Hydrology of catchments, rivers and deltas (CIE5450)

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Lecture 'Flood routing'







FLOOD PROPAGATION

- Reservoir routing
- Flood routing in natural channels

Reservoir routing



Reservoir routing



$$\frac{dS}{dt} = I - Q + A \cdot (P - E)$$

$$S_1 = S_0 + (I - Q + A(P-E)) * (t_1-t_0)$$

$$A = A(H) \qquad A = A_{o} + a(H-H_{o})^{b}$$

$$S = \int_{H_{o}}^{H} AdH \qquad A = A_{o} \exp(b(H-H_{o}))$$

$$Q = K(H-H_{c})^{c}$$

Short term model, Flood routing: **Neglect P-E**

Predictor-Corrector:

1. Initial condition: $H_0 = H_c$

- 2. Predictor: $S_1^* = S_0 + (I Q(H_0))\Delta t$
- 3. $H_1^* = H(S_1^*)$ -> $Q^* = K\left(\frac{H_1^* + H_0}{2} H_c\right)$ 4. Corrector: $S_1 = S_0 + (I Q^*)\Delta t$
- 5. $H_1 = H(S_1)$
- 6. Possible iteration
- 7. Next time step

Reservoir routing

When at t=0 water level is at the spillway crest:



Surfaces are equal

What happens when water level is NOT at the spillway crest ?

Long term model, Reservoir yield analysis:

$$S_1 = S_0 + (I - Q + A(P-E)) * (t_1 - t_0)$$

Q is draft (regulated) and flood discharge (unregulated) Main questions:

What is the safe yield?

Reservoir routing – yield analysis



FRC = Flood Rule CurveURC = Utility Rule CurveDSC = Dead Storage Curve

Reservoir routing – yield analysis

$$S_1 = S_0 + (I - Q + A(P-E)) * (t_1-t_0)$$

Use operating rules:

- 1. Assume Q=D
- 2. Apply water balance with $A(H_0)$
- 3. Check rule curves
- 4. Redo water balance, if rule curves apply
- 5. Next time step





So here there is no unequivocal relation between Q and S

Muskingum equation: S = K[x I+(1-x)Q]

Because dS/dt = I-Q: $I - Q = \frac{dS}{dI} = \kappa \left[x \frac{dI}{dI} + (1 - x) \frac{dI}{dI} \right]$

$$I - Q = \frac{dS}{dt} = K \left[x \frac{dI}{dt} + (1 - x) \frac{dQ}{dt} \right]$$

If I = Q, then:

$$x = \frac{\frac{dQ}{dt}}{\frac{dQ}{dt} - \frac{dI}{dt}}$$

Muskingum-Cunge equations:

$$K = \frac{\Delta x}{c}$$

$$C = \frac{\mathrm{d}\,q}{\mathrm{d}\,h} \approx 1.67\overline{v}$$

$$x = 0.5 \left(1 - \frac{q}{S_b c \Delta x}\right) \approx 0.5 \left(1 - 0.6 \frac{h}{S_b \Delta x}\right)$$

Conditions:

Courant number

$$C = \frac{c\Delta t}{\Delta x} = \frac{\Delta t}{K} \le 1$$

Physical boundaries of x

$$0 \le x \le 0.5$$



Muskingum routing equation:

 $Q_2 = C_0 I_2 + C_1 I_1 + C_2 Q_1$

 $c_0 = -\frac{Kx - 0.5\Delta t}{K - Kx + 0.5\Delta t}$

$$c_1 = \frac{Kx + 0.5\Delta t}{K - Kx + 0.5\Delta t}$$

$$c_2 = \frac{K - Kx - 0.5\Delta t}{K - Kx + 0.5\Delta t}$$

$$C_0 + C_1 + C_2 = 1$$

Date	Hour	I, m³/s	C ₀ I ₂	c ₁ I ₁	c ₂ O ₁	O, m ³ /s
4/9	6 a.m.	1000				1000
	Noon	2400	-408	530	640	762
	6 p.m.	3900	-663	1272	488	1097
	Midnight	5000	-850	2067	702	1919
4/10	6 a.m.	4900	-833	2650	1228	3045
	Noon	4000	-680	2597	1949	3866

 $C_0 = -0.17$; $c_1 = 0.53$; $c_2 = 0.64$

Local Inflow:

Four-point method:

$$Q_2 = c_0 I_2 + c_1 I_1 + c_2 Q_1 + c_3 Q_L$$

$$c_3 = \frac{2\Delta t \,/\,K}{2(1-x) + \Delta t \,/\,K}$$

is sum of c_0 and c_1

Three parameter Muskingum method:

$$\frac{\mathrm{d}S}{\mathrm{d}t} = I(1+\alpha) - Q$$

$$S = K[x(1+\alpha)I + (1-x)Q]$$

Kinematic routing:

Continuity equation

$$\mathsf{Q} = \mathsf{I} - \mathsf{L} \frac{\Delta \mathsf{A}}{\Delta \mathsf{t}}$$

Manning equation

 $Q = KAR^{2/3}S^{1/2}$