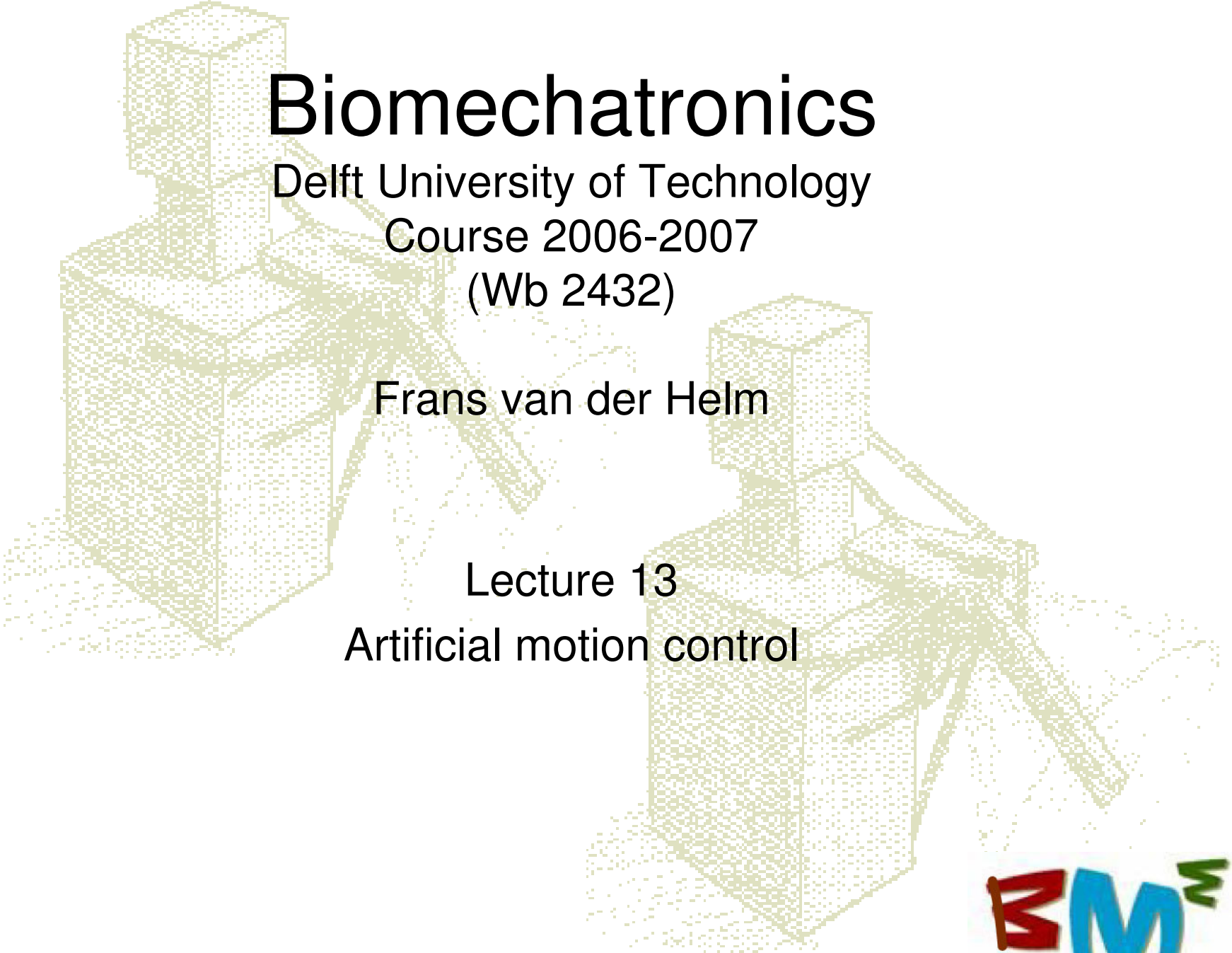




Biomechatronics

Delft University of Technology

Course 2006-2007

(Wb 2432)

Frans van der Helm

Lecture 13

Artificial motion control



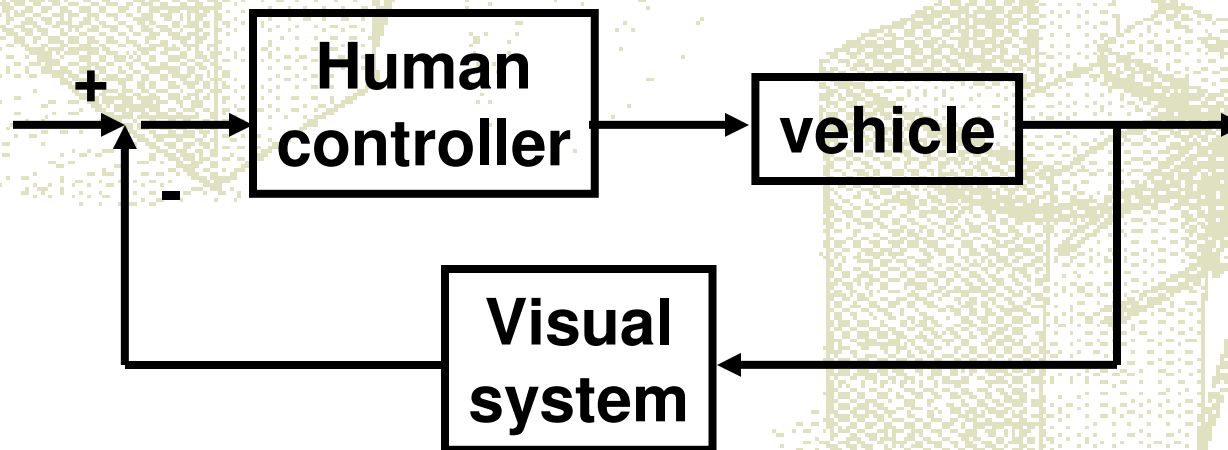
Contents

- Introduction
- Definitions from control engineering
 - dynamical systems
 - stability
 - Phase-margin and gain margin
- Model of human controller
 - stability analysis
 - limitations and adaptation
- Supervisory control situations
 - supervisor over automated control loops



The human as controller

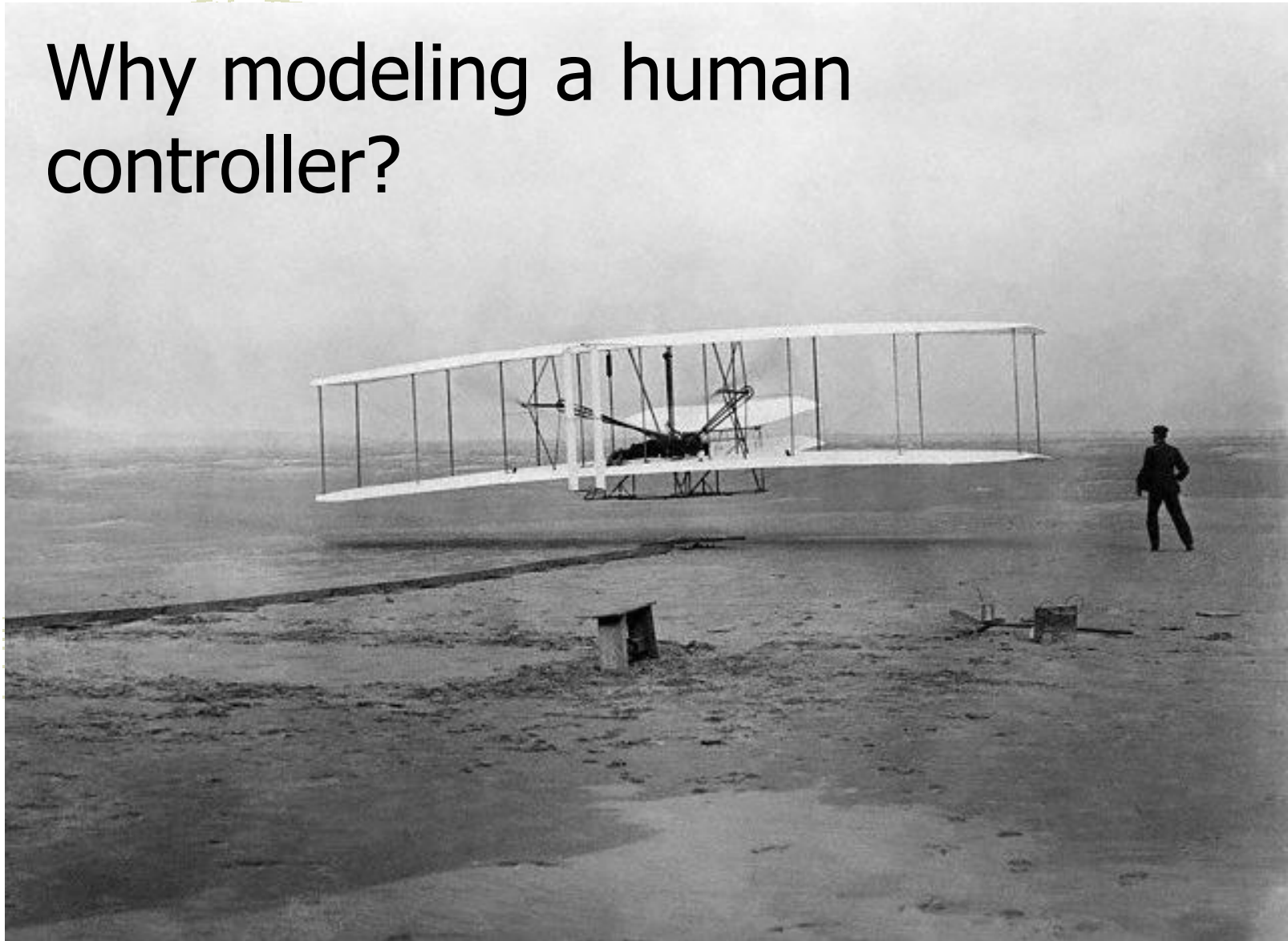
- Marine vessels
- Vehicles
- Airplanes
-



Closed-loop system



Why modeling a human controller?

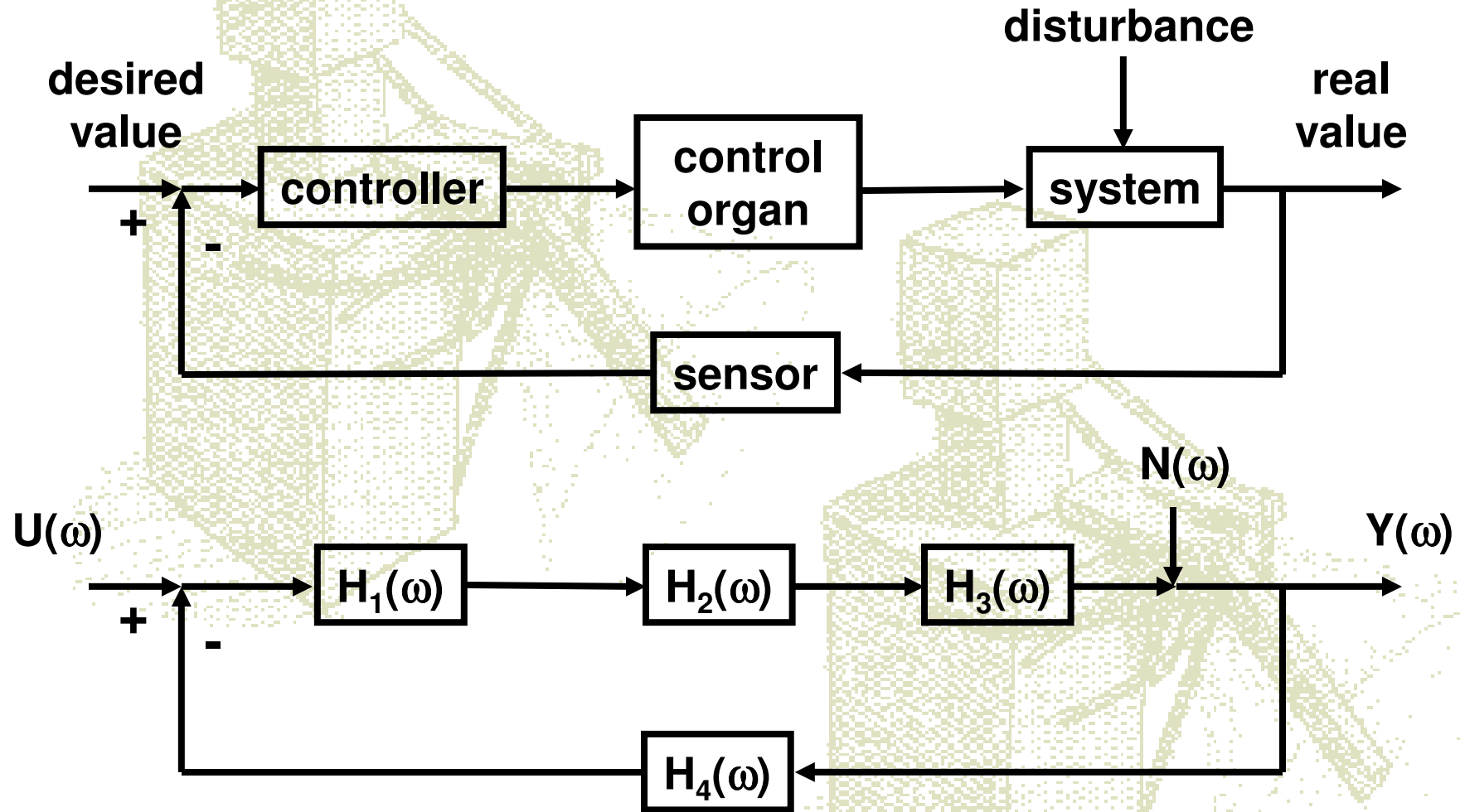


BM³



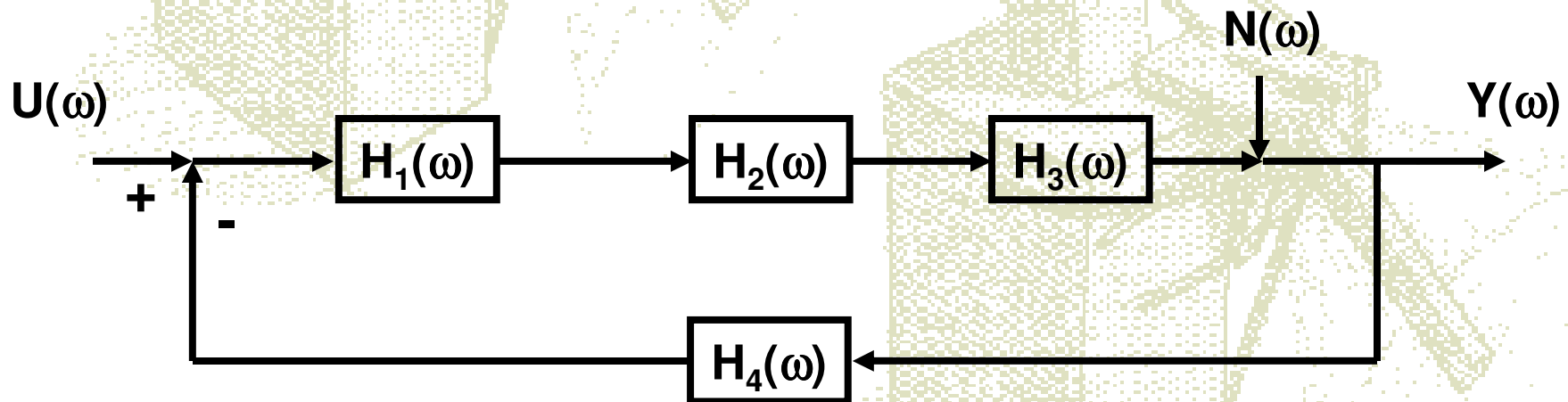
BM^M

Block diagram of a control loop

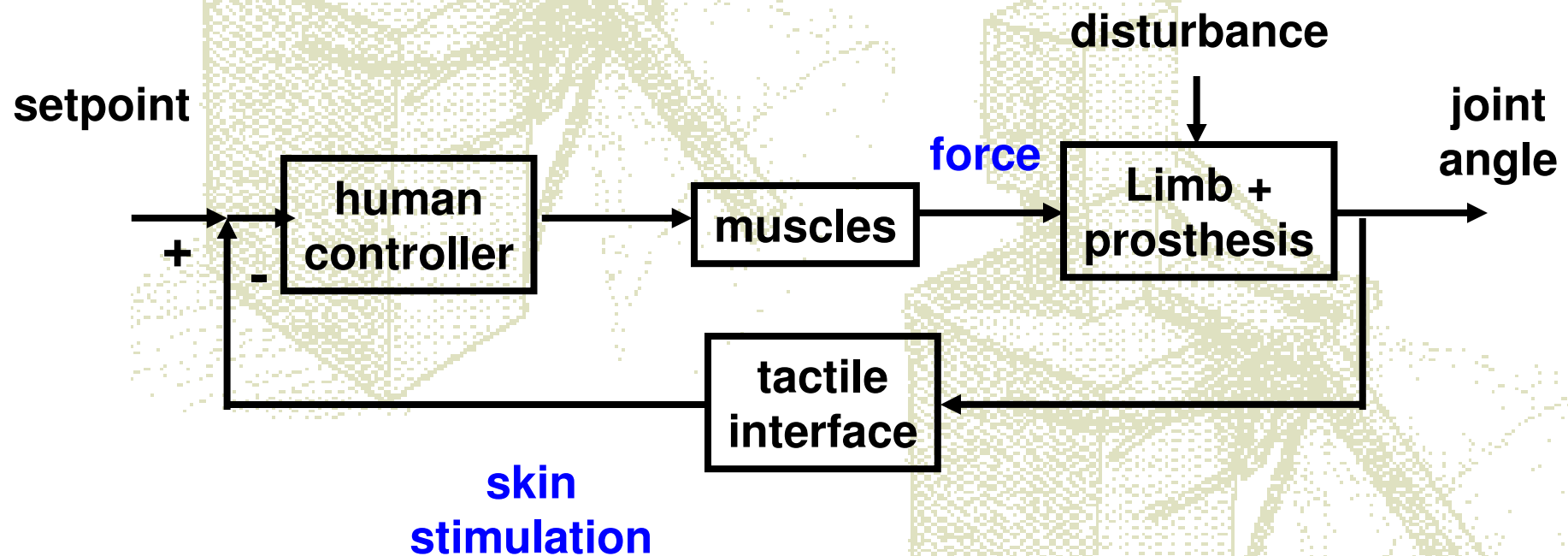


Block diagram of a control loop

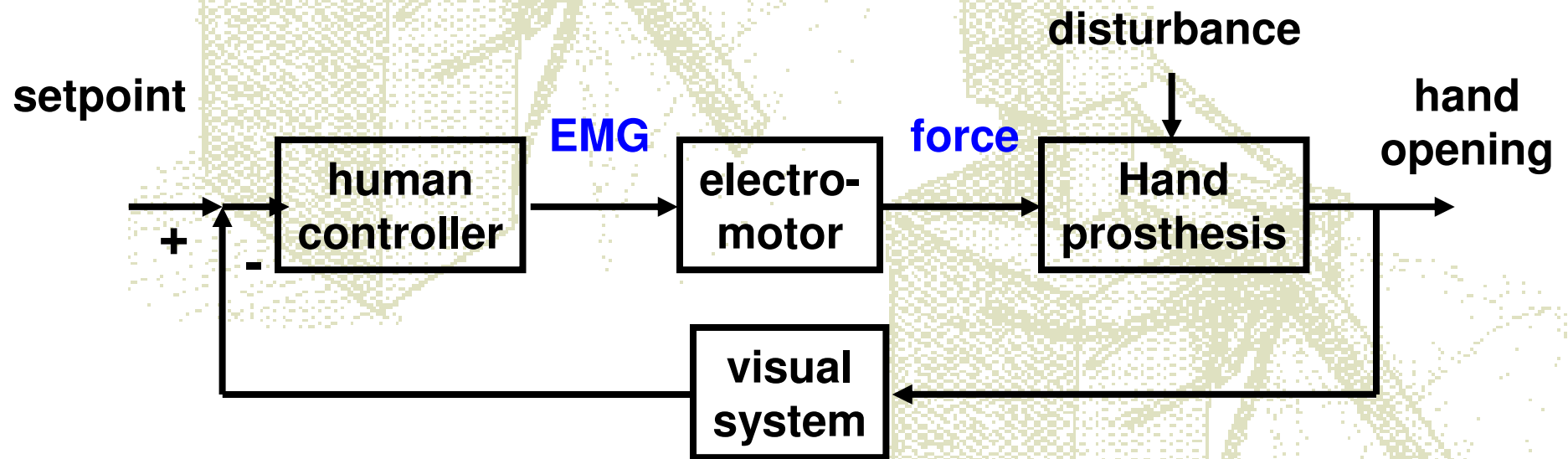
$$Y = \frac{H_1 H_2 H_3}{1 + H_1 H_2 H_3 H_4} U + \frac{1}{1 + H_1 H_2 H_3 H_4} N$$



Examples in biomechatronics



Examples in biomechatronics



Stability of a control loop

- Stability: Analyze loop gain function

$$H_r = H_1 \cdot H_2 \cdot H_3 \cdot H_4$$

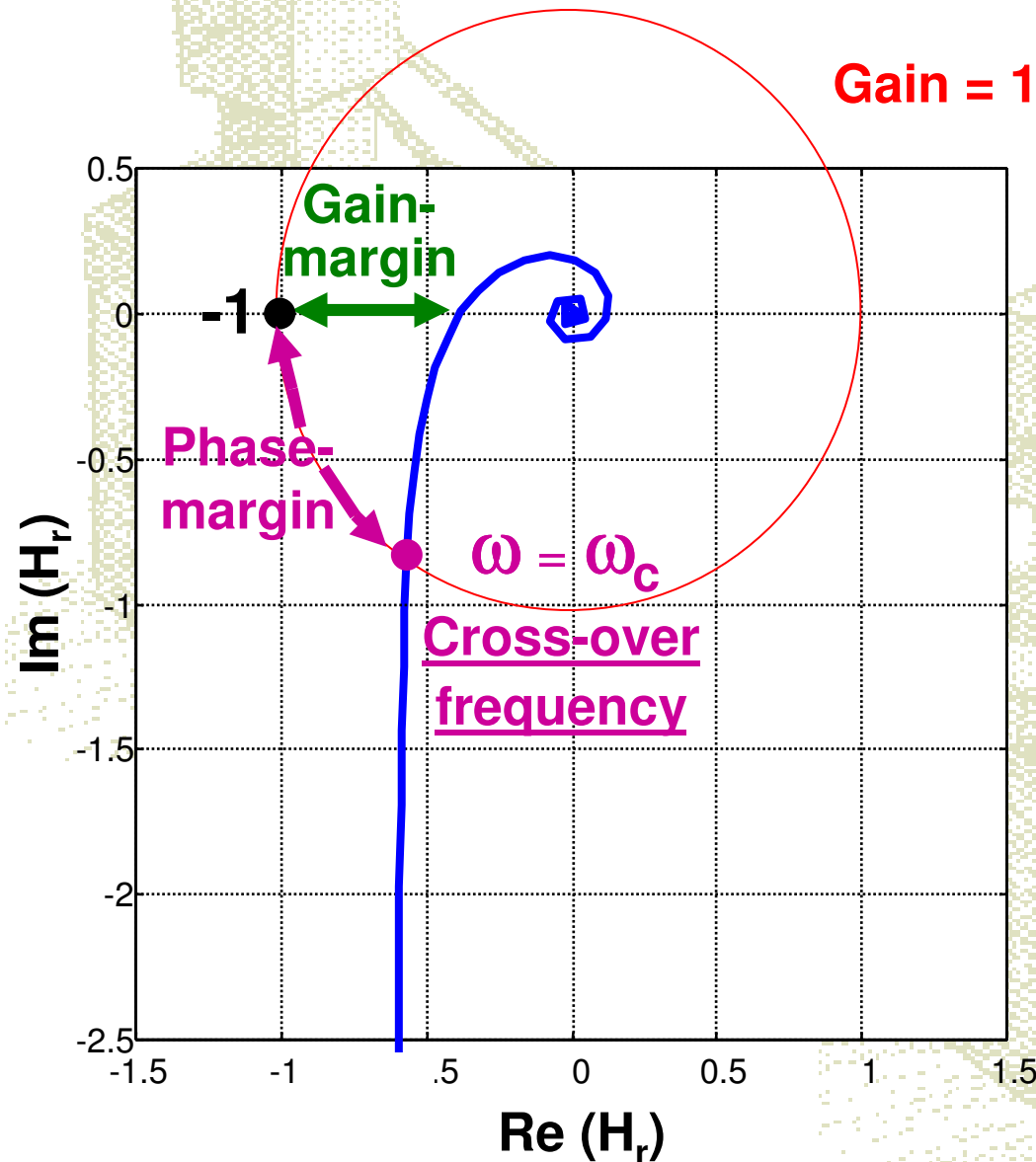
- $H_r(\omega)$ is complex:
mod $H_r(\omega)$ = gain, arg $H_r(\omega)$ = phase

- Phase-margin:
If mod $H_r(\omega) = 1$ then arg $H_r(\omega) > -180^\circ$

- Gain-margin:
If arg $H_r(\omega) = -180^\circ$ then mod $H_r(\omega) < 1$



Phase-margin & gain-margin

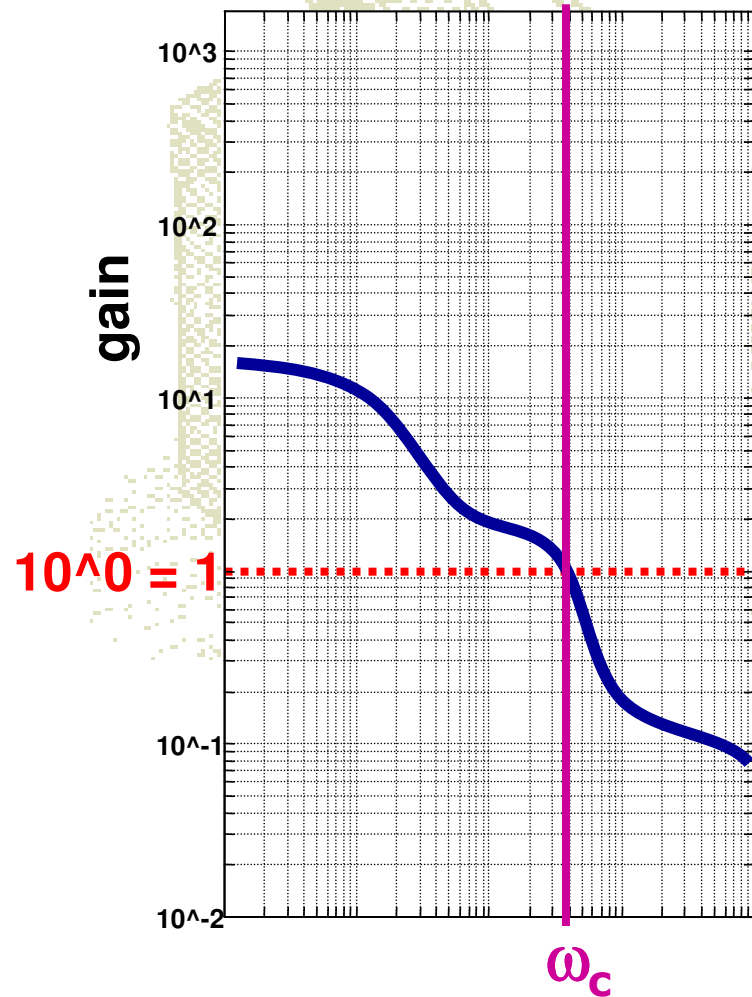


Nyquist
plot
 H_r

BM^M

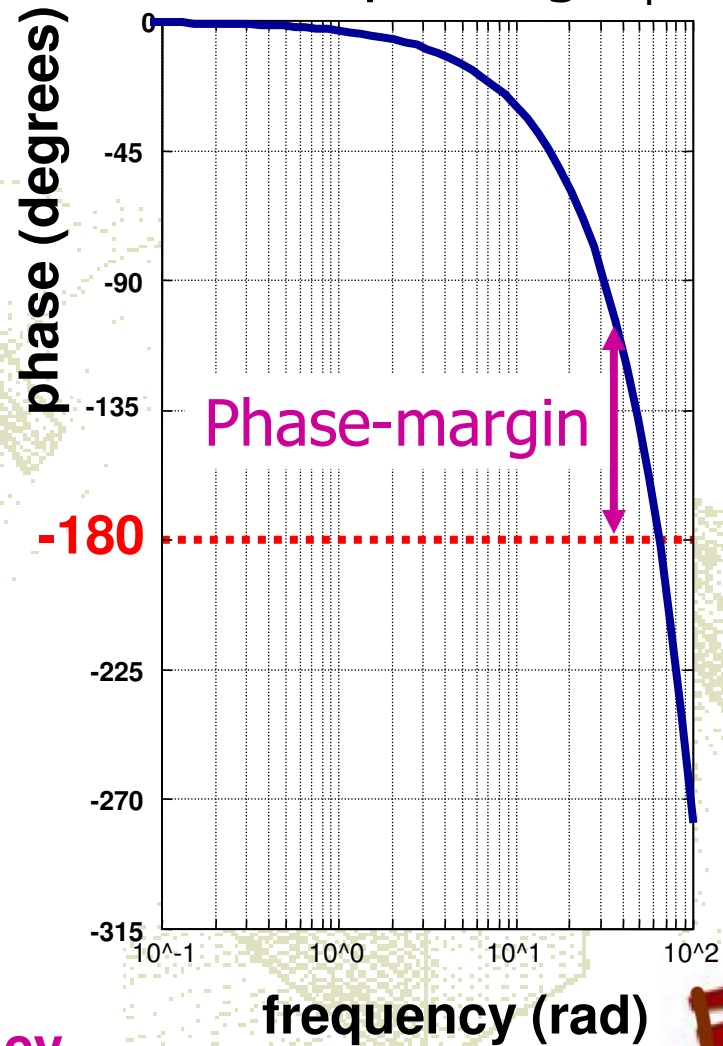
Phase-margin

Bode-plot mod H_r



Cross-over frequency

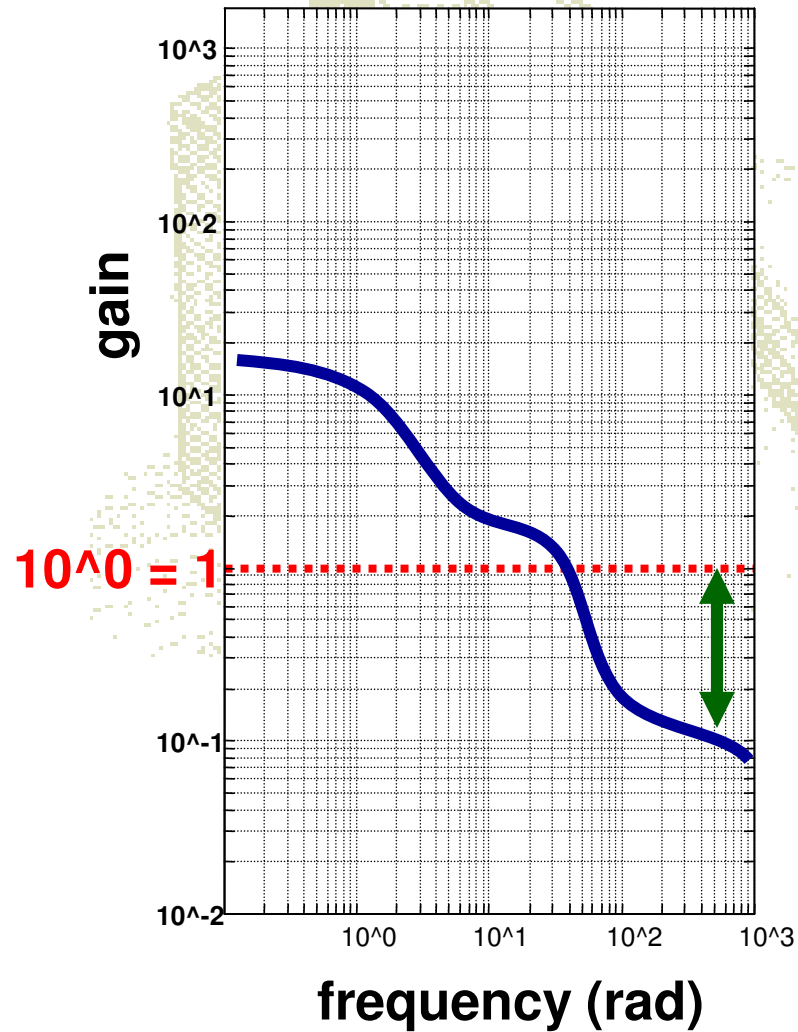
Bode-plot arg H_r



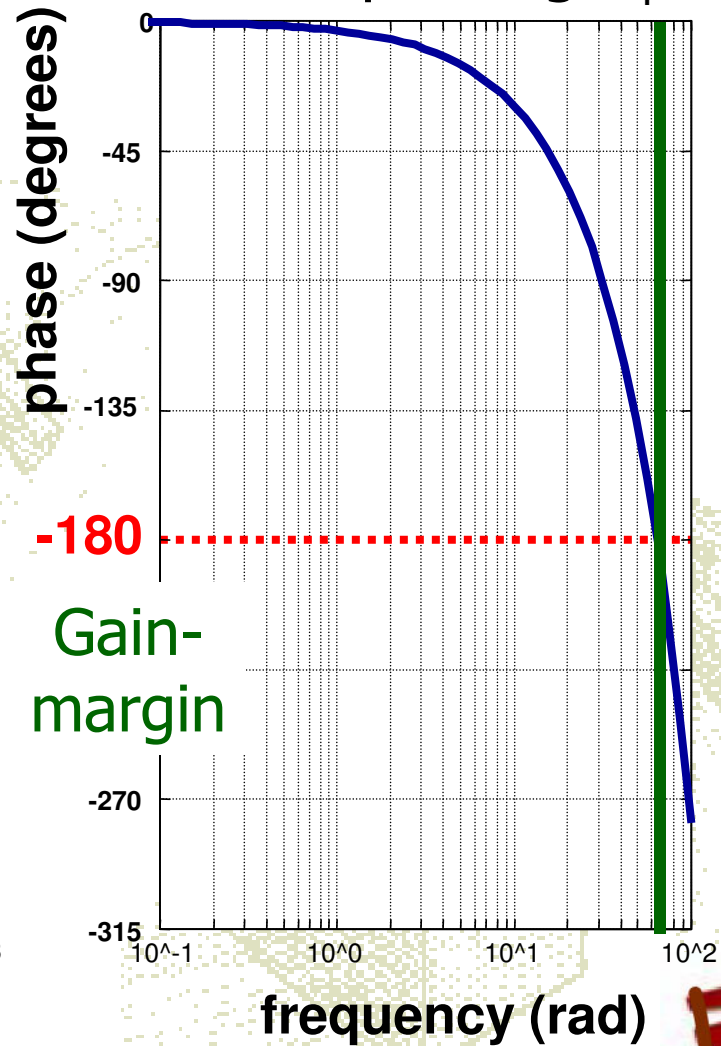
BM³

Gain-margin

Bode-plot mod H_r



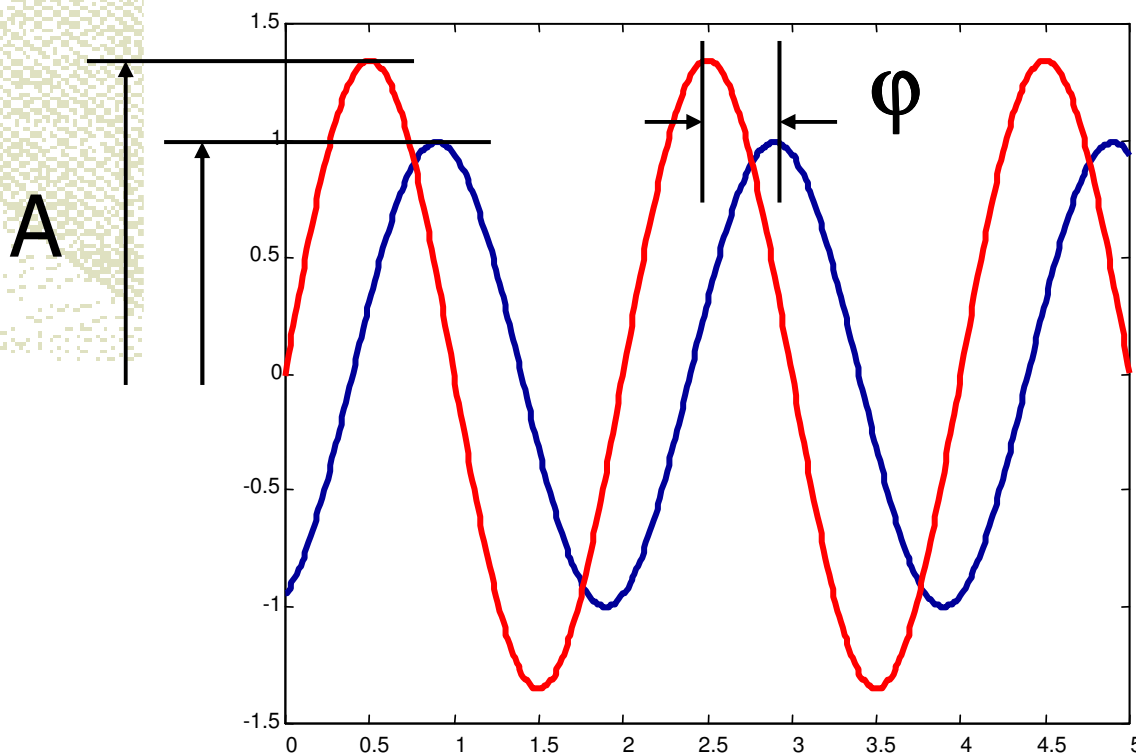
Bode-plot arg H_r



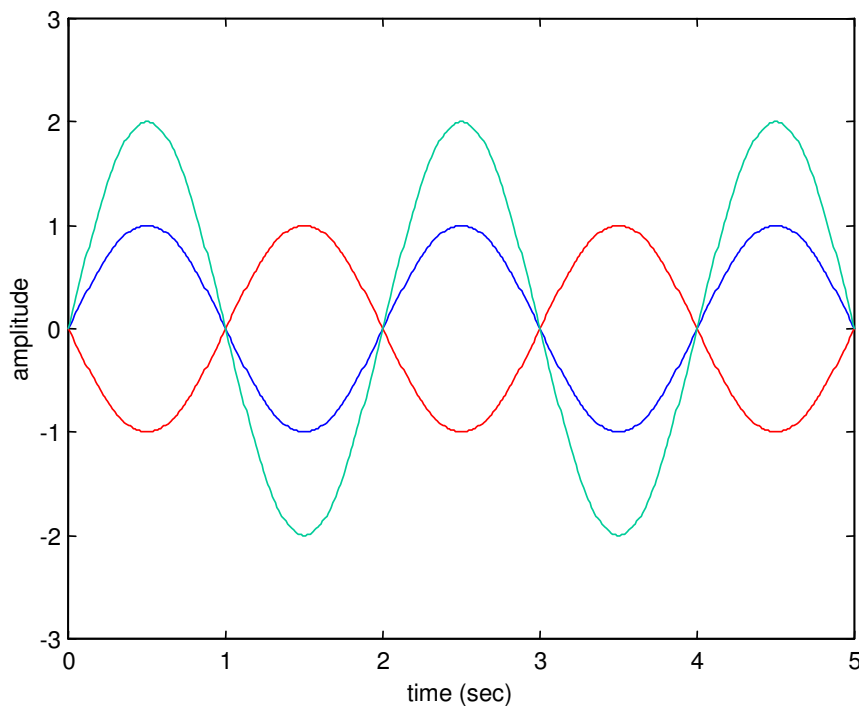
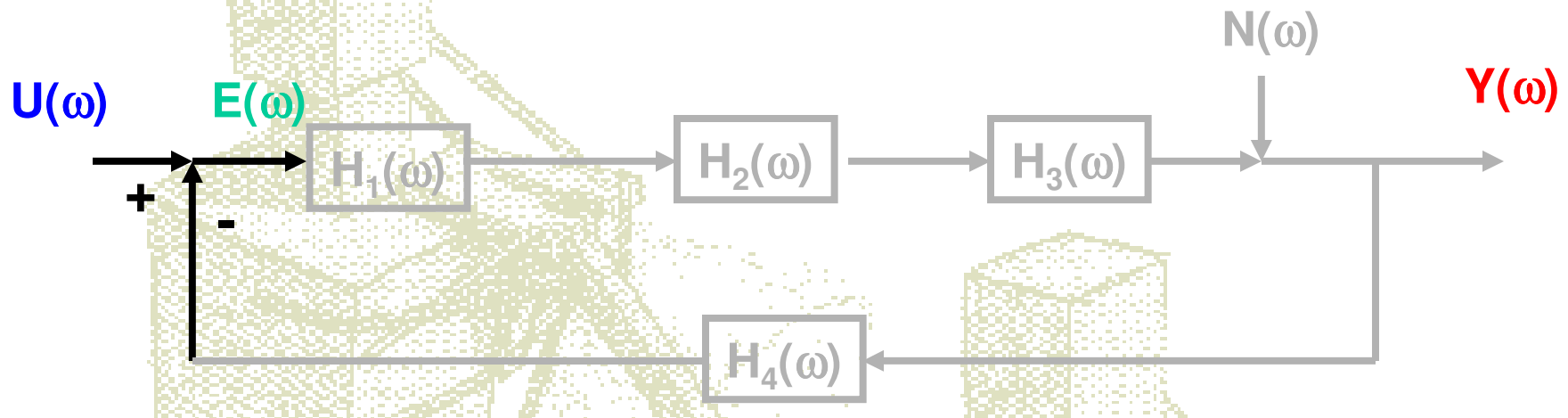
BM³

Input- & output signals

- Input: $u(t) = \sin(\omega t)$
- Output: $y(t) = A \sin(\omega t + \varphi)$
- Gain A en phase φ



Stability of a control loop

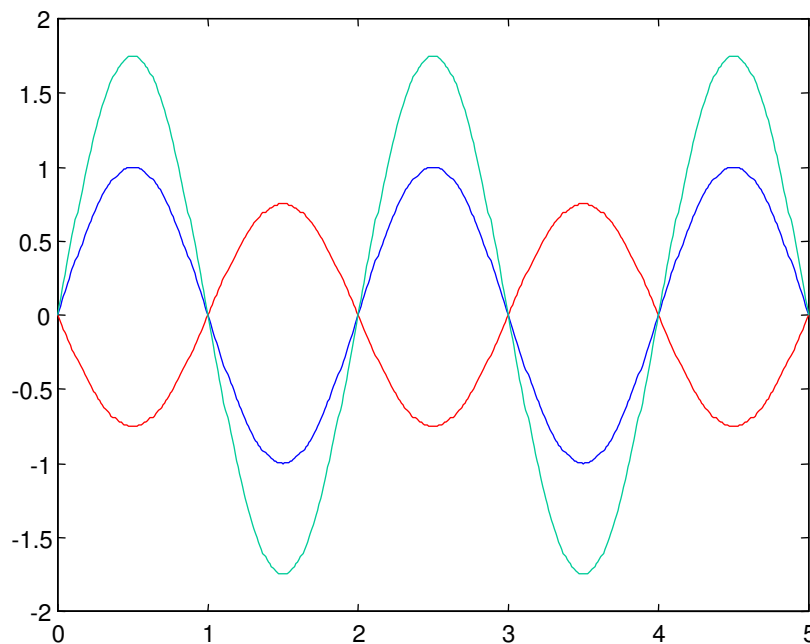
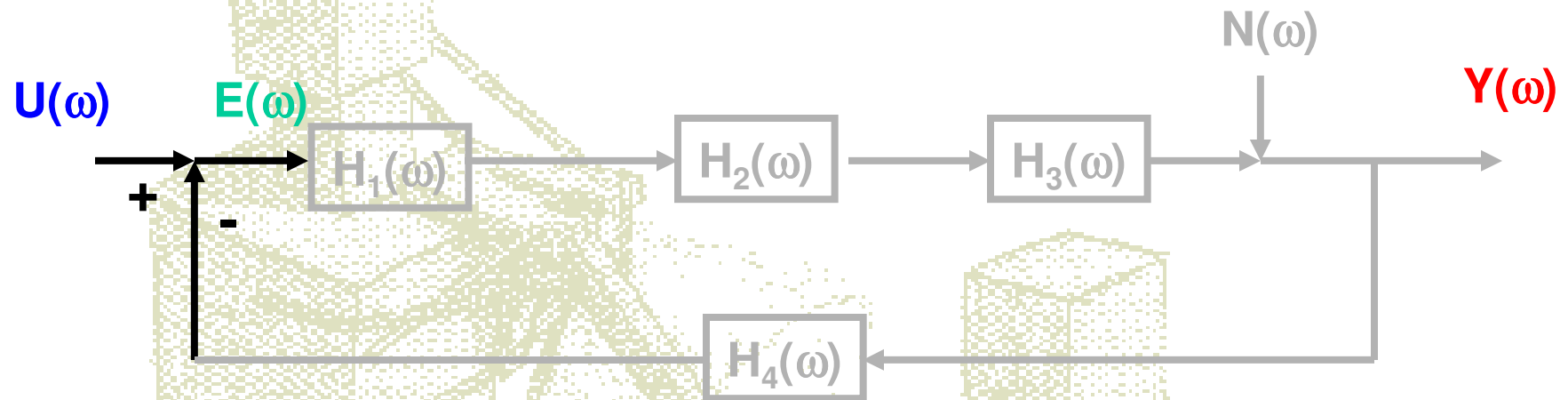


Phase-lag $H_r = -180^\circ$

- Gain $H_r < 1$
 $\Rightarrow$ stable
- Gain $H_r = 1$
 $\Rightarrow$ on verge of instability
- Gain $H_r > 1$
 $\Rightarrow$ unstable

BM^M

Stability of a control loop

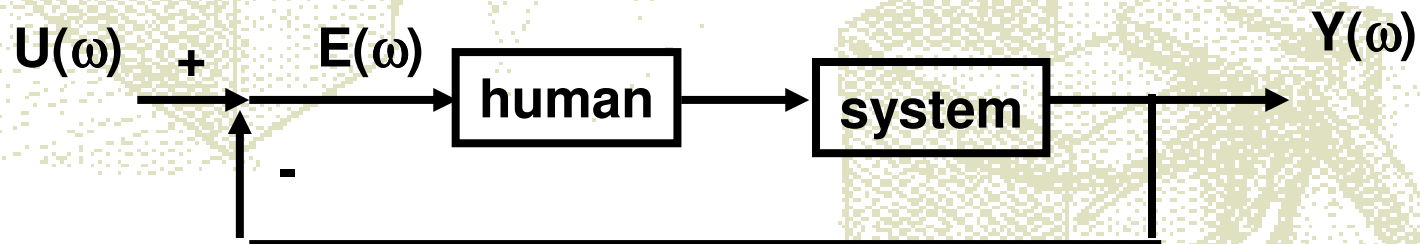
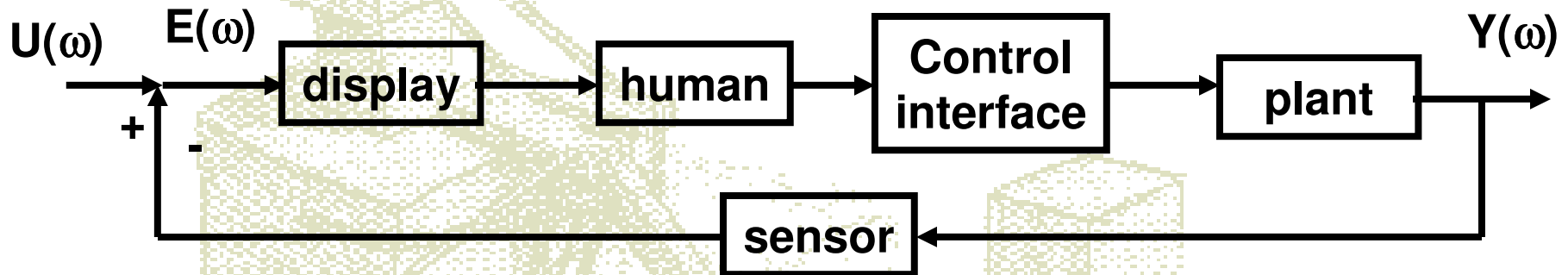


Phase shift = -180 degrees
gain = 0.75

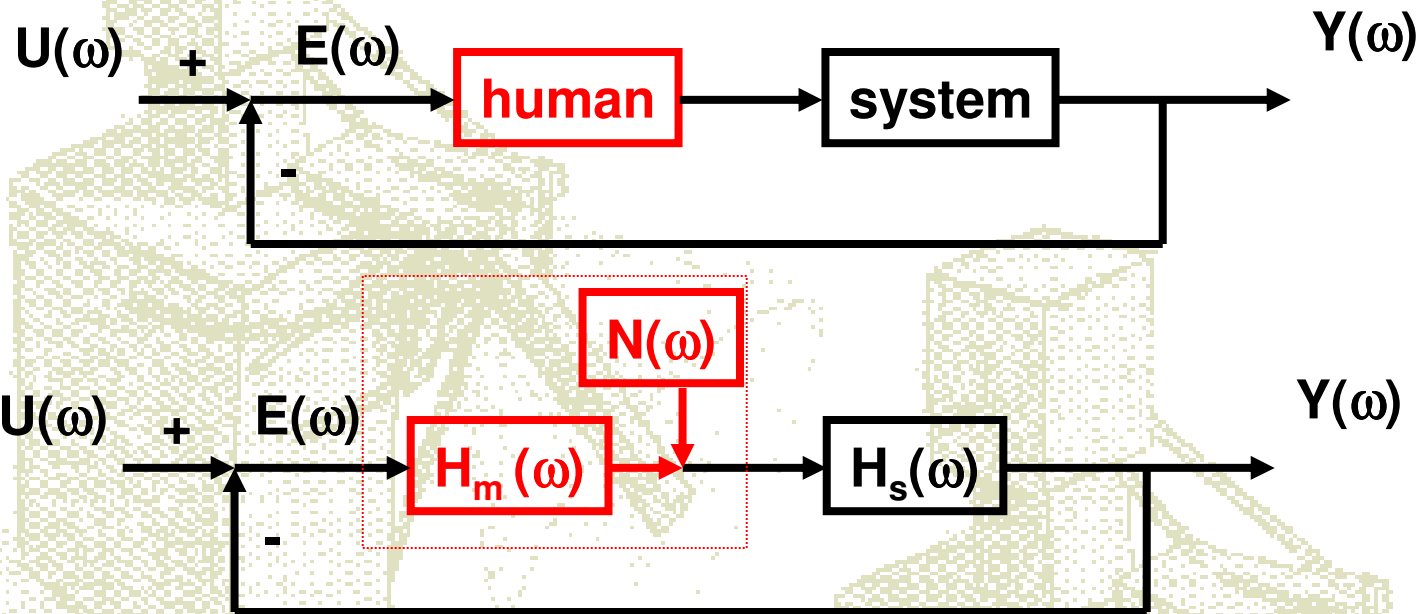
Positive gain margin



Model human controller



Model human controller 1



McRuer:

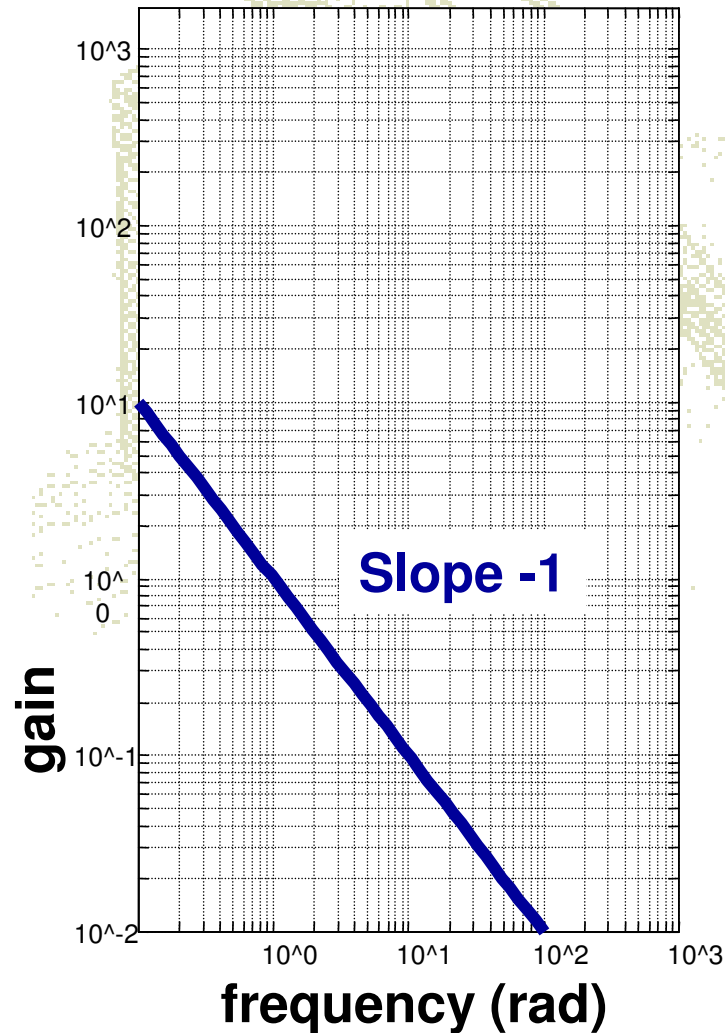
- Human shows different behaviour when controlling different systems
- Human tries to simulate servo-behaviour:

$$H_r(\omega) = H_m(\omega) \cdot H_s(\omega) = 1/j\omega$$

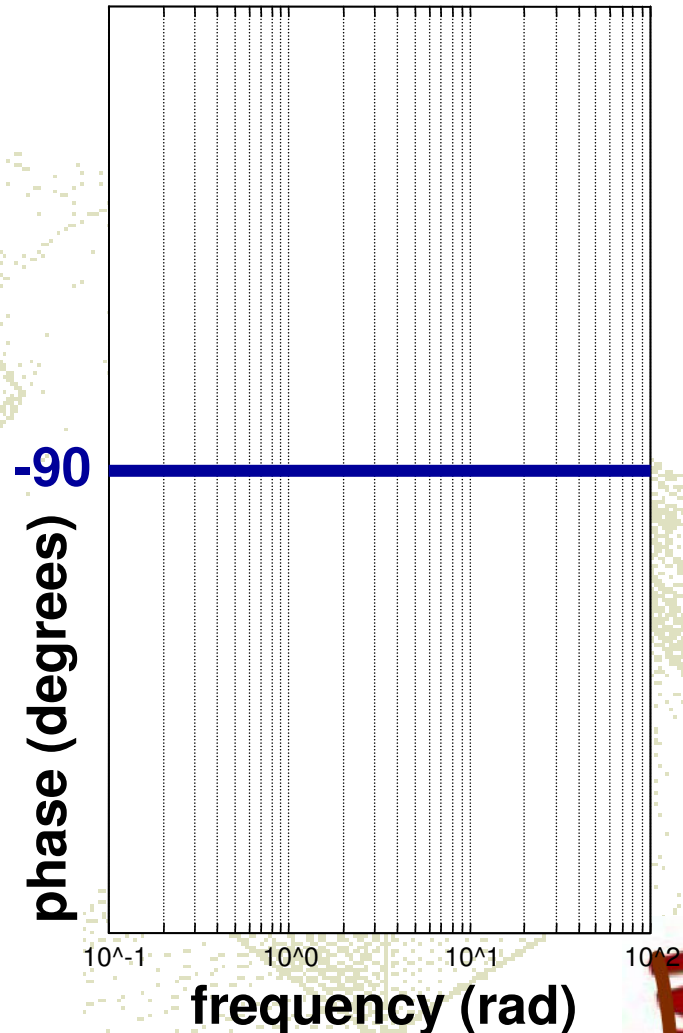


Optimal servo behaviour: $H_r(\omega) = 1/j\omega$

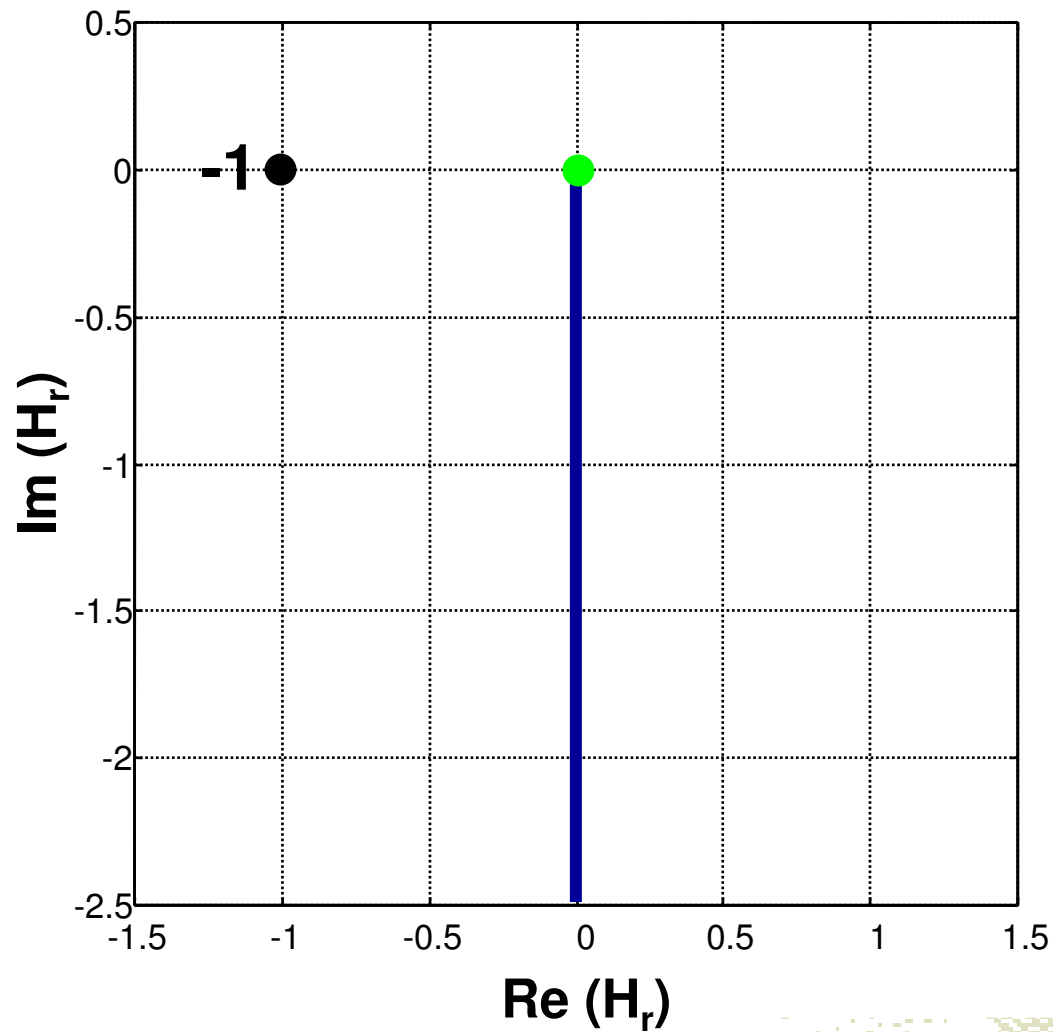
Bode-plot mod H_r



Bode-plot arg H_r



Optimal servo behaviour: $H_r(\omega) = 1/j\omega$



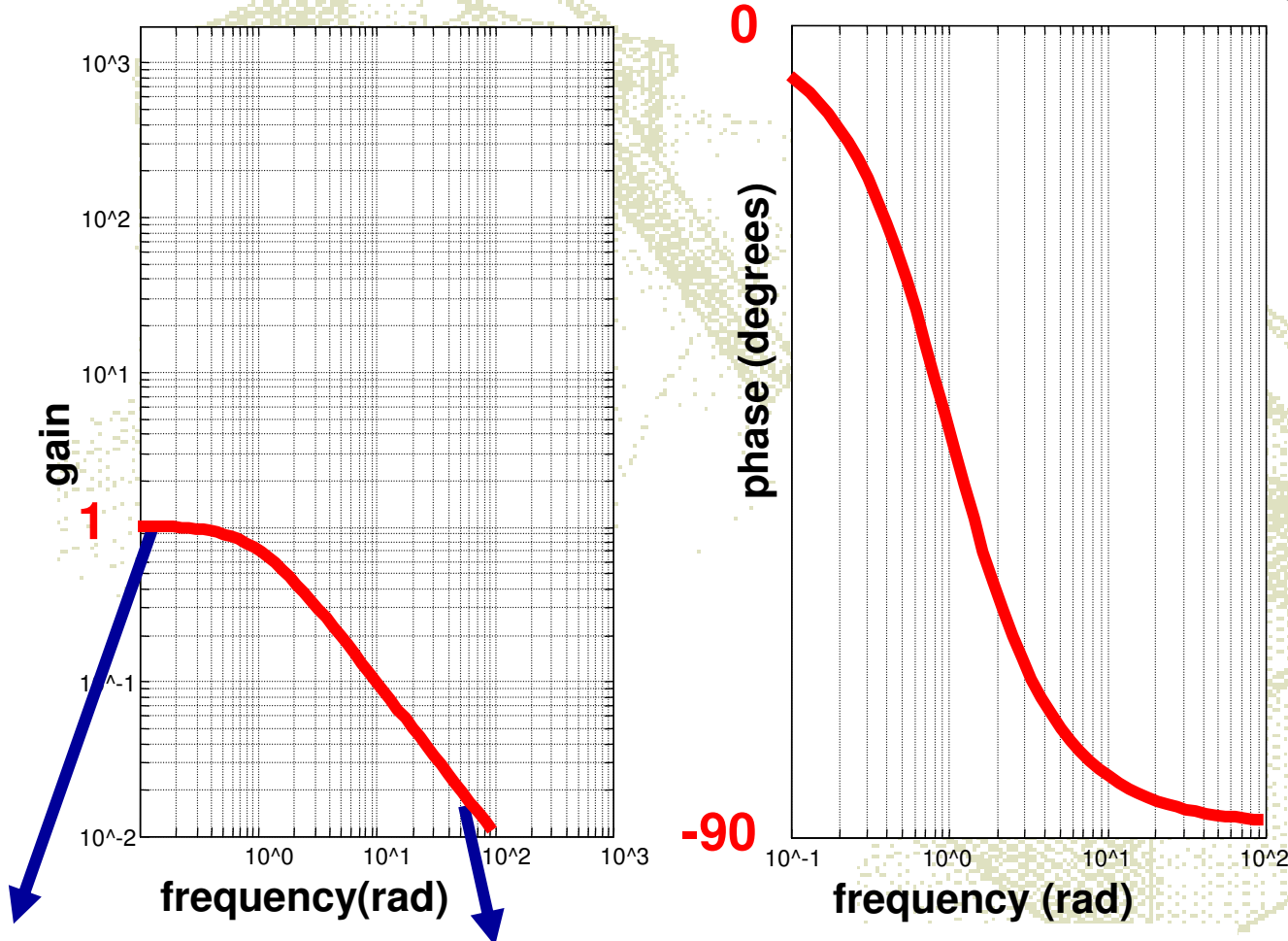
Nyquist
plot
 H_r

Always
stable



Transfer input-output

$$H_{uy}(\omega) = \frac{Y(\omega)}{U(\omega)} = \frac{\frac{1}{j\omega}}{1 + \frac{1}{j\omega}} = \frac{1}{j\omega + 1}$$

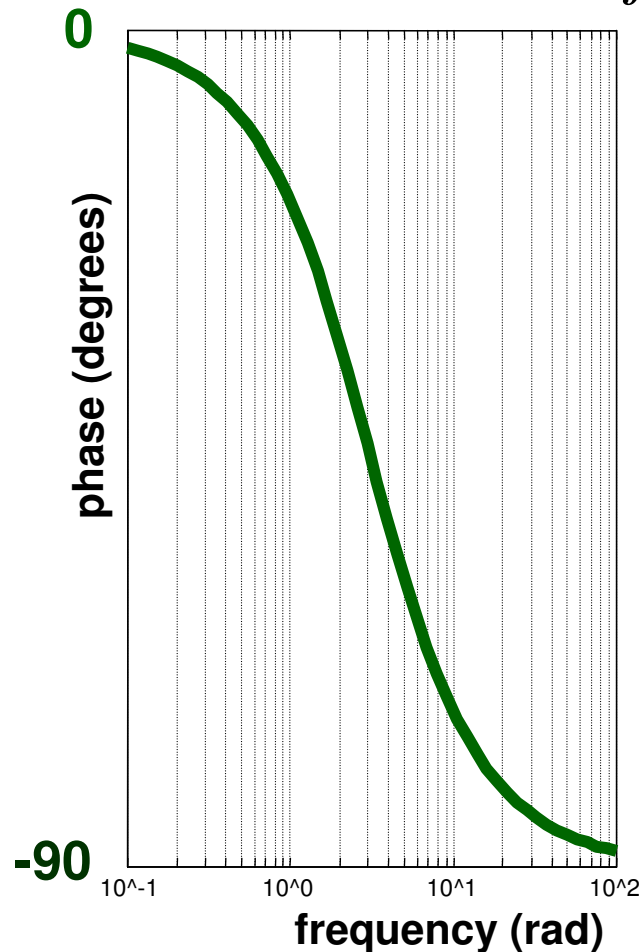
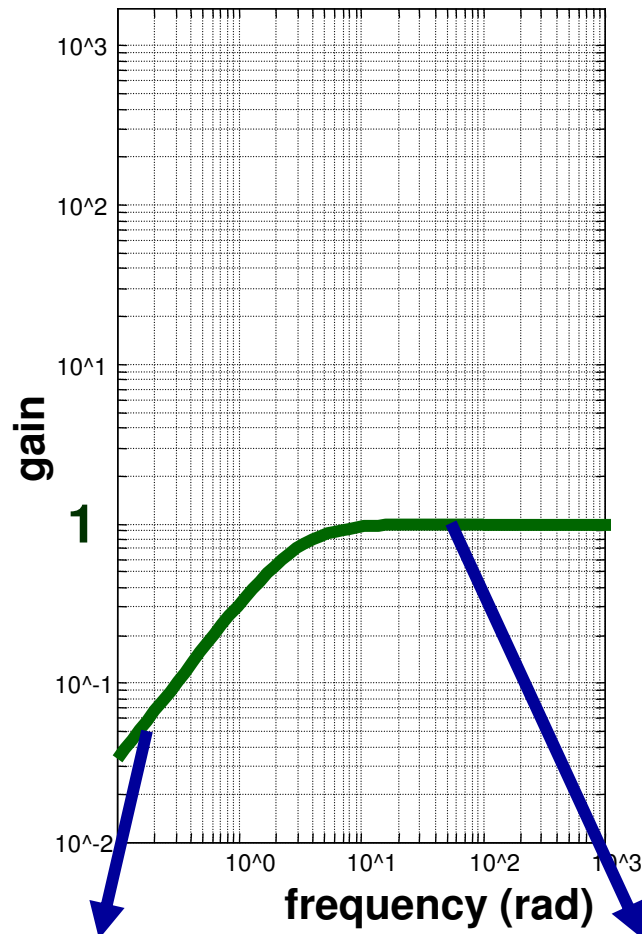


Low frequencies: transfer almost 1
 High frequencies: transfer almost 0
 Input is followed accurately
 Input is followed badly

BM

Transfer input-error

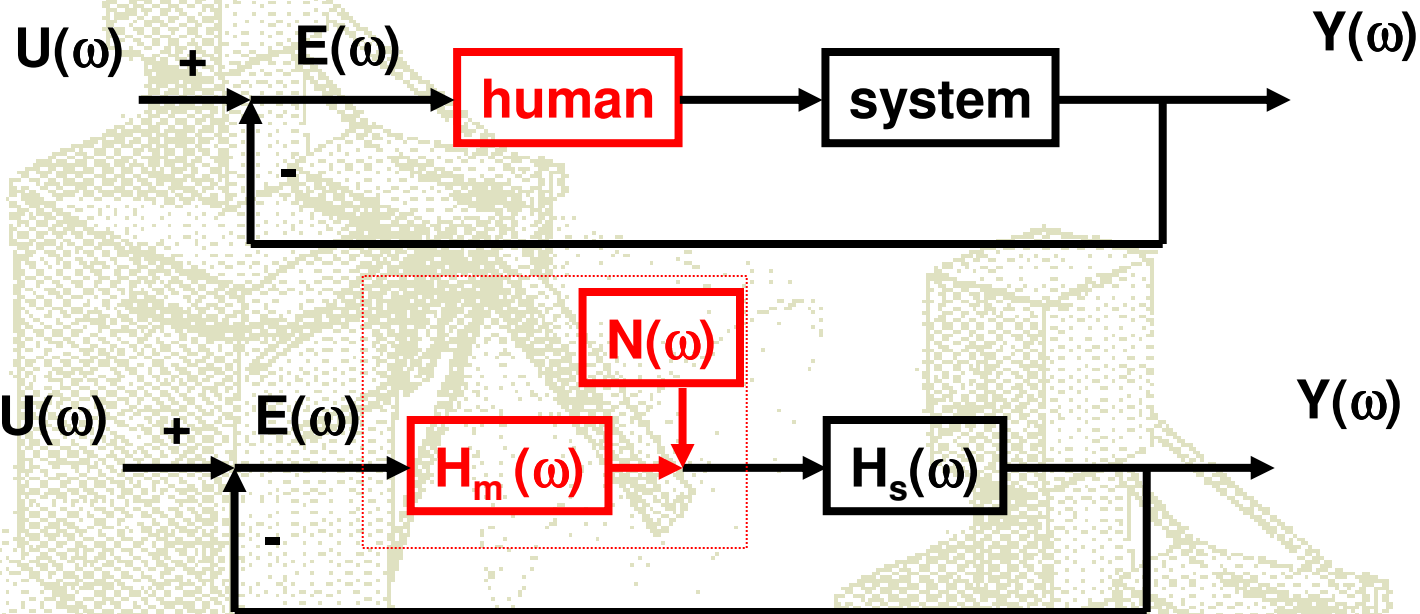
$$H_{ue}(\omega) = \frac{E(\omega)}{U(\omega)} = \frac{1}{1 + \frac{1}{j\omega}} = \frac{j\omega}{j\omega + 1}$$



Low frequencies: error High frequencies: error = input
Input is followed accurately Input is followed badly



Model human controller 2



McRuer:

- Human tries to approximate optimal servo-behaviour: $H_r(\omega) = H_m(\omega) \cdot H_s(\omega) \approx 1/j\omega$

But is not perfect!

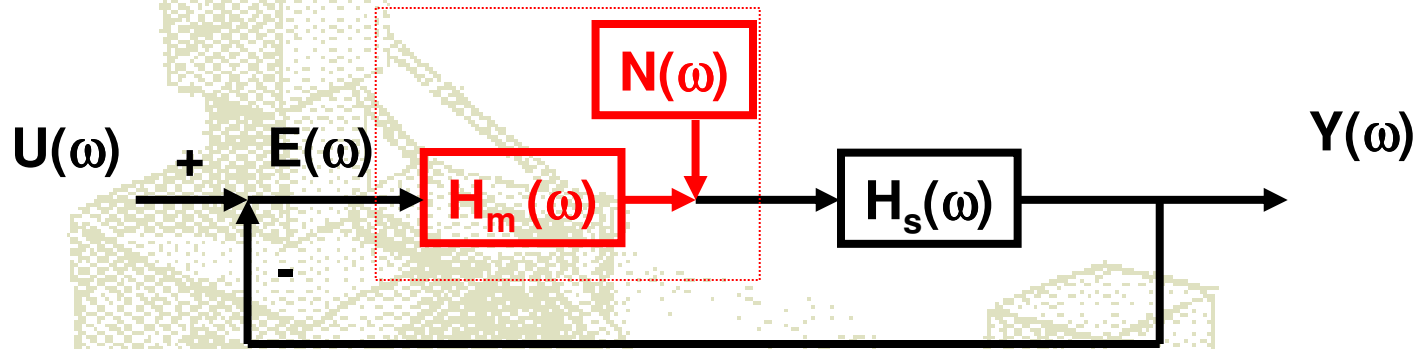


Limitations & adaptability human controller

- Limitations:
 - Human needs processing time
 - Inertia neuromuscular system arm with control organ
 - Human has limited accuracy
 - Human can estimate speed reasonably
but cannot estimate acceleration
- Adaptability:
 - Human can adapt well to system dynamics
 - Human tries to develop optimal control strategy
(effort versus result)



Cross-over model



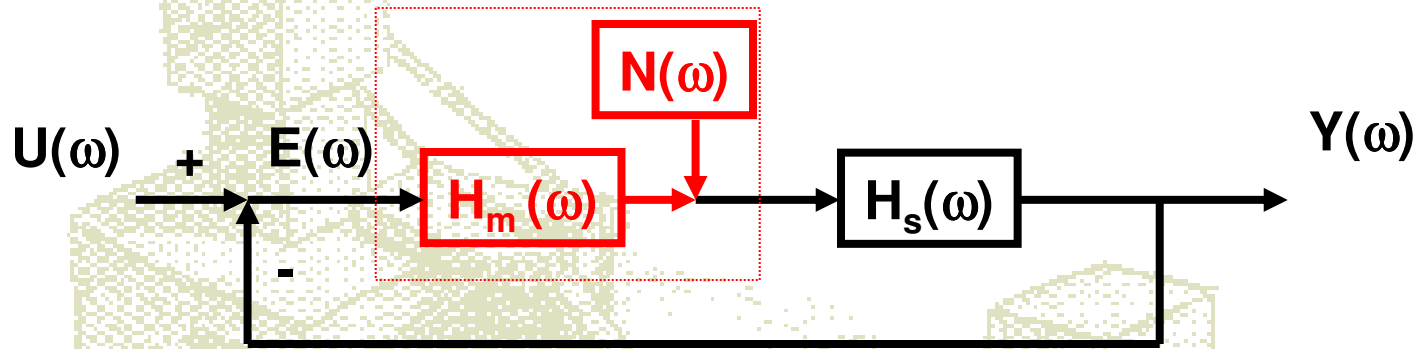
$$H_m(\omega) = K_m \underbrace{\frac{1 + j\omega\tau_1}{1 + j\omega\tau_2}}_{\text{adaptability}} \cdot \underbrace{\frac{1}{1 + j\omega\tau_3}}_{\text{limitations}} \cdot e^{-j\omega\tau_v}$$

For low frequencies ($\omega < 3 \text{ rad/s} \approx 0.5 \text{ Hz}$):

$$H_m(\omega) = K_m \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} \cdot e^{-j\omega\tau_e}$$



Cross-over model



For frequencies around $\omega = \omega_c$ human tries to:

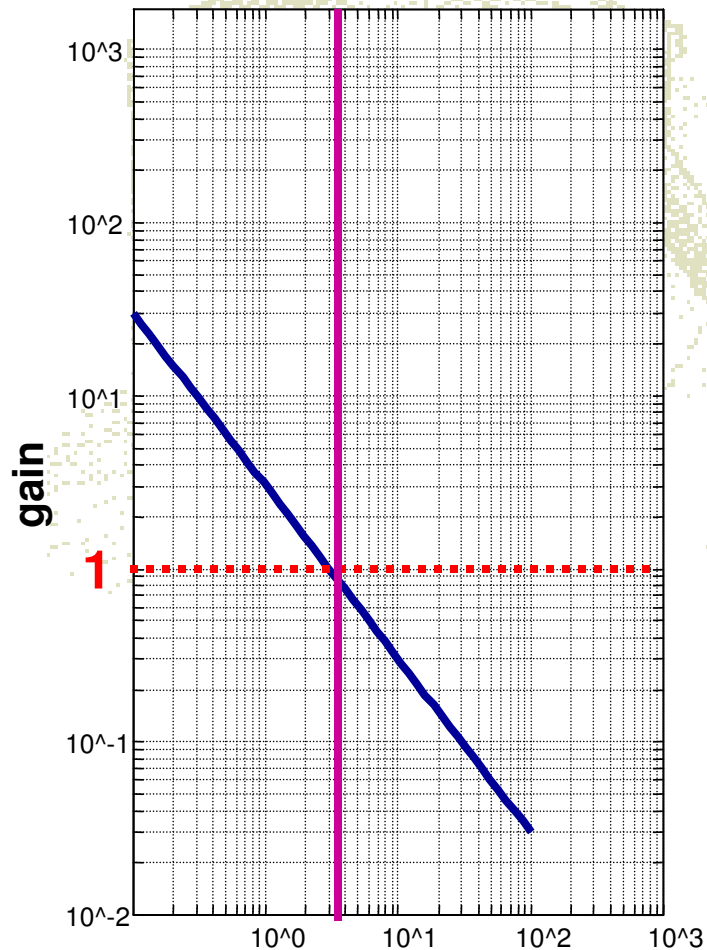
$$H_m(\omega).H_s(\omega) = \frac{\omega_c}{j\omega} e^{-j\omega\tau_e}$$

- Loop gain is then equal to 1
- Loop gain function approximates integrator
- ω_c roughly between 2 & 6 rad/s (≈ 0.3 & 1 Hz)
- τ_e equal to 200 till 300 ms



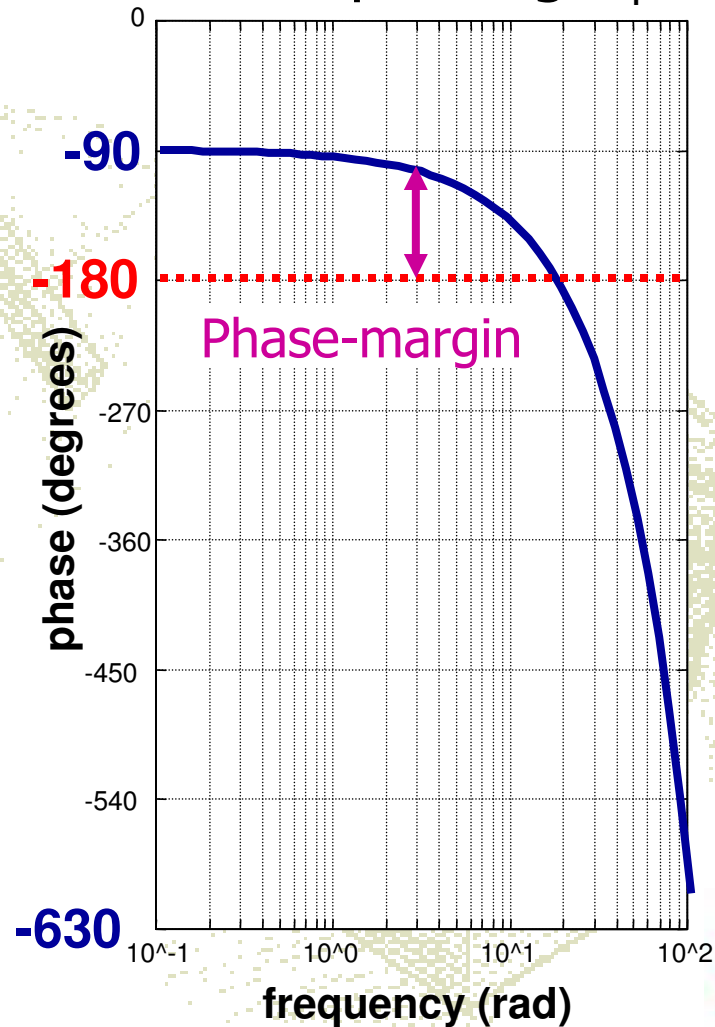
$$H_r(\omega) = H_m(\omega) \cdot H_s(\omega) = \omega_c / j(\omega) \cdot e^{-j\omega\tau_e}$$

Bode-plot mod H_r



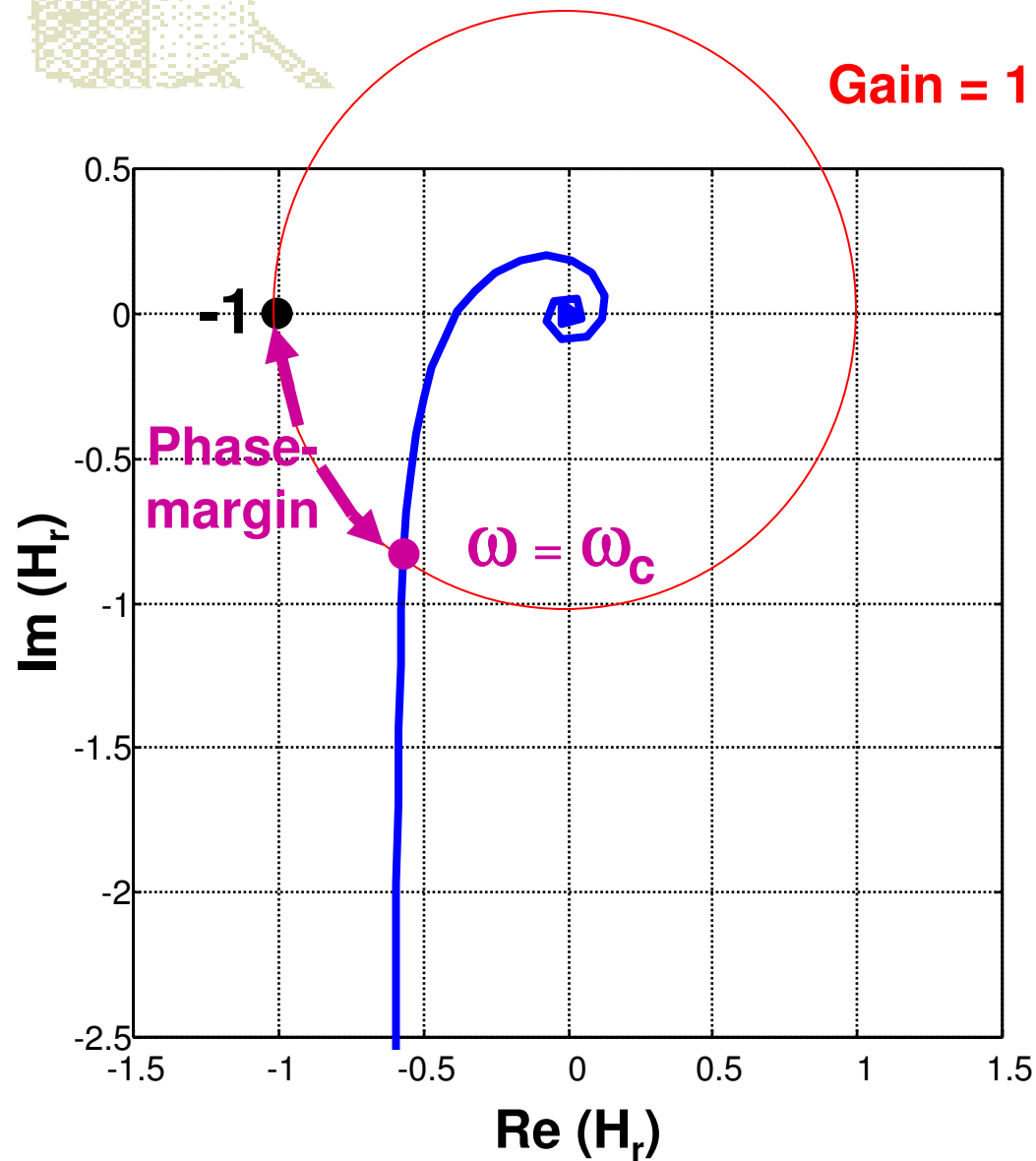
$$\omega_c = 3 \text{ rad/s}$$

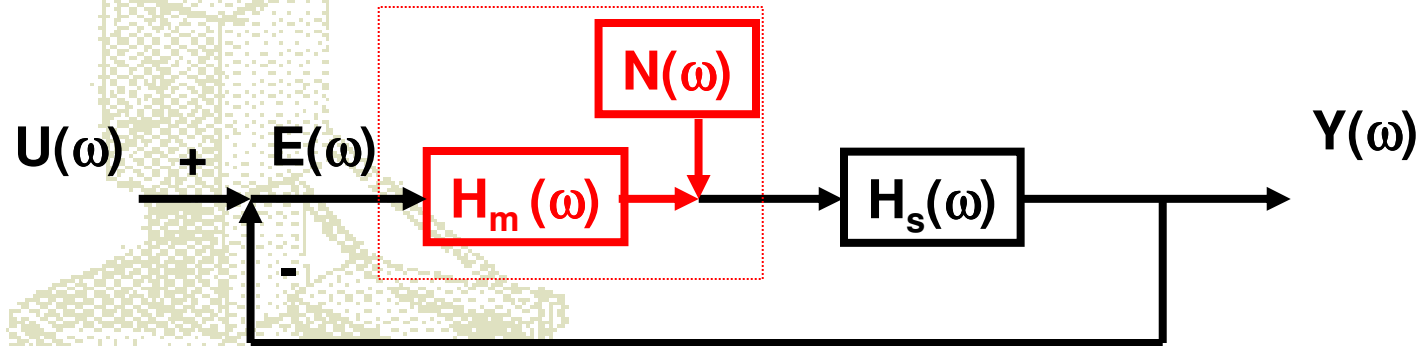
Bode-plot arg H_r



BM^M

$$H_r(\omega) = H_m(\omega) \cdot H_s(\omega) = \omega_c / j(\omega) \cdot e^{-j\omega\tau_e}$$





Human tries to:

$$H_m(\omega) \cdot H_s(\omega) = \frac{\omega_c}{j\omega} e^{-j\omega\tau_e}$$

Human is able to:

$$H_m(\omega) = K_m \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} \cdot e^{-j\omega\tau_e}$$



Examples of adaptation

$$H_m(\omega) \cdot H_s(\omega) = \frac{\omega_c}{j\omega} \cdot e^{-j\omega\tau} \rightarrow H_m(\omega) = \frac{\omega_c}{j\omega} \cdot \frac{1}{H_s(\omega)} \cdot e^{-j\omega\tau}$$

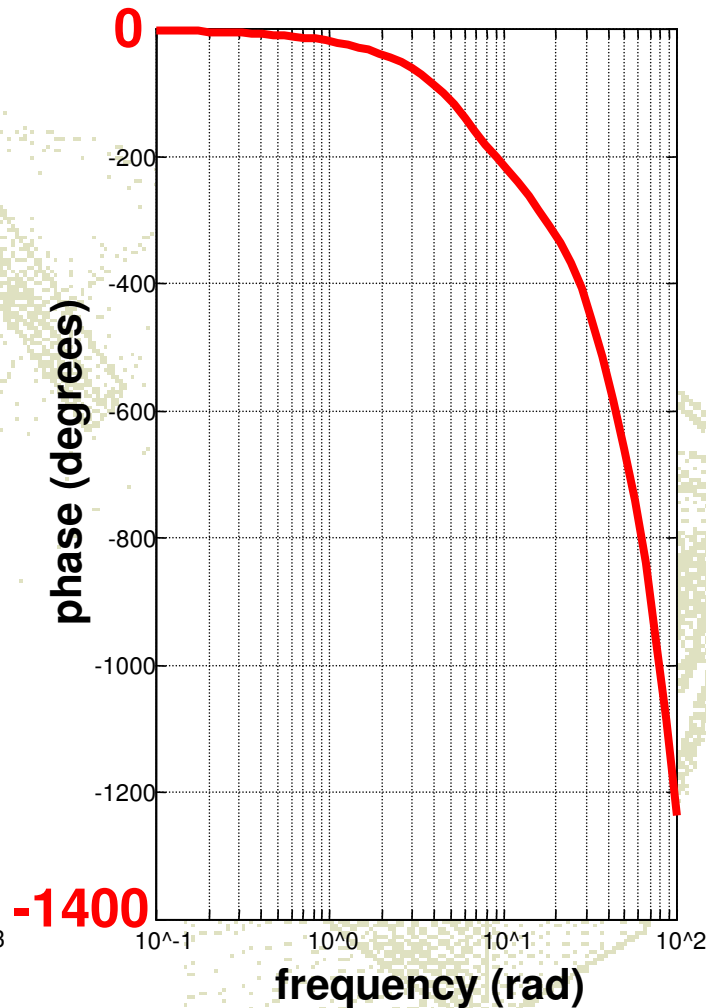
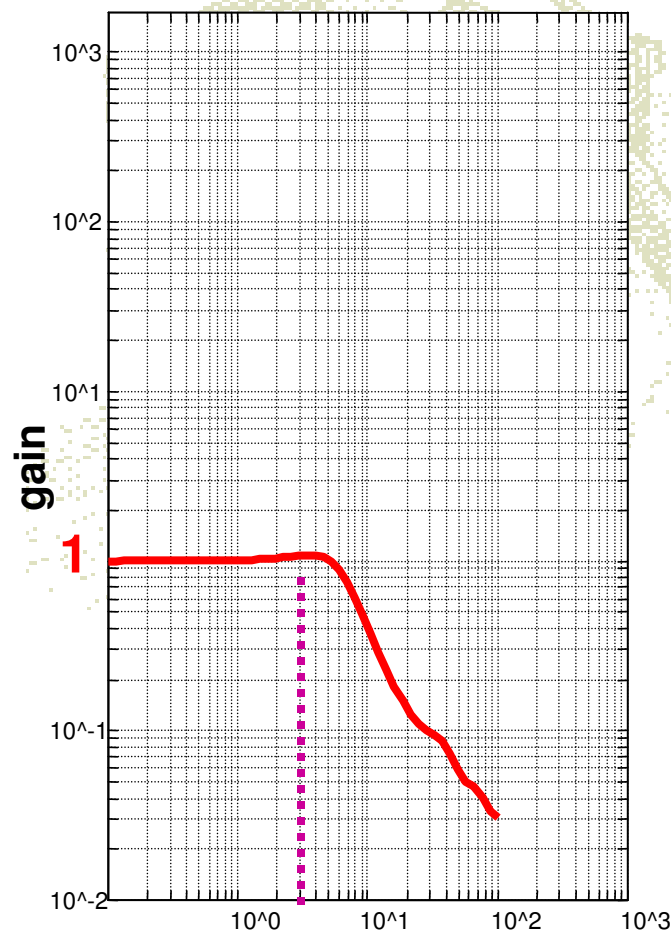
$$H_m(\omega) = K_m \cdot \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} \cdot e^{-j\omega\tau_e}$$

- $H_s(\omega) = K_s \rightarrow K_m \cdot \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} = \frac{\omega_c}{j\omega} \cdot \frac{1}{K_s} \rightarrow \tau_2 \gg 1, \tau_1 = 0, K_m = \frac{\omega_c \cdot \tau_2}{K_s}$
- $H_s(\omega) = \frac{K_s}{j\omega} \rightarrow K_m \cdot \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} = \frac{\omega_c}{j\omega} \cdot \frac{j\omega}{K_s} \rightarrow \tau_2 = 0, \tau_1 = 0, K_m = \frac{\omega_c}{K_s}$
- $H_s(\omega) = \frac{K_s}{(j\omega)^2} \rightarrow K_m \cdot \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} = \frac{\omega_c}{j\omega} \cdot \frac{(j\omega)^2}{K_s} \rightarrow \tau_2 = 0, \tau_1 \gg 1, K_m = \frac{\omega_c}{K_s \cdot \tau_1}$
- $H_s(\omega) = \frac{K_s}{(j\omega)^3} \rightarrow K_m \cdot \frac{1 + j\omega\tau_1}{1 + j\omega\tau_2} = \frac{\omega_c}{j\omega} \cdot \frac{(j\omega)^3}{K_s} \rightarrow \text{not controllable}$



Transfer input-output

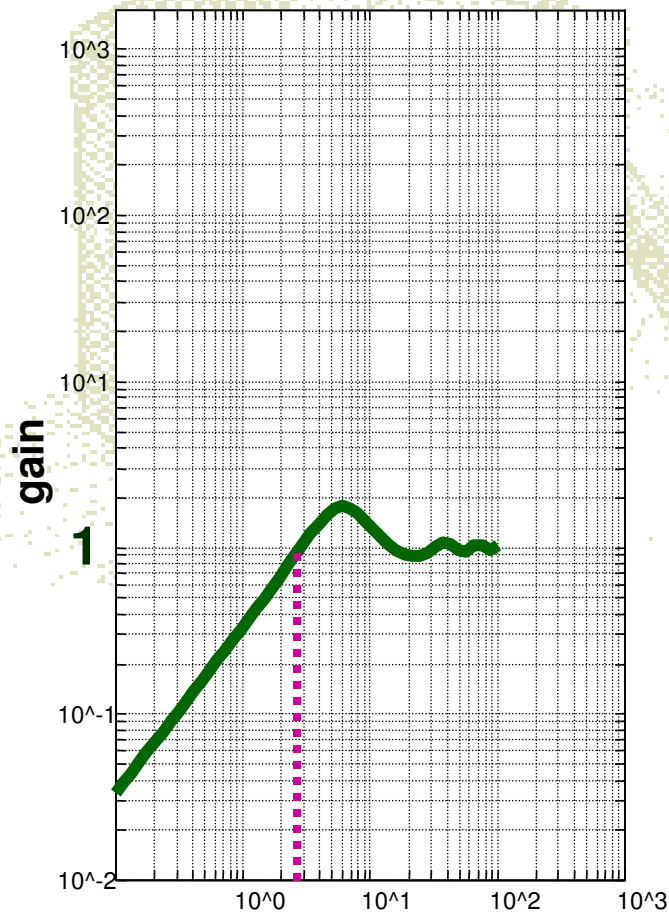
$$H_{uy}(\omega) = \frac{Y(\omega)}{U(\omega)} = \frac{\frac{\omega_c}{j\omega} e^{-j\omega\tau_e}}{1 + \frac{\omega_c}{j\omega} e^{-j\omega\tau_e}} = \frac{\omega_c e^{-j\omega\tau_e}}{j\omega + \omega_c e^{-j\omega\tau_e}}$$



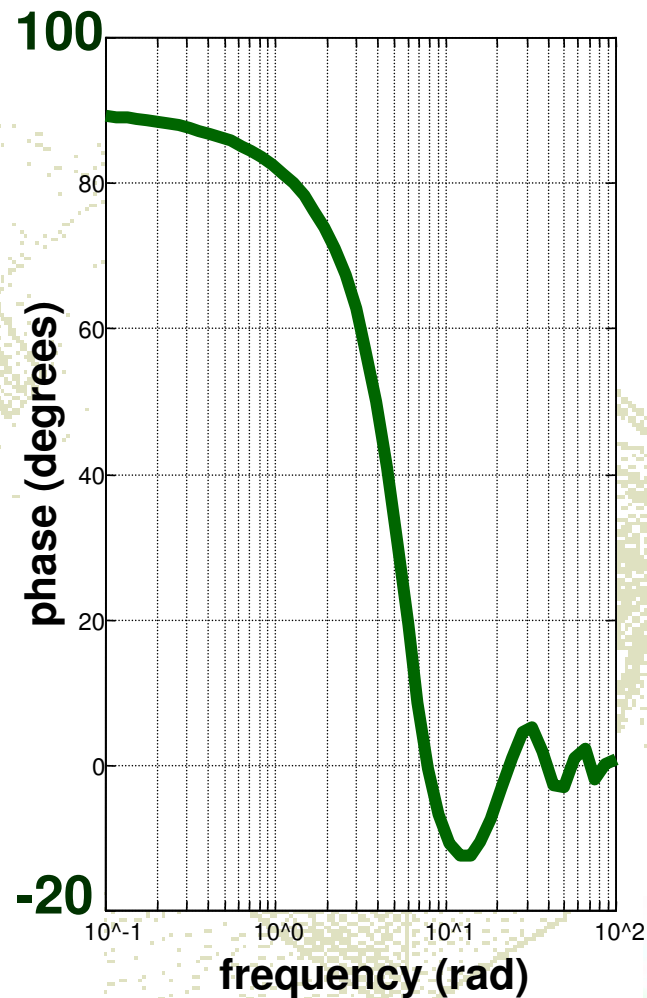
BM³

Transfer input-error

$$H_{ue}(\omega) = \frac{E(\omega)}{U(\omega)} = \frac{1}{1 + \frac{\omega_c}{j\omega} e^{-j\omega\tau_e}} = \frac{j\omega}{j\omega + \omega_c e^{-j\omega\tau_e}}$$



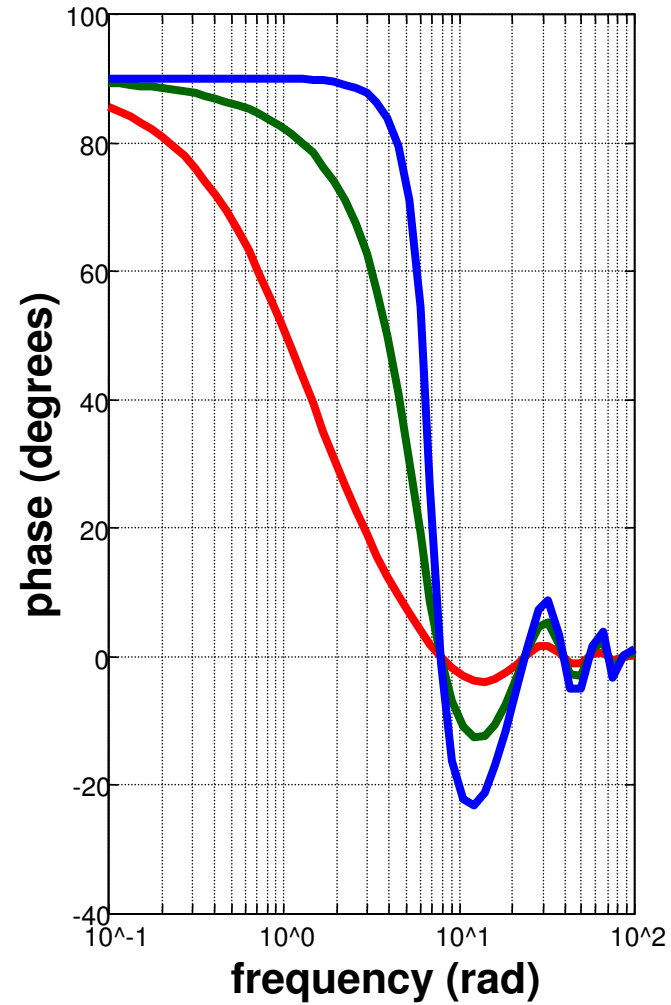
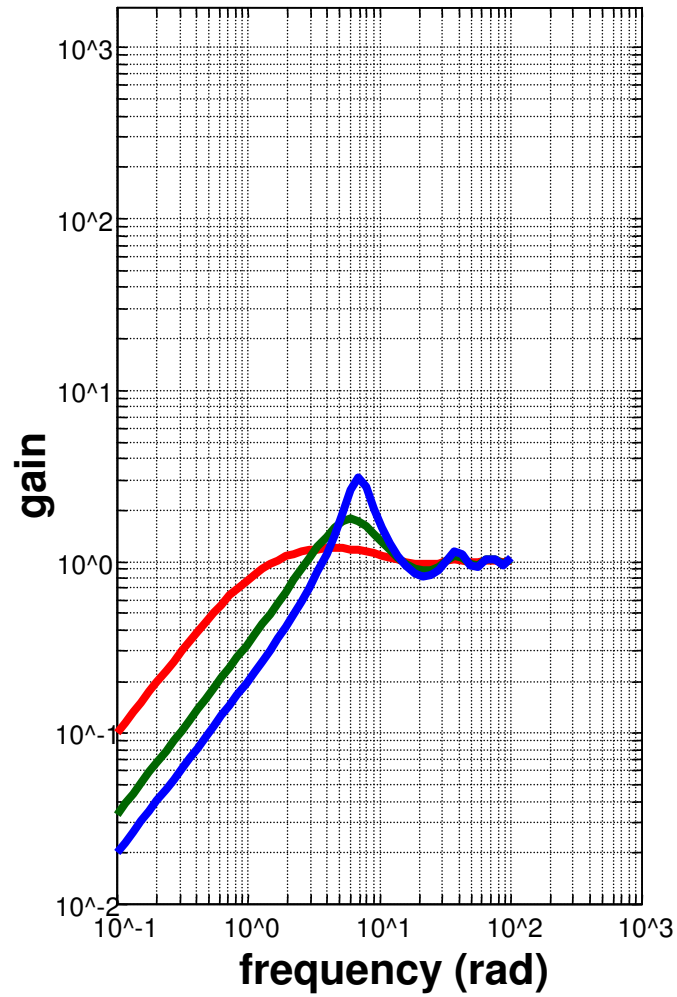
$\omega_c = 3$ rad/s



BM³

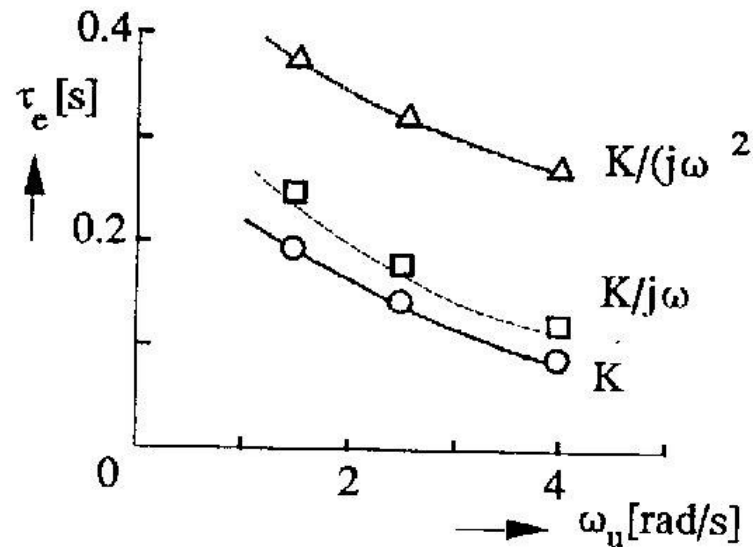
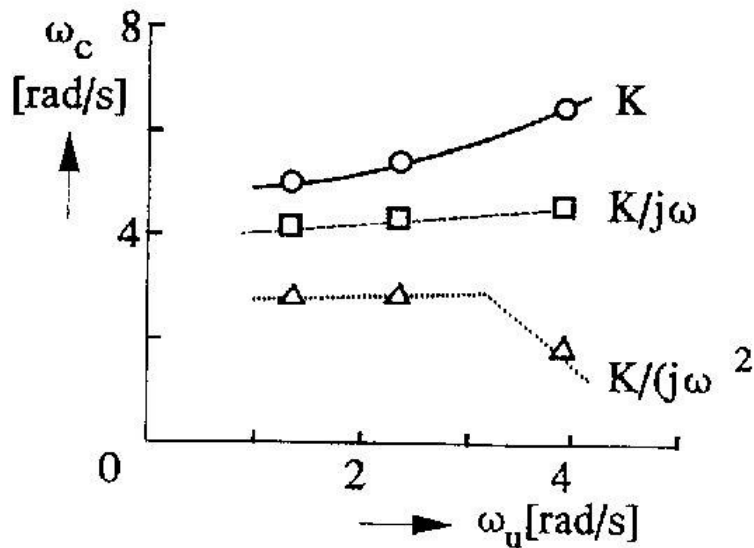
ω_c & τ_e differ
per human & situation

— $\omega_c = 1$ rad/s
— $\omega_c = 3$ rad/s
— $\omega_c = 5$ rad/s



M^W

Effect bandwidth input & order system on ω_c & τ_e



Higher bandwidth

⇒ More effort ⇒ higher ω_c and lower τ_e

Higher order system

⇒ More difficult ⇒ lower ω_c and higher τ_e



Demonstration



Conclusions

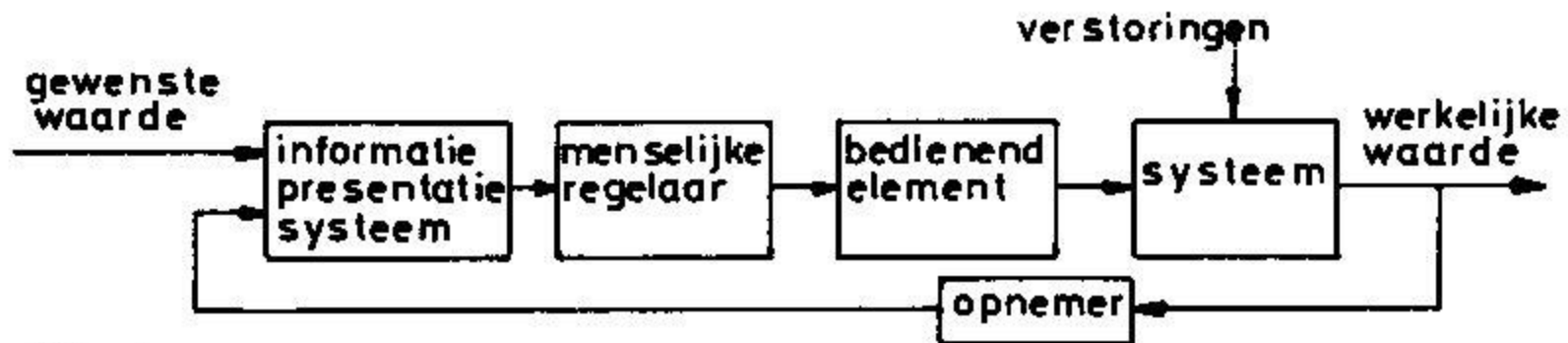
- Humans can adapt to the system to be controlled:
 - K_m , τ_1 and τ_2 : Adaptation parameters
 - ω_c : Determines bandwidth of controlled system
- Still some limitations apply:
 - Only zero, first order and second order systems can be controlled!!
 - Human controller properties known for systems with visual and vestibular feedback, not for tactile feedback, etc.
- Design of biomechatronic systems:
 - Be aware that humans must be able to control the system



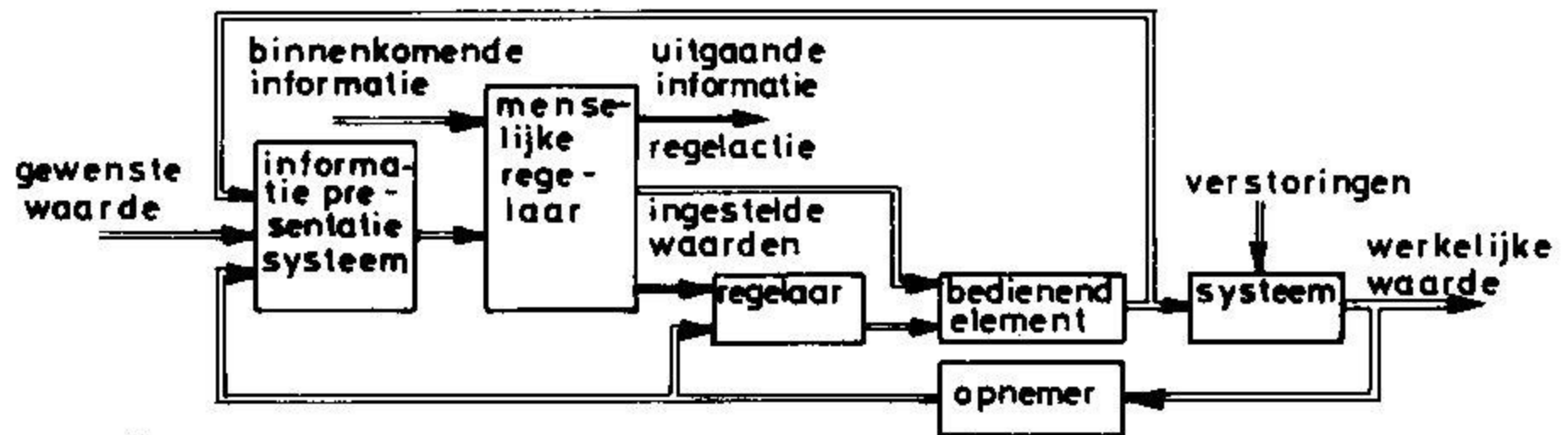
Supervisory control situations

- System with automated control loops
 - FES system with artificial sensors, controller and stimulator
 - Above-knee prosthesis with automatic knee locking
- Humans should be in control of whole system
 - Monitoring:
 - Feedback of result
 - Feedback of performance controller
 - Actions:
 - Setpoint generation for controller
 - Overruling of controller



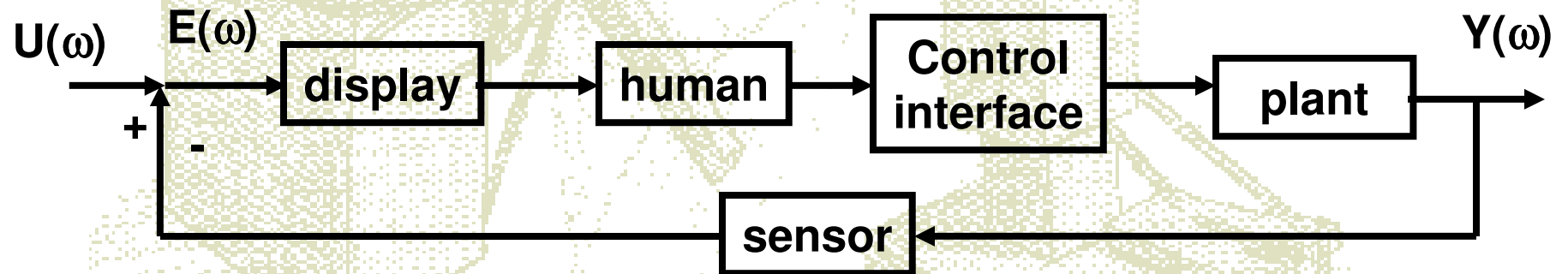


(a) handregeling

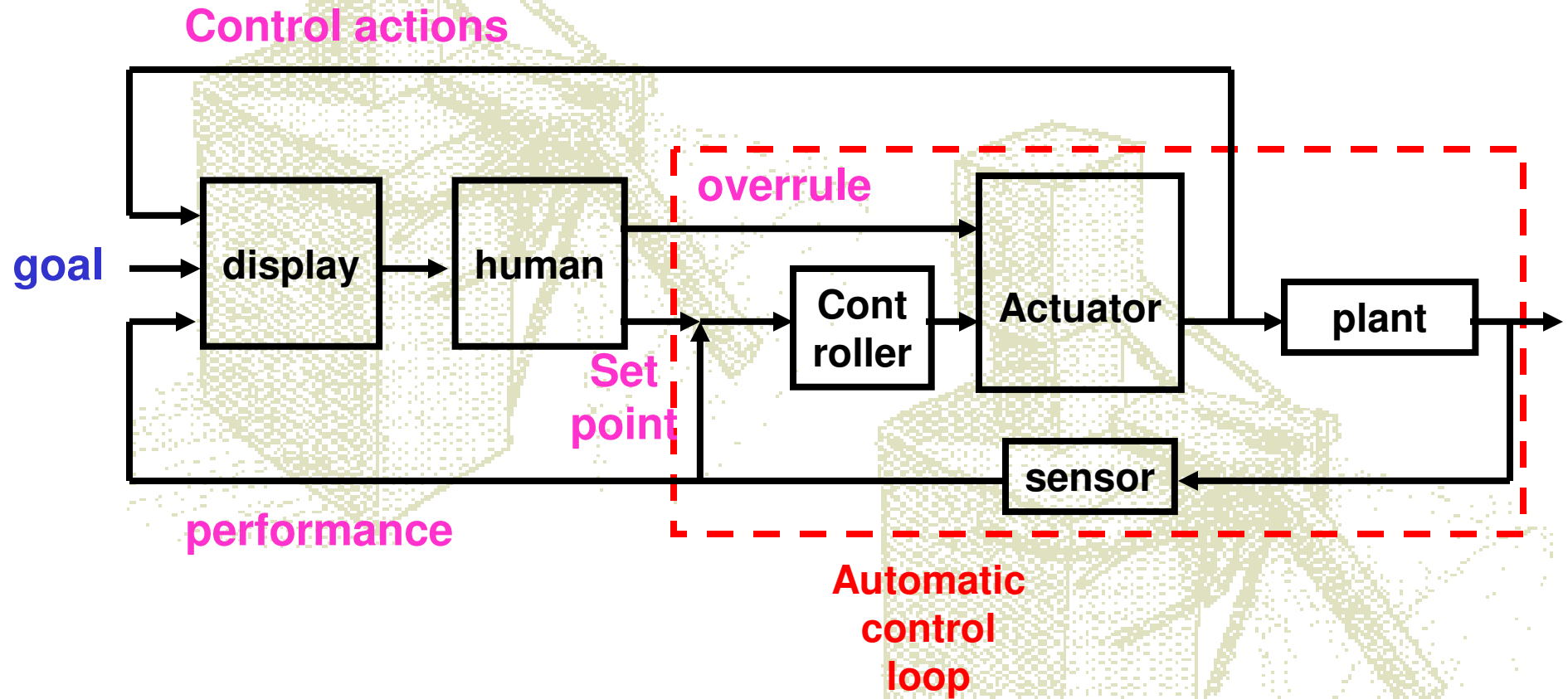


(b) supervisieregeling

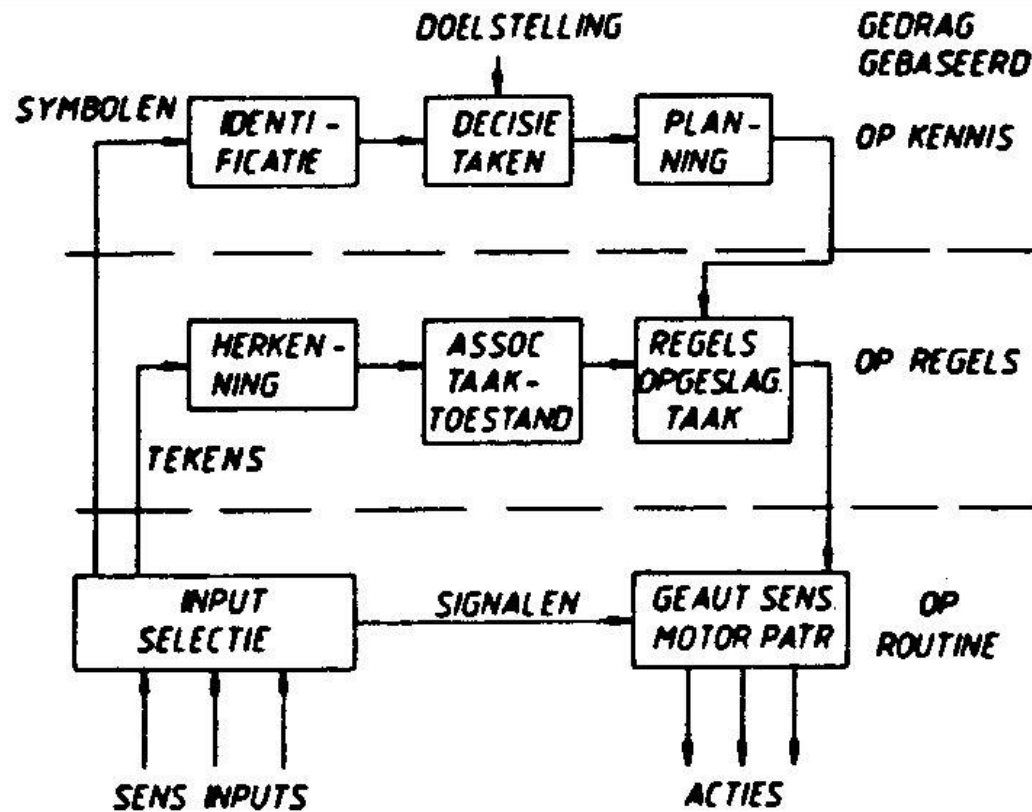
Manual control



Supervisory control



Model Rasmussen



Knowledge-based

Rule-based

Skill-based

BM^M

Model Rasmussen

- Knowledge-based behaviour:
 - Difficult tasks
 - performance based on reasoning
 - Requires much attention: High mental loading
 - Examples: control room, FES walking?
- Rule-based behaviour:
 - Tasks with intermediate difficulty
 - Performance based on applying standard rules
 - Examples: Control of helping robots
- Skill-based behaviour:
 - Easy tasks, incorporated in normal behaviour
 - Performance based on well-trained skills
 - Requires little mental effort
 - Examples: Body-powered prosthesis, Bladder control, Cochlear implants



Model Rasmussen

- Decrease mental load: From knowledge-based behaviour to skill-based behaviour
- Humans generate internal model of system
- 'Ecological' interface displays system output resembling internal model
- 'Ecological' interfaces allow for an intuitive control

