi_n'' - \nu d^2\varphi_n) \delta\varphi_n' + \left(\varphi_n'''' - (2-\nu)d^2\varphi_n'' + \frac{4q_0}{Da\alpha} \right) \delta\varphi_n \right]_{x=a}$$

So, from $\delta\pi_n = 0$ we get:

$$\psi_n''(a) - \nu \alpha^2 \psi_n(a) = 0 \quad (\text{BC3})$$

$$\psi_n'''(a) - (2-\nu) \alpha^2 \psi_n'(a) = -\frac{4q_0}{D\alpha a} = -\frac{4q_0}{Dn\pi} \quad \text{for } n \text{ odd} \quad (\text{BC4})$$

1c) Assume $\psi_n = C_n e^{\lambda_n x} \Rightarrow \psi_n' = C_n \lambda_n e^{\lambda_n x}, \psi_n'' = \dots$ etc

Into (7):

$$(\lambda_n^4 - 2\alpha^2 \lambda_n^2 + \alpha^4) C_n e^{\lambda_n x} = 0$$

$$(\lambda_n^2 - \alpha^2)^2 = 0$$

$$\lambda_n = \pm \alpha$$

So:

$$\psi_n = C_1 e^{\alpha x} + C_2 e^{-\alpha x} + C_3 x e^{\alpha x} + C_4 x e^{-\alpha x}$$

$$\psi_n' = C_1 \alpha e^{\alpha x} - C_2 \alpha e^{-\alpha x} + C_3 (e^{\alpha x} + \alpha x e^{\alpha x}) + C_4 (e^{-\alpha x} - \alpha x e^{-\alpha x}) \quad (8)$$

$$\psi_n'' = \dots \quad \left. \begin{array}{l} \psi_n''' = \dots \end{array} \right\} \text{Use Maple / MATLAB}$$

Substitute (8) into (BC1) - (BC4) to solve for C_1, C_2, C_3, C_4 .

$$\begin{bmatrix} 1 & 1 & 0 & 0 \\ \alpha & -\alpha & 1 & 1 \\ \dots & \dots & \dots & \dots \end{bmatrix} \begin{pmatrix} C_1 \\ C_2 \\ C_3 \\ C_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ -\frac{4q_0}{Dn\pi} \end{pmatrix}$$

Solve using MATLAB/Maple
Substitute into (1) and show the plots.

$$1d) \sigma_{vm} = \sqrt{\sigma_x^2 - \sigma_x \sigma_y + \sigma_y^2 + 3\tau_{xy}^2}$$

In order to find σ_x , σ_y , τ_{xy} , use:

$$M_x = -D(w_{,xx} + \nu w_{,yy})$$

$$M_y = -D(w_{,yy} + \nu w_{,xx})$$

$$M_{xy} = -D(1-\nu) w_{,xy}$$

Assuming a linear stress distribution through the thickness of the plate, we get:

$$\sigma_{x,max} = b \frac{M_x}{t^2}$$

$$\sigma_{y,max} = b \frac{M_y}{t^2}$$

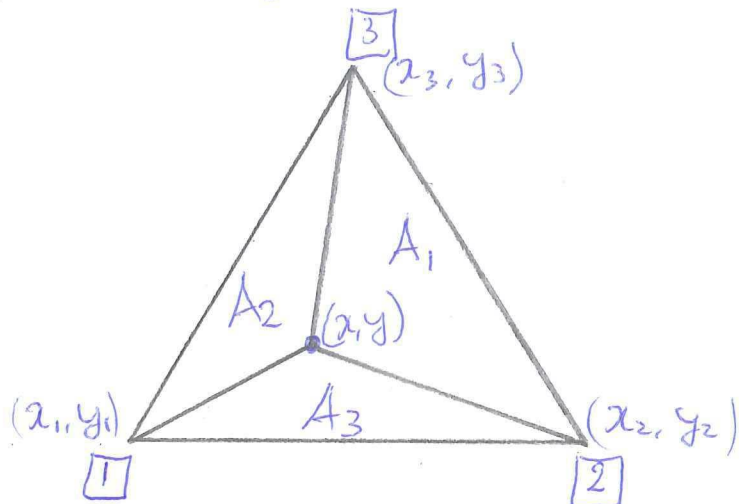
$$\tau_{xy,max} = b \frac{M_{xy}}{t^2}$$

Use these, together with the derivatives of (1) to compute σ_{vm} , and show the plots.

Problem 2

2a) One way of showing that a general point (x, y) inside the triangle can be located by

$x = \sum_{i=1}^3 x_i \xi_i$, $y = \sum_{i=1}^3 y_i \xi_i$ is as follows:



We have $A_1 + A_2 + A_3 = A$, with A the area of the large triangle

$$\Rightarrow \frac{A_1}{A} + \frac{A_2}{A} + \frac{A_3}{A} = 1 \quad (')$$

With:

$$A_1 = \frac{1}{2} \begin{vmatrix} 1 & 1 & 1 \\ x_2 & x_3 & x \\ y_2 & y_3 & y \end{vmatrix}, \quad A_2 = \frac{1}{2} \begin{vmatrix} 1 & 1 & 1 \\ x_1 & x & x_3 \\ y_1 & y & y_3 \end{vmatrix}, \quad A_3 = \frac{1}{2} \begin{vmatrix} 1 & 1 & 1 \\ x_1 & x_2 & x \\ y_1 & y_2 & y \end{vmatrix}$$

$$A = \frac{1}{2} \begin{vmatrix} 1 & 1 & 1 \\ x_1 & x_2 & x_3 \\ y_1 & y_2 & y_3 \end{vmatrix}$$

Now, let $\xi_1 \equiv \frac{A_1}{A}$, $\xi_2 \equiv \frac{A_2}{A}$, $\xi_3 \equiv \frac{A_3}{A}$.

Then it can be shown that indeed

$$x = \sum_{i=1}^3 x_i \xi_i, \quad y = \sum_{i=1}^3 y_i \xi_i$$

and with (1), we also get:

$$\xi_1 + \xi_2 + \xi_3 = 1$$

To find the expressions for ξ_1, ξ_2, ξ_3 as functions of x, x_i, y, y_i , use:

$$\begin{pmatrix} 1 \\ x \\ y \end{pmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ x_1 & x_2 & x_3 \\ y_1 & y_2 & y_3 \end{bmatrix} \begin{pmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{pmatrix}$$

$$\text{Use: } \xi_3 = 1 - \xi_1 - \xi_2 =$$

$$\begin{pmatrix} x \\ y \end{pmatrix} = \begin{bmatrix} x_1 - x_3 & x_2 - x_3 \\ y_1 - y_3 & y_2 - y_3 \end{bmatrix} \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} + \begin{pmatrix} x_3 \\ y_3 \end{pmatrix}$$

Inverting gives:

$$\begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} = \frac{1}{2A} \begin{bmatrix} y_2 - y_3 & x_3 - x_2 \\ y_3 - y_1 & x_1 - x_3 \end{bmatrix} \begin{pmatrix} x - x_3 \\ y - y_3 \end{pmatrix}, \quad \text{with } 2A = \begin{vmatrix} x_1 - x_3 & x_2 - x_3 \\ y_1 - y_3 & y_2 - y_3 \end{vmatrix}$$

2b) Simply supported means:

$$\psi_i = 0 \quad \text{on all edges}$$

$$\left. \psi_i'' \right|_{\text{normal to edge}} = 0 \quad \text{on all edges}$$

Consider the edge [2]-[3], which is characterized by $\xi_1 = 0$. So at this edge:

$$\psi_i = \xi_1^{p_{1i}} \xi_2^{p_{2i}} \xi_3^{p_{3i}} = 0 \quad \{$$

For the bending moments ($\psi'' = 0$), we have:

$$\frac{\partial^2 \psi_i}{\partial \xi_1^2} = 0 \quad \text{as this denotes the } \textcircled{a} \text{ normal direction to the edge}$$

So:

$$\psi_i = \xi_1^{p_{1i}} \xi_2^{p_{2i}} \xi_3^{p_{3i}} = \xi_1^{p_{1i}} \xi_2^{p_{2i}} \xi_3^{p_{3i}} (1 - \xi_1 - \xi_2)^{p_{3i}}$$

$$\frac{\partial \psi_i}{\partial \xi_1} = p_{1i} \xi_1^{p_{1i}-1} \xi_2^{p_{2i}} \xi_3^{p_{3i}} (1 - \xi_1 - \xi_2)^{p_{3i}} - p_{3i} \xi_1^{p_{1i}} \xi_2^{p_{2i}} \xi_3^{p_{3i}-1} (1 - \xi_1 - \xi_2)^{p_{3i}-1}$$

$$\begin{aligned} \frac{\partial^2 \psi_i}{\partial \xi_1^2} &= p_{1i}(p_{1i}-1) \xi_1^{p_{1i}-2} \xi_2^{p_{2i}} \xi_3^{p_{3i}} (1 - \xi_1 - \xi_2)^{p_{3i}} - 2p_{1i}p_{3i} \xi_1^{p_{1i}-1} \xi_2^{p_{2i}} \xi_3^{p_{3i}-1} (1 - \xi_1 - \xi_2)^{p_{3i}-1} \\ &\quad + p_{3i}(p_{3i}-1) \xi_1^{p_{1i}} \xi_2^{p_{2i}} \xi_3^{p_{3i}-2} (1 - \xi_1 - \xi_2)^{p_{3i}-2} \end{aligned}$$

From this we see that $\frac{\partial^2 \psi_i}{\partial \xi_1^2} = 0$ for $p_{1i}, p_{2i}, p_{3i} \geq 3$

The same argumentation can be applied to the other two edges.

2c) Assume $\omega = \sum_i c_i \psi_i$

From the lecture notes we get for buckling analysis the following governing equation:

$$\left(\underline{\underline{K}} - \lambda \underline{\underline{K}}_g \right) \underline{\underline{u}} = \underline{\underline{0}} \quad (9)$$

with

$$K_{ij} = \iint_A D \left[\psi_{i,xx} \psi_{j,xx} + \psi_{i,yy} \psi_{j,yy} + \nu (\psi_{i,xx} \psi_{j,yy} + \psi_{i,yy} \psi_{j,xx}) + 2(1-\nu) \psi_{i,xy} \psi_{j,xy} \right] dA \quad (10)$$

$$K_{gij} = - \iint_A \left[N_x \psi_{i,x} \psi_{j,x} + N_y \psi_{i,y} \psi_{j,y} \right] dA \quad (\text{for } N_{xy} = 0) \quad (11)$$

For equal biaxial loading we can assume $N_x = N_y = 1$ such that λ in (9) becomes the buckling load, and $\underline{\underline{u}}$ in (9) becomes the eigenvector, i.e. the collection of c_i that makes up the mode.

From Q. 2a we know that:

$$\begin{pmatrix} x \\ y \end{pmatrix} = \underline{\underline{y}} \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} + \begin{pmatrix} x_3 \\ y_3 \end{pmatrix}$$

$$\text{with } \underline{\underline{y}} = \begin{bmatrix} x_1 - x_3 & x_2 - x_3 \\ y_1 - y_3 & y_2 - y_3 \end{bmatrix} = \begin{bmatrix} \frac{\partial x}{\partial \xi_1} & \frac{\partial x}{\partial \xi_2} \\ \frac{\partial y}{\partial \xi_1} & \frac{\partial y}{\partial \xi_2} \end{bmatrix} \quad (12)$$

Therefore :

$$\begin{pmatrix} \psi_{ix} \\ \psi_{iy} \end{pmatrix} = \underline{\underline{Y}}^{-1} \begin{pmatrix} \frac{\partial \psi_i}{\partial \xi_1} \\ \frac{\partial \psi_i}{\partial \xi_2} \end{pmatrix} \quad (13)$$

which can be easily evaluated using $\psi_i = \xi_1^{P_{i1}} \xi_2^{P_{i2}} (+\xi_1 - \xi_2)^{P_{i3}}$

Then also:

$$\psi_{ixx} = \underline{\underline{Y}}^{-1} (1, :) \begin{pmatrix} \frac{\partial \psi_{i,x}}{\partial \xi_1} \\ \frac{\partial \psi_{i,x}}{\partial \xi_2} \end{pmatrix} \quad (14)$$

First row of $\underline{\underline{Y}}^{-1}$ → Can be evaluated from (13), as this equation gives ψ_{ix} as function of ξ_1, ξ_2

Similarly:

$$\psi_{iyy} = \underline{\underline{Y}}^{-1} (2, :) \begin{pmatrix} \frac{\partial \psi_{i,y}}{\partial \xi_1} \\ \frac{\partial \psi_{i,y}}{\partial \xi_2} \end{pmatrix} \quad (15)$$

$$\psi_{ixy} = \underline{\underline{Y}}^{-1} (1, :) \begin{pmatrix} \frac{\partial \psi_{i,y}}{\partial \xi_1} \\ \frac{\partial \psi_{i,y}}{\partial \xi_2} \end{pmatrix} \quad (16)$$

Also:

$$dA = \det(\underline{\underline{Y}}) d\xi_1 d\xi_2 = 2A d\xi_1 d\xi_2 \quad (17)$$

Substitution of (13)-(14) into (10) & (11) gives the stiffness matrices. The integration boundaries are:

$$\int_0^1 \int_0^{1-\xi_1} [\dots] d\xi_2 d\xi_1$$

The number of modes is determined by the permutations satisfying $p_0 \leq p_{ii} + p_{zi} + p_{zi} \leq p$, with $p_0 = 9$ and $p_{ii}, p_{zi}, p_{zi} \geq 3$. So:

$$p=9: \quad \begin{array}{ccc} p_{ii} & p_{zi} & p_{zi} \\ \hline 3 & 3 & 3 \end{array}$$

$$p=10: \quad \begin{array}{ccc} p_{ii} & p_{zi} & p_{zi} \\ \hline 3 & 3 & 3 \\ 4 & 3 & 3 \\ 3 & 4 & 3 \\ 3 & 3 & 4 \end{array}$$

$$p=11: \quad \dots$$

$$p=12: \quad \dots$$

Now ~~everything~~ \underline{k} and \underline{k}_g are fully defined for a given p , and (9) can be solved.

The values for λ need to be presented in the report together with the mode shapes obtained from \underline{u} is (9).

Convergence of λ has to be discussed.