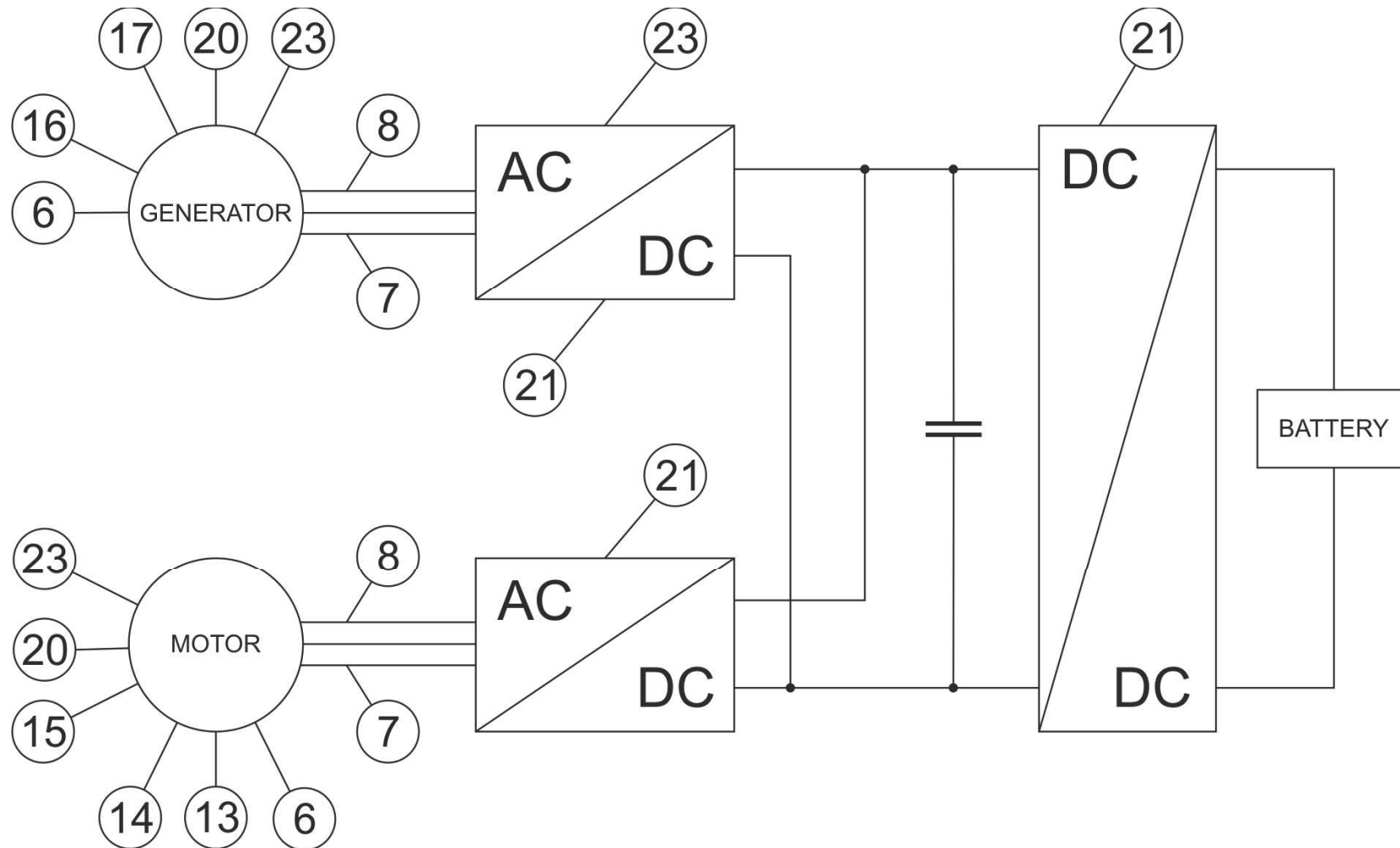


Elektrische Aandrijvingen

WTB

Lokatie/evenement

P.BAUER



Fundamental Elements of Power Electronics

Figure 21.1 Potential level method of representing voltages.

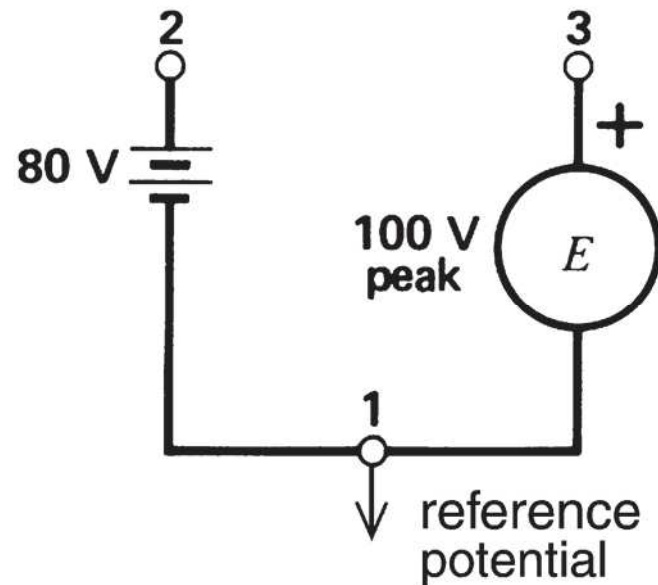


Figure 21.2 Potential levels of terminals 1, 2, and 3.

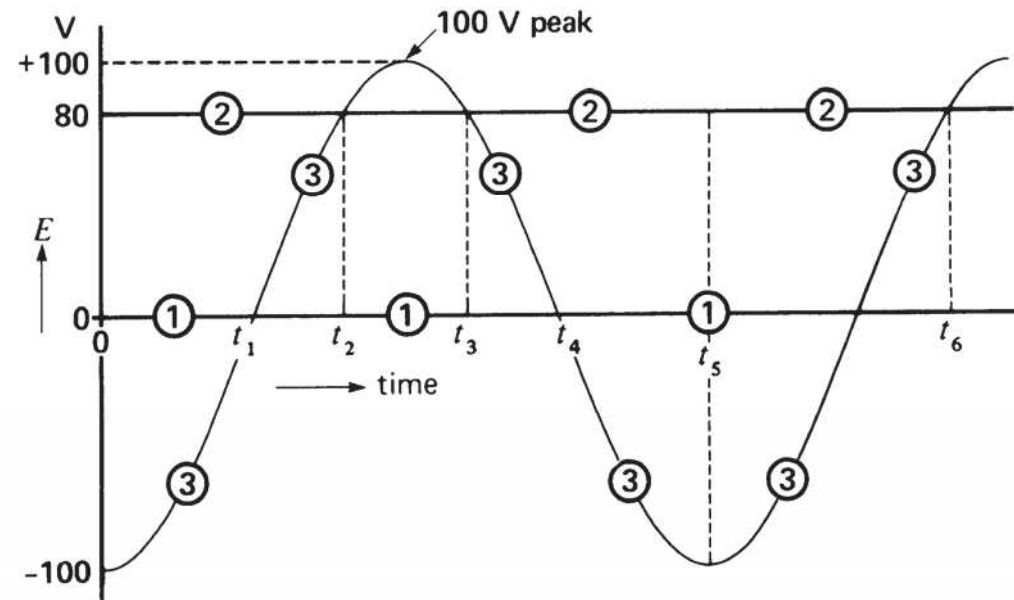


Figure 21.3 Changing the reference terminal.

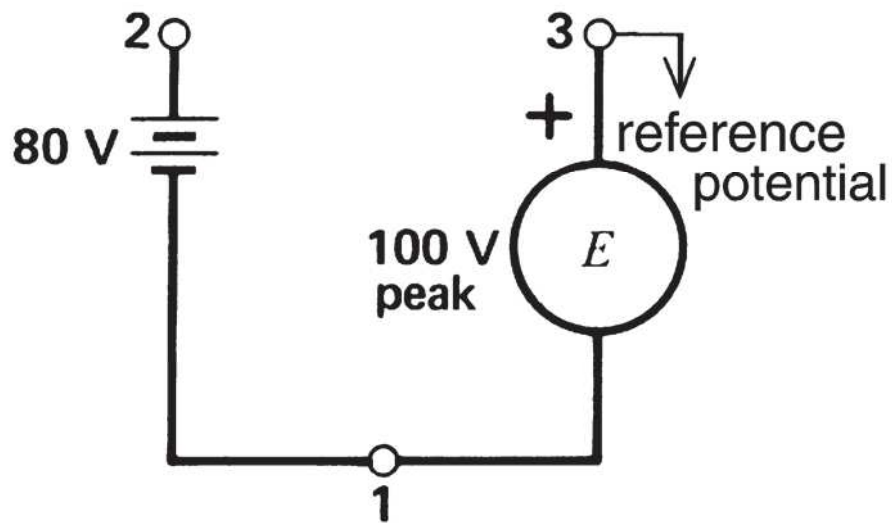
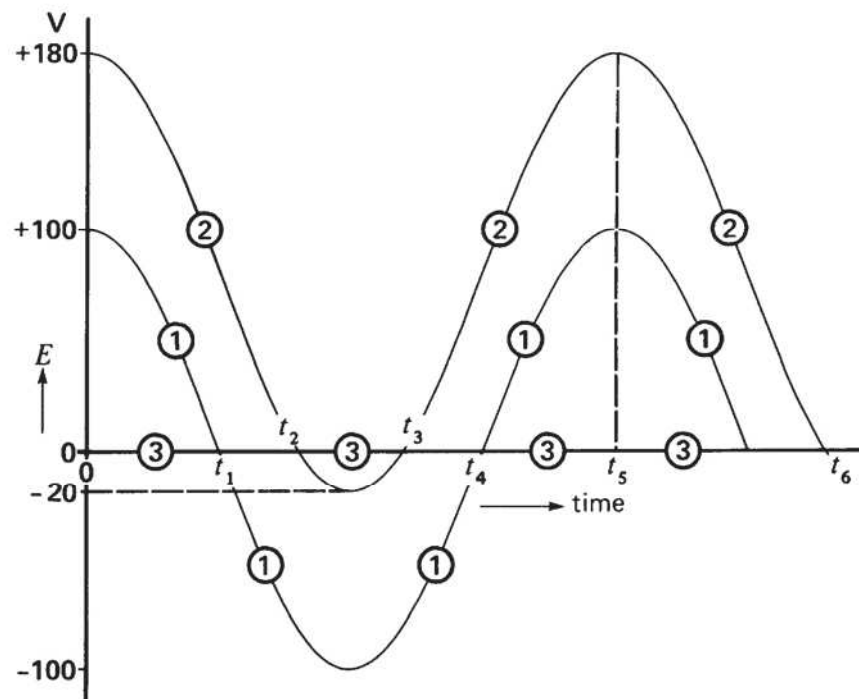


Figure 21.4 The relative potential levels are the same as in Fig. 21.2.



Voltage across some circuit elements

Figure 21.5 Potential across a switch.



Figure 21.6 Potential across a resistor.

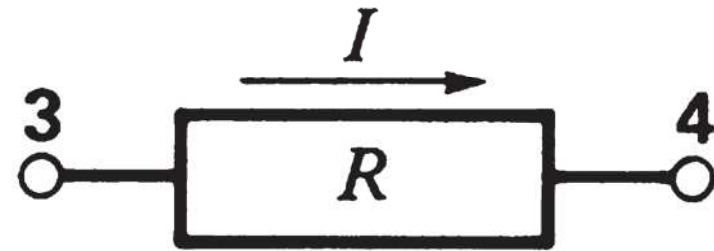


Figure 21.7 Potential across an inductor.

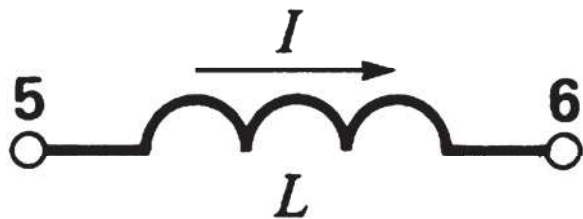
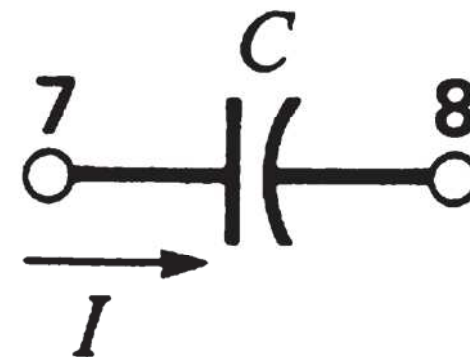


Figure 21.8 Potential across a capacitor.



Diode

Figure 21.9 Basic rules governing diode behavior.

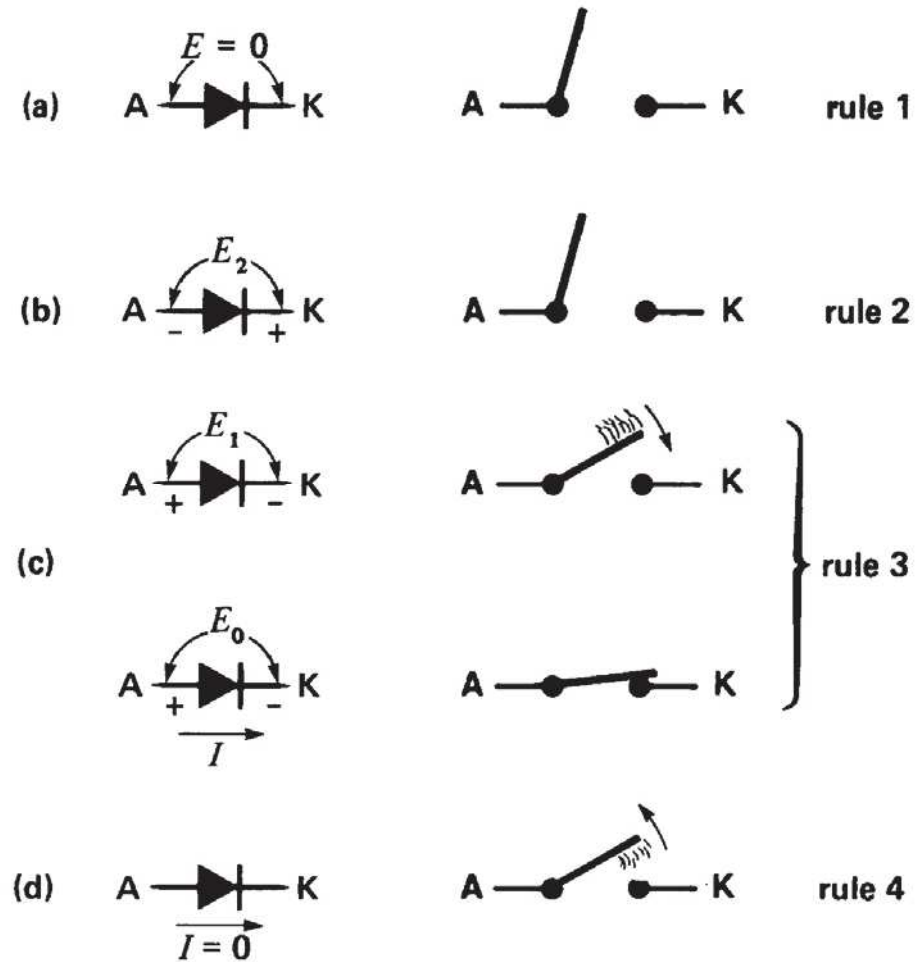


Figure 21.10 (continued) a. Average current: 4 A; PIV: 400 V; body length: 10 mm; diameter: 5.6 mm. b. Average current: 15 A; PIV: 500 V; stud type; length less thread: 25 mm; diameter: 17 mm. c. Average current: 500 A; PIV: 2000 V; length less thread: 244 mm; diameter: 40 mm. d. Average current: 2600 A; PIV: 2500 V; Hockey Puk; distance between pole-faces: 35 mm; diameter: 98 mm. (Photos courtesy of International Rectifier)



Figure 21.10 a. Average current: 4 A; PIV: 400 V; body length: 10 mm; diameter: 5.6 mm. b. Average current: 15 A; PIV: 500 V; stud type; length less thread: 25 mm; diameter: 17 mm. c. Average current: 500 A; PIV: 2000 V; length less thread: 244 mm; diameter: 40 mm. d. Average current: 2600 A; PIV: 2500 V; Hockey Puk; distance between pole-faces: 35 mm; diameter: 98 mm. (Photos courtesy of International Rectifier)



Figure 21.10 (continued) a. Average current: 4 A; PIV: 400 V; body length: 10 mm; diameter: 5.6 mm. b. Average current: 15 A; PIV: 500 V; stud type; length less thread: 25 mm; diameter: 17 mm. c. Average current: 500 A; PIV: 2000 V; length less thread: 244 mm; diameter: 40 mm. d. Average current: 2600 A; PIV: 2500 V; Hockey Puk; distance between pole-faces: 35 mm; diameter: 98 mm. (Photos courtesy of International Rectifier)

Figure 21.10 (continued) a. Average current: 4 A; PIV: 400 V; body length: 10 mm; diameter: 5.6 mm. b. Average current: 15 A; PIV: 500 V; stud type; length less thread: 25 mm; diameter: 17 mm. c. Average current: 500 A; PIV: 2000 V; length less thread: 244 mm; diameter: 40 mm. d. Average current: 2600 A; PIV: 2500 V; Hockey Puk; distance between pole-faces: 35 mm; diameter: 98 mm. (Photos courtesy of International Rectifier)



Battery charger with resistor

Figure 21.11 a. Simple battery charger circuit. b. Corresponding voltage and current waveforms.

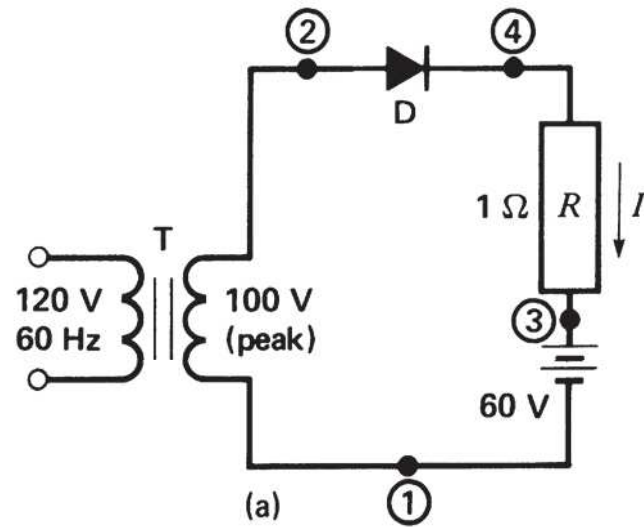
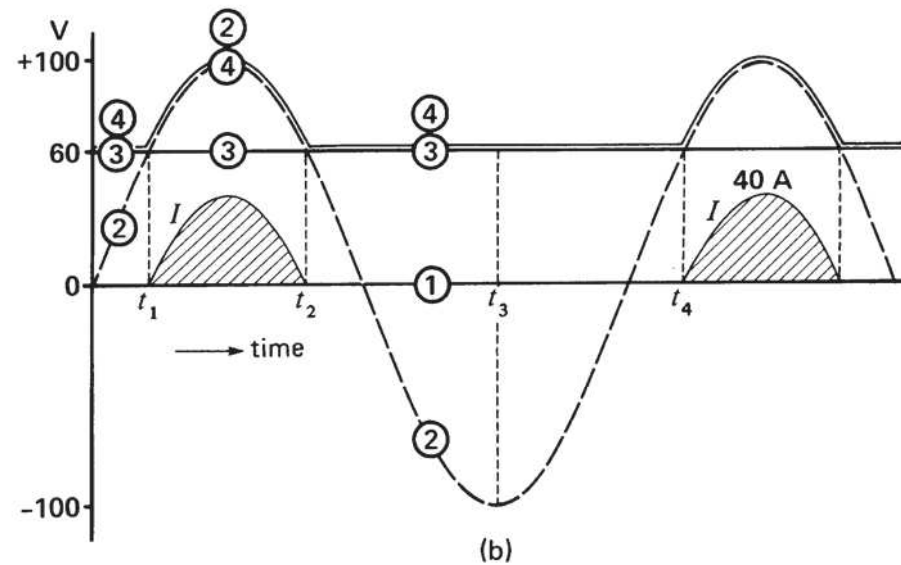


Figure 21.11 (continued) a. Simple battery charger circuit. b. Corresponding voltage and current waveforms.



Battery charger with inductor

Figure 21.12 a. Battery charger using a series inductor. b. Corresponding voltage and current waveforms.

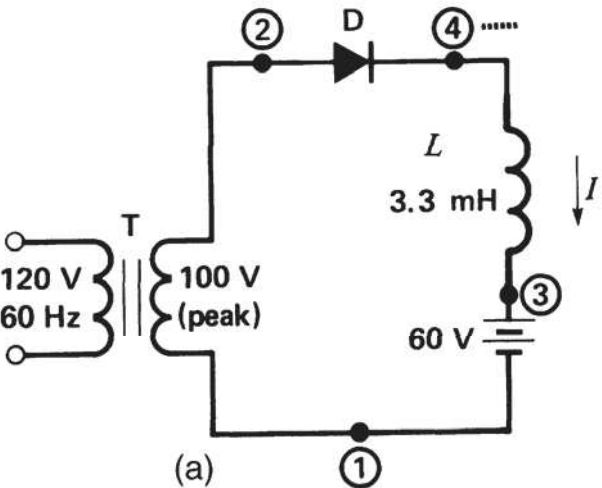
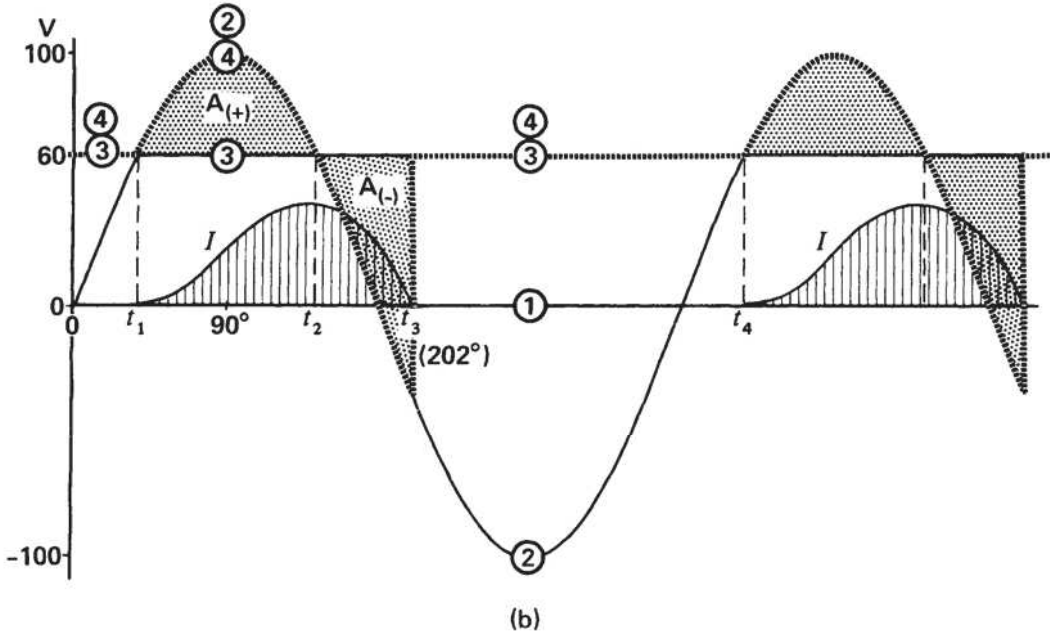
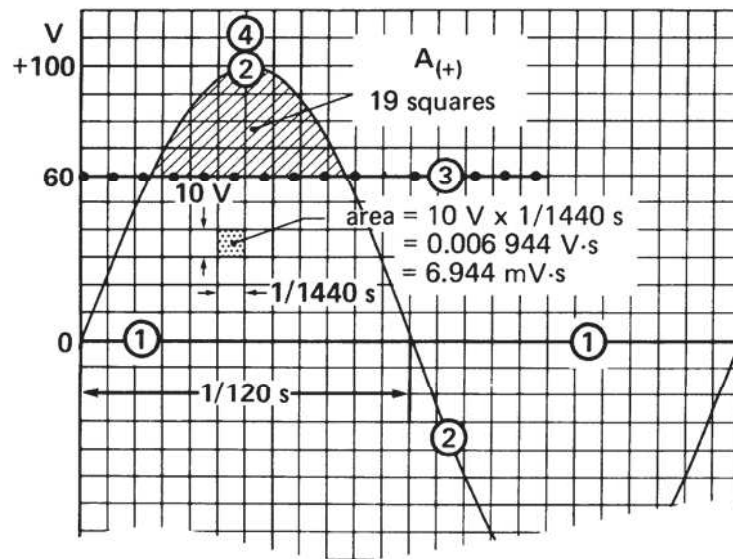


Figure 21.12 (continued) a. Battery charger using a series inductor. b. Corresponding voltage and current waveforms.



Example 21.1

Figure 21.12c See Example 21-1.



Single bridge diode rectifier

Figure 21.13a a. Single-phase bridge rectifier. b. Voltage levels.

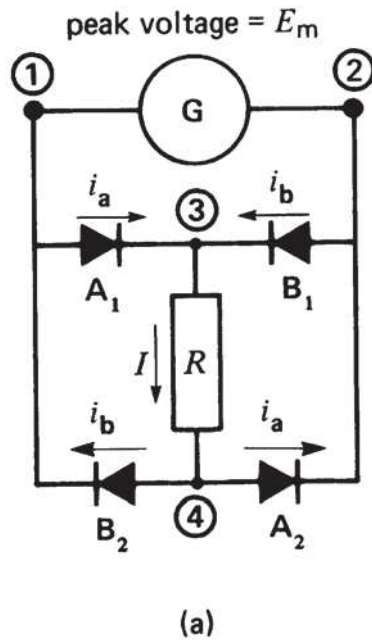


Figure 21.13b a. Single-phase bridge rectifier. b. Voltage levels.

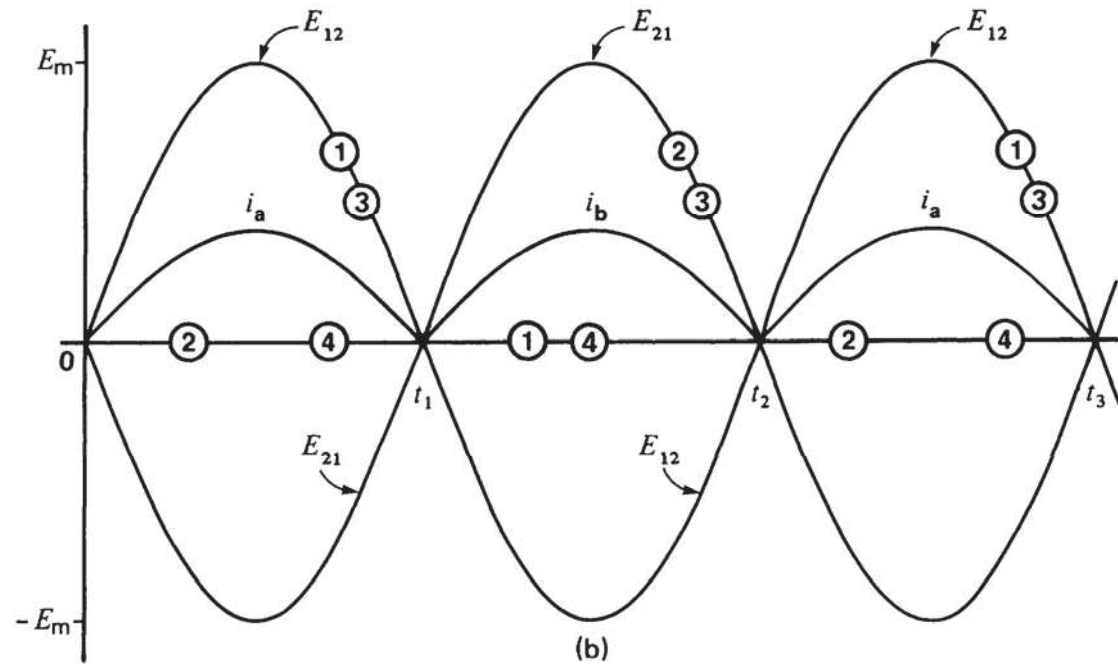


Figure 21.13c Voltage and current waveforms in load R .

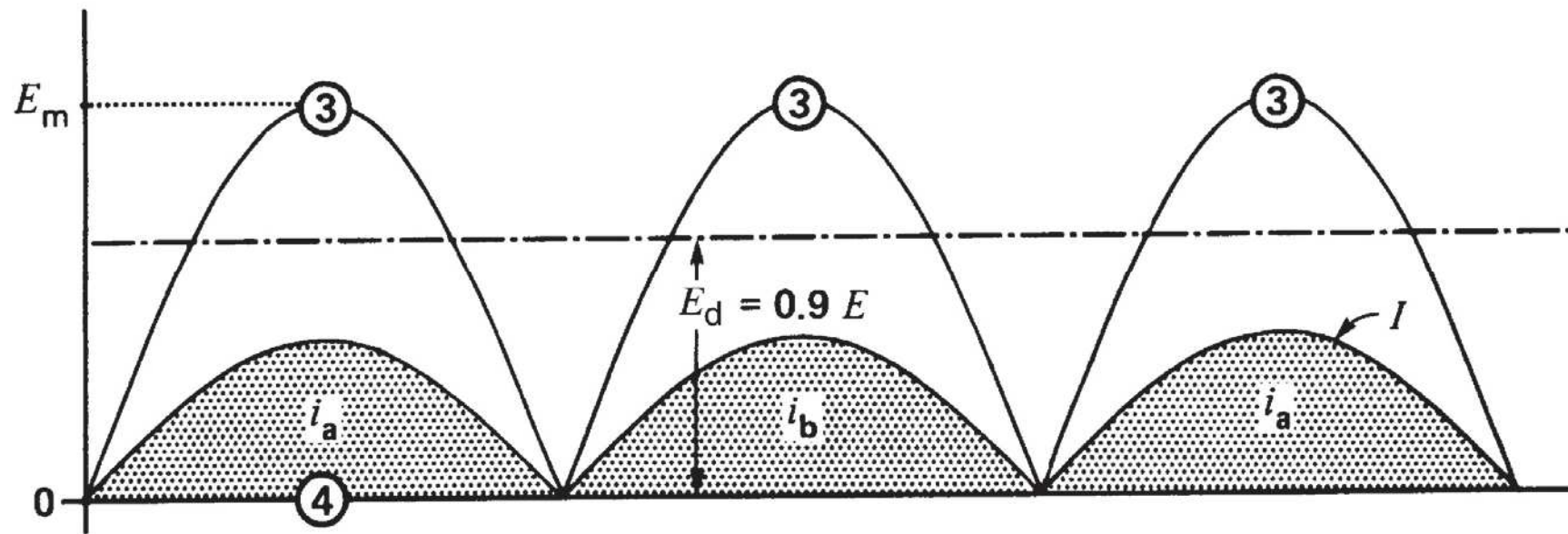


Figure 21.14 a. Rectifier with inductive filter. b. Rectifier with capacitive filter.

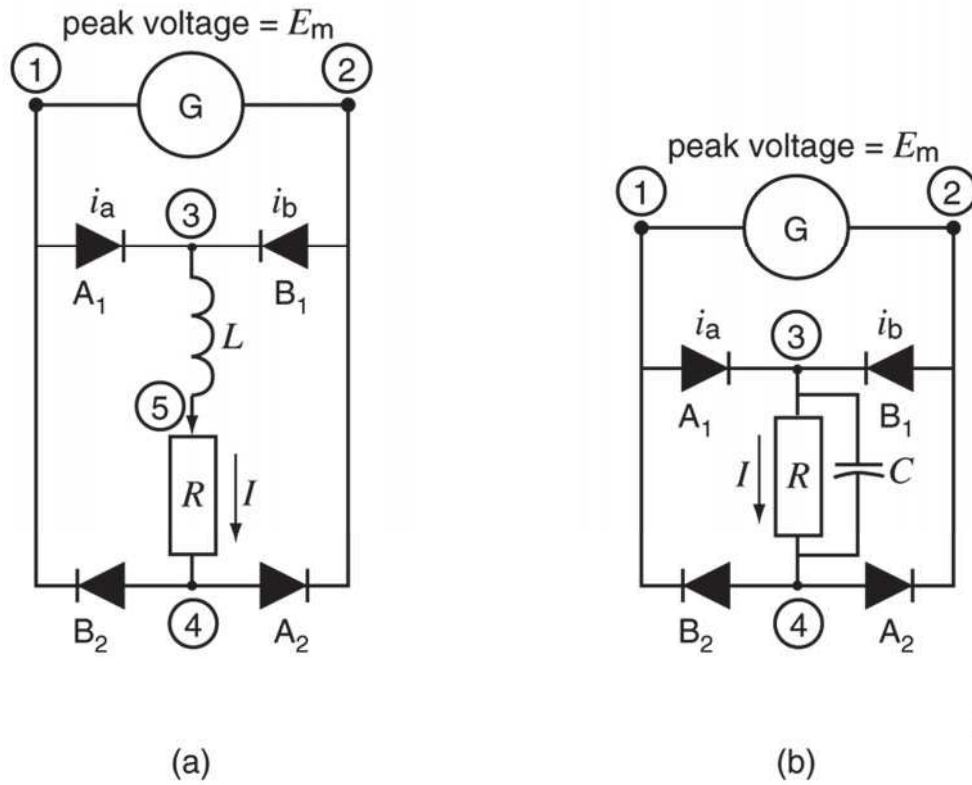


Figure 21.15 Current and voltage waveforms with inductive filter.

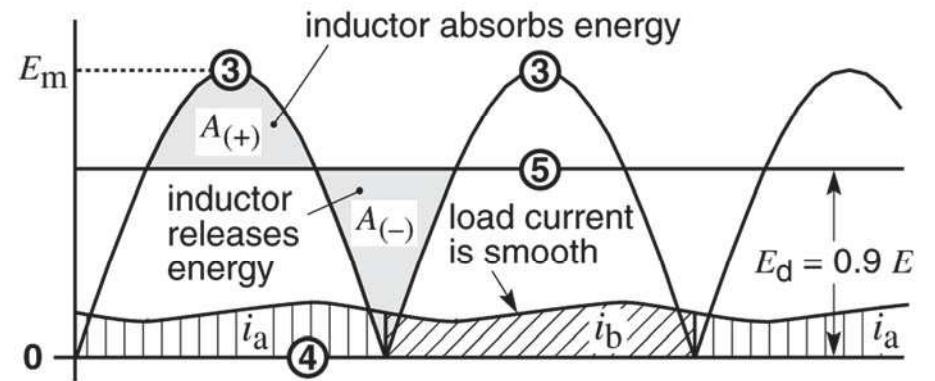
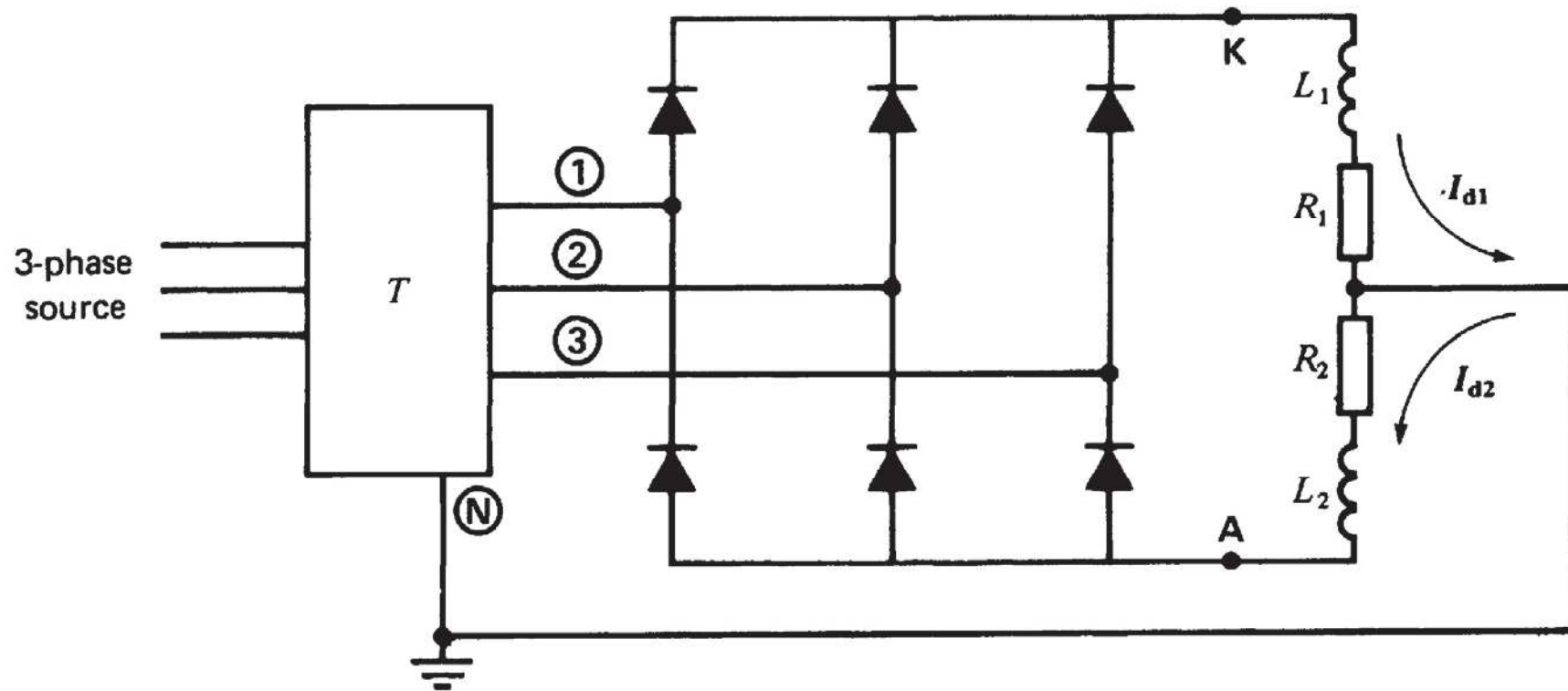


Figure 21.18 Dual 3-phase, 3-pulse rectifier.



Three-phase 6 pulse rectifier

Figure 21.20 Voltage and current waveforms in Fig. 21.19.

Figure 21.19 Three-phase, 6-pulse rectifier with inductive filter.

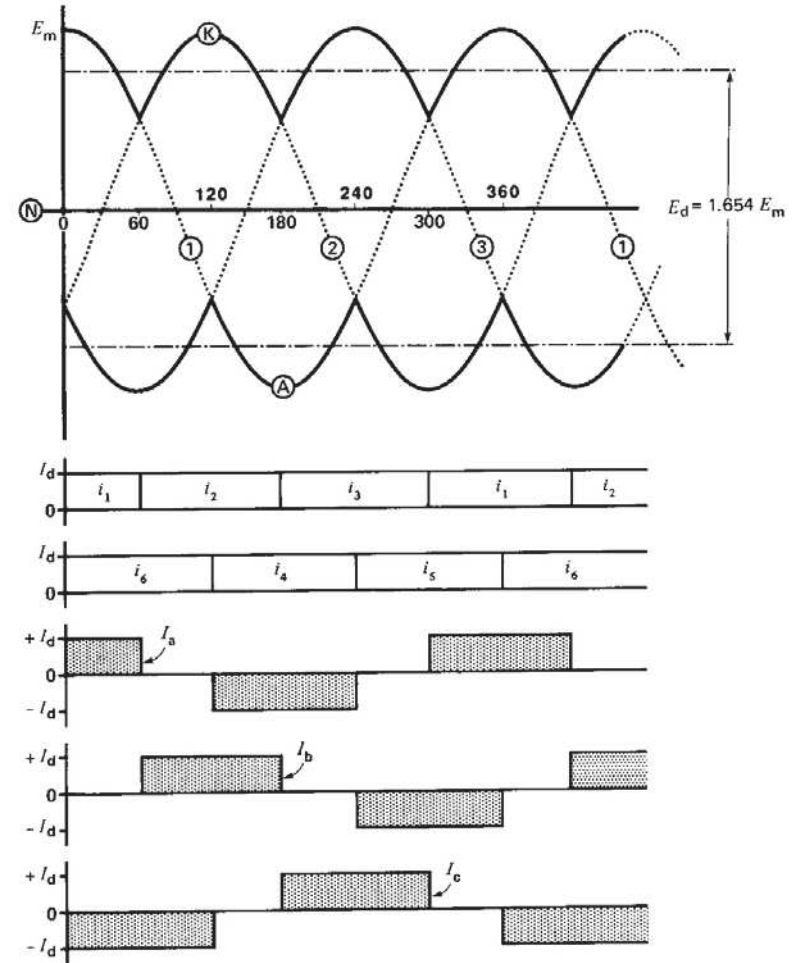
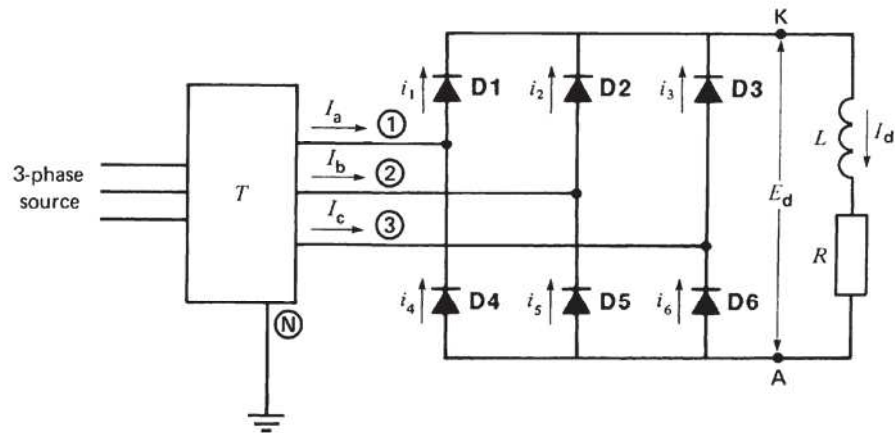


Figure 21.21 Another way of showing EKA using line voltage potentials. Note also the position of E_{2N} with respect to the line voltages.

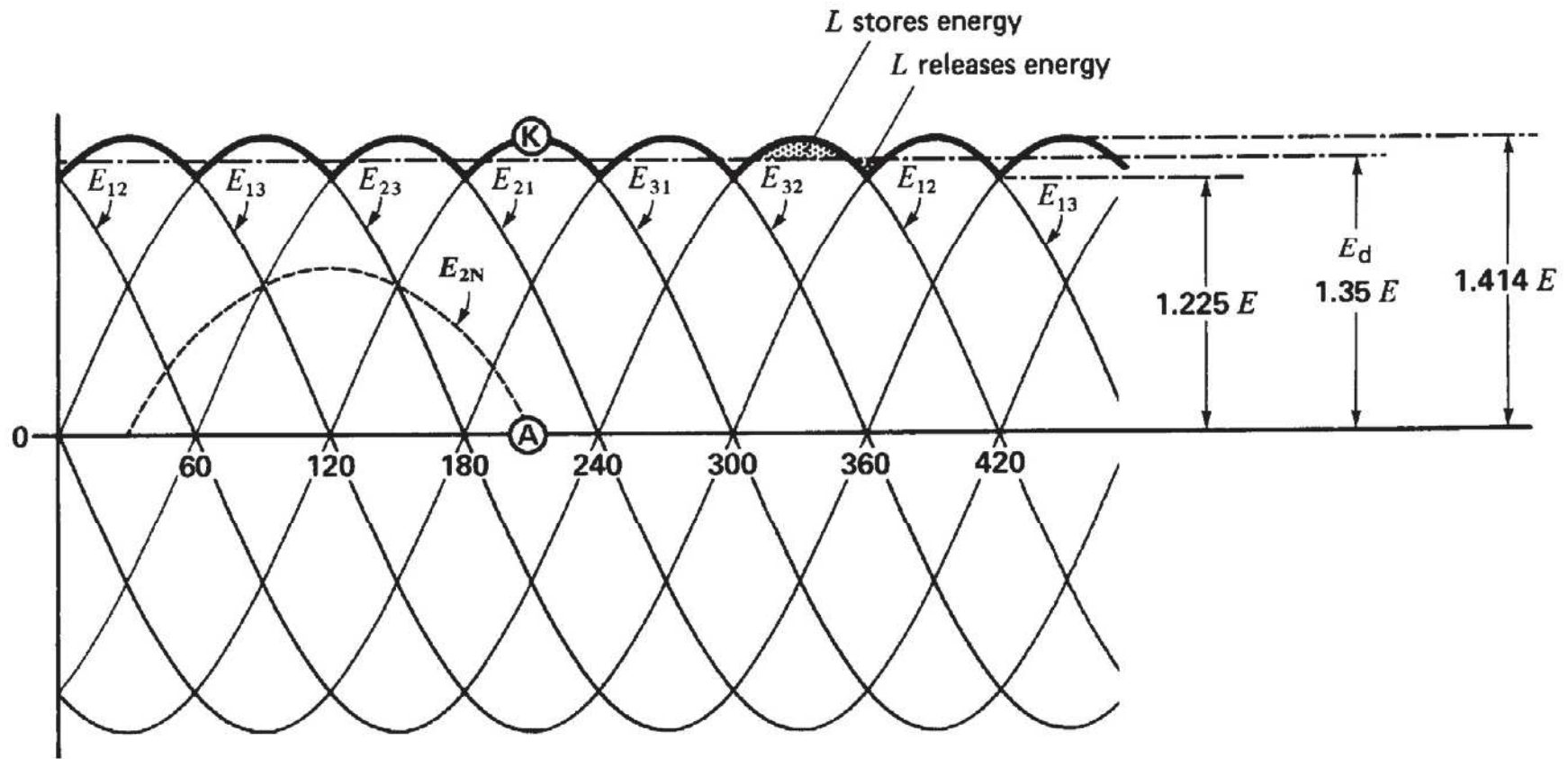
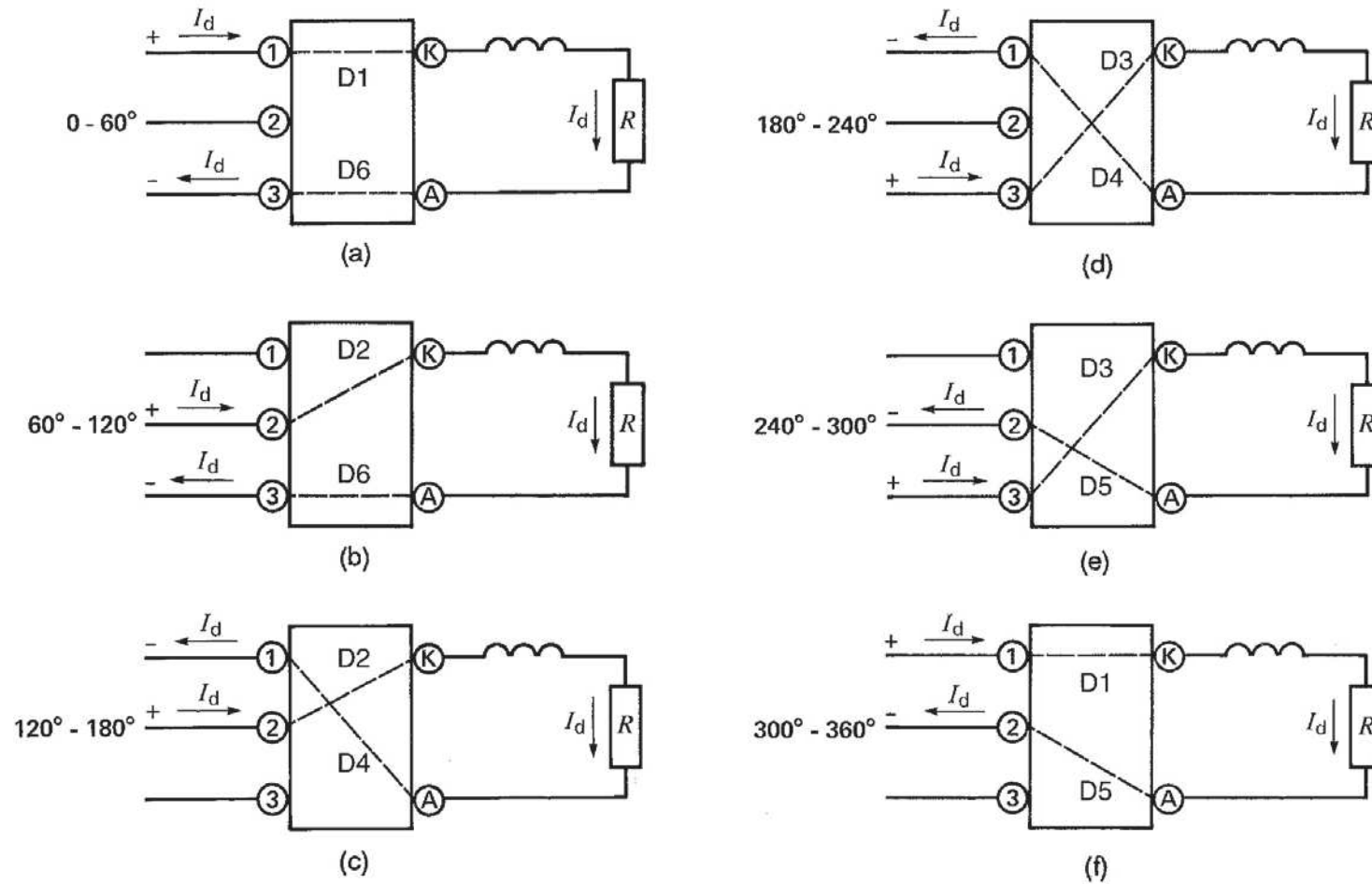
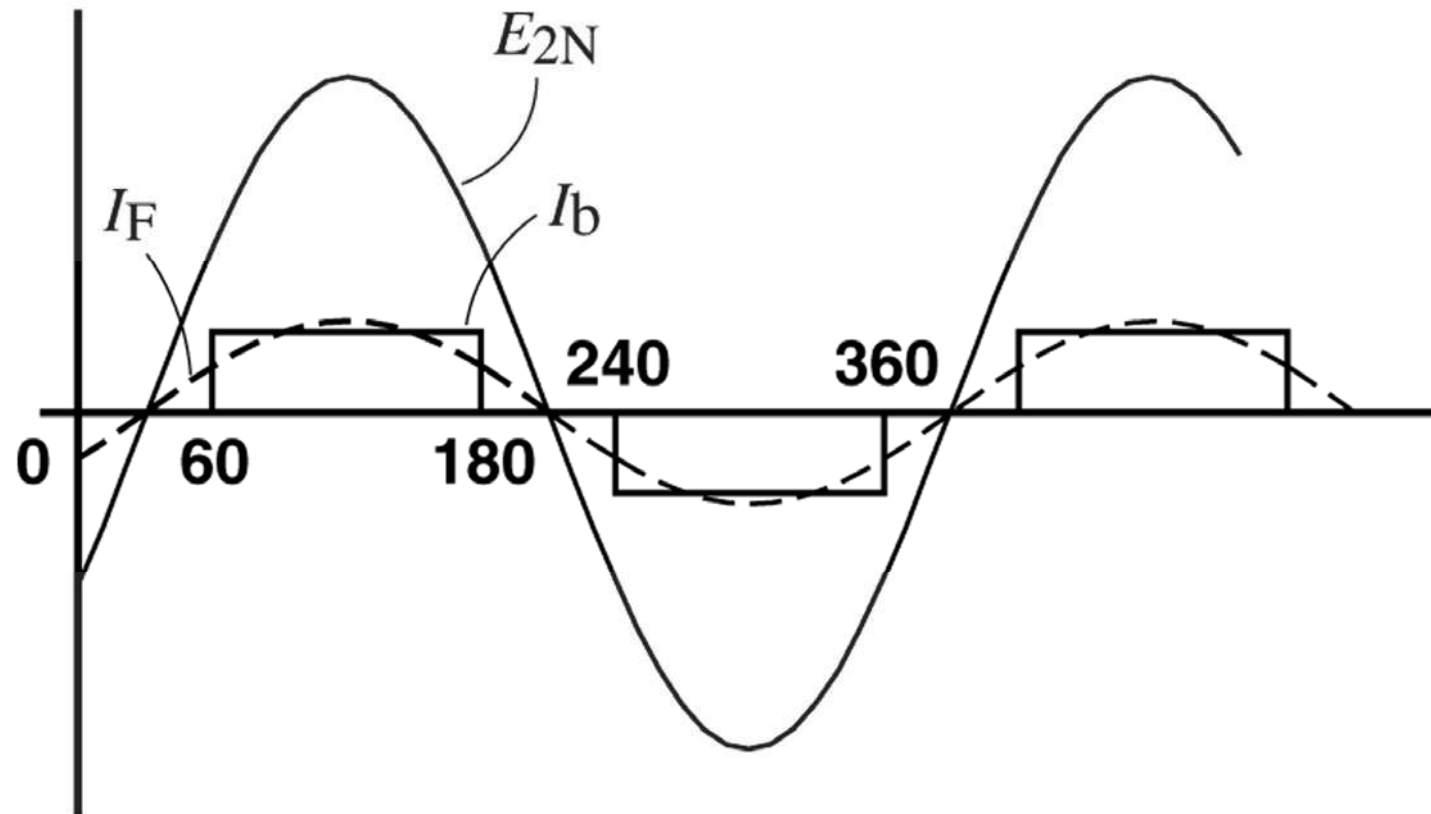


Figure 21.22 Successive diode connections between the 3-phase input and dc output terminals of a 3-phase, 6-pulse rectifier.



Effective, fundamental line current

Figure 21.23 Line-to-neutral voltage and line current in phase 2 of Fig. 21.20.



The thyristor

Figure 21.24 Symbol of a thyristor, or SCR.

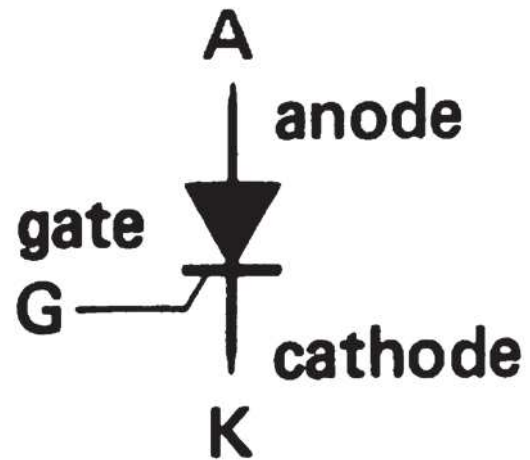
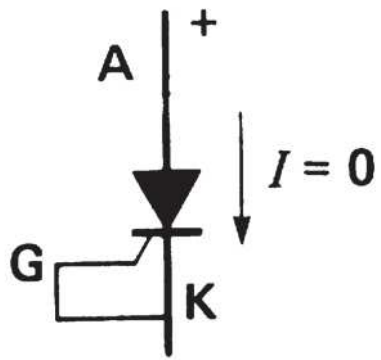
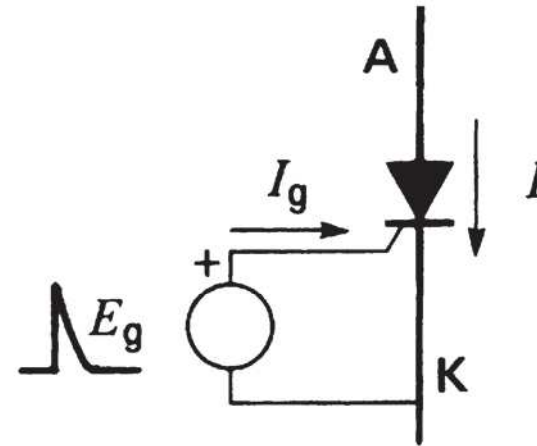


Figure 21.25 a. A thyristor does not conduct when the gate is connected to the cathode. b. A thyristor conducts when the anode is positive and a current pulse is injected into the gate.



(a)



(b)

Figure 21.26 Range of SCRs from medium to very high power capacity.

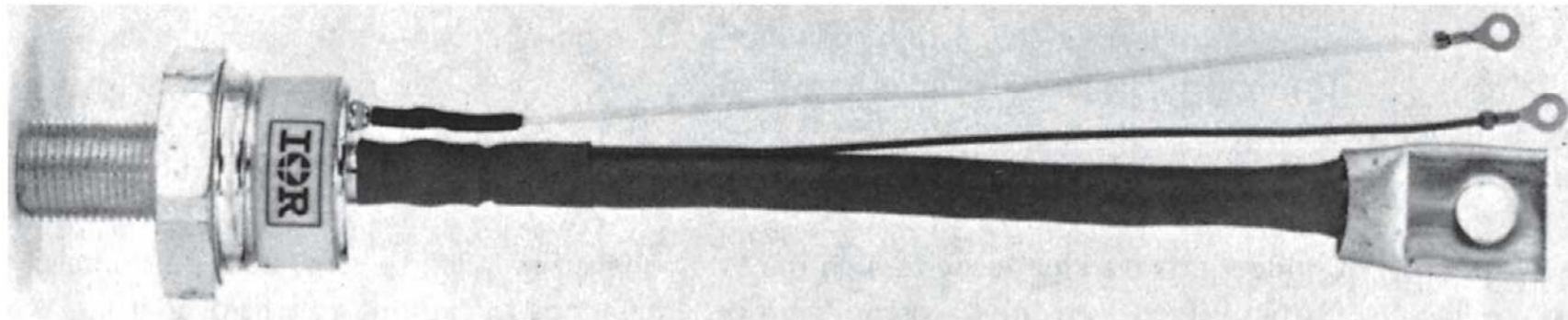
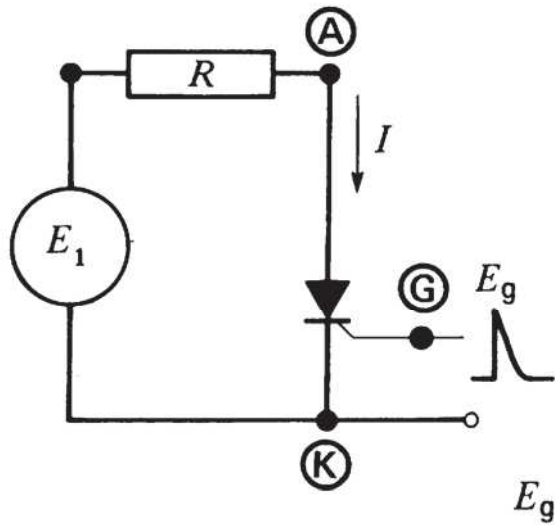
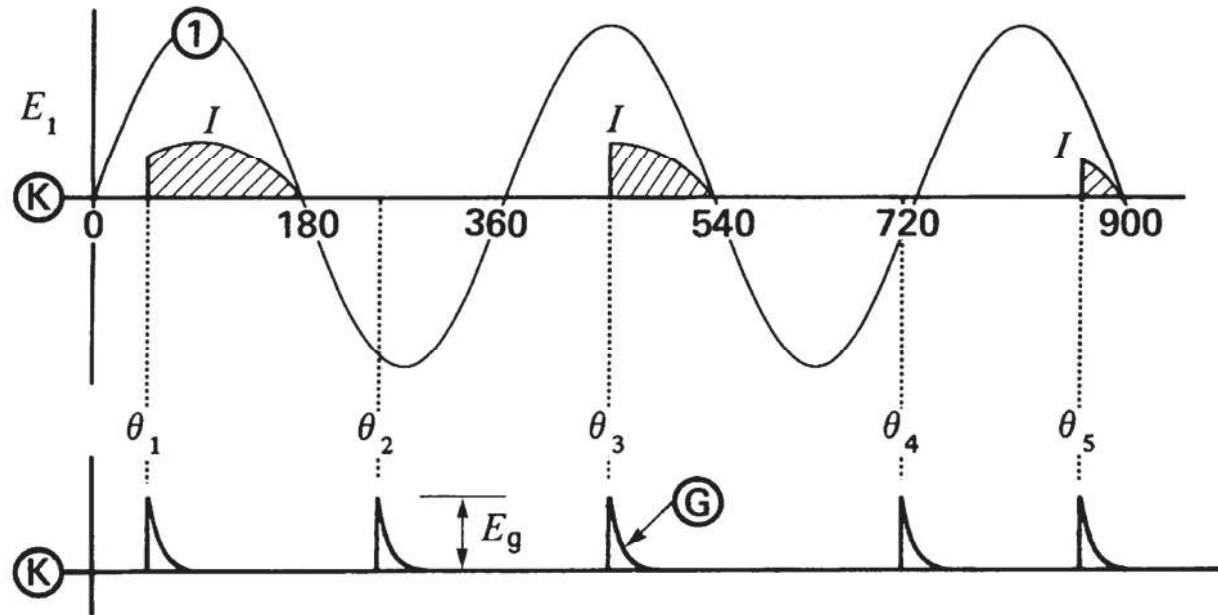


Figure 21.27 a. Thyristor and resistor connected to an ac source. B
 . Thyristor behavior depends on the timing of the gate pulses.



(a)

Figure 21.27 (continued) a. Thyristor and resistor connected to an ac source
 . b. Thyristor behavior depends on the timing of the gate pulses.



(b)

Figure 21.28 a. Thyristor connected to a dc source. b. Forced commutation.

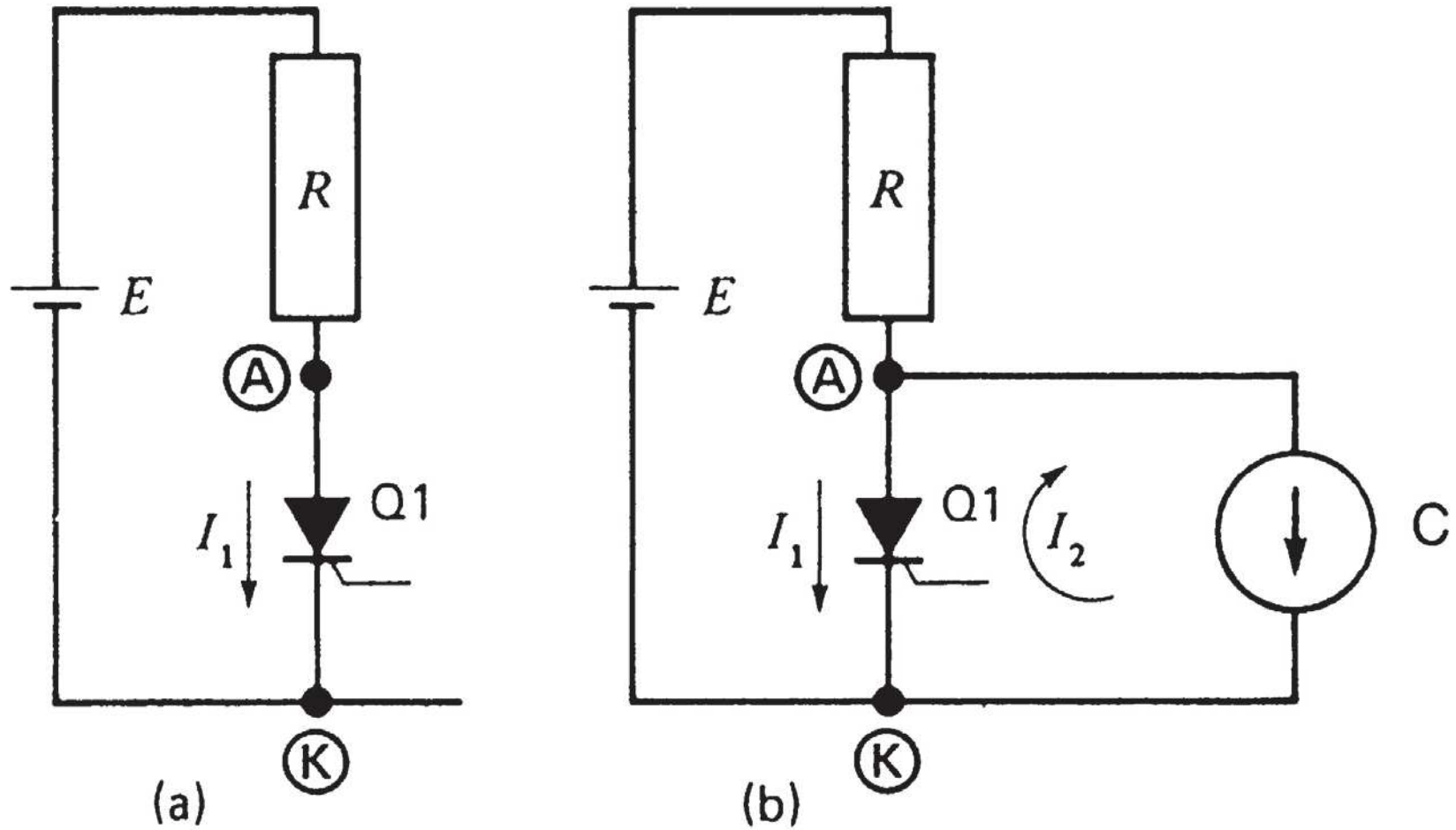


Figure 21.29 A discharging capacitor C and an auxiliary thyristor $Q2$ can force-commutate the main thyristor $Q1$. Thus, the current in load R can be switched on and off by triggering $Q1$ and $Q2$ in succession.

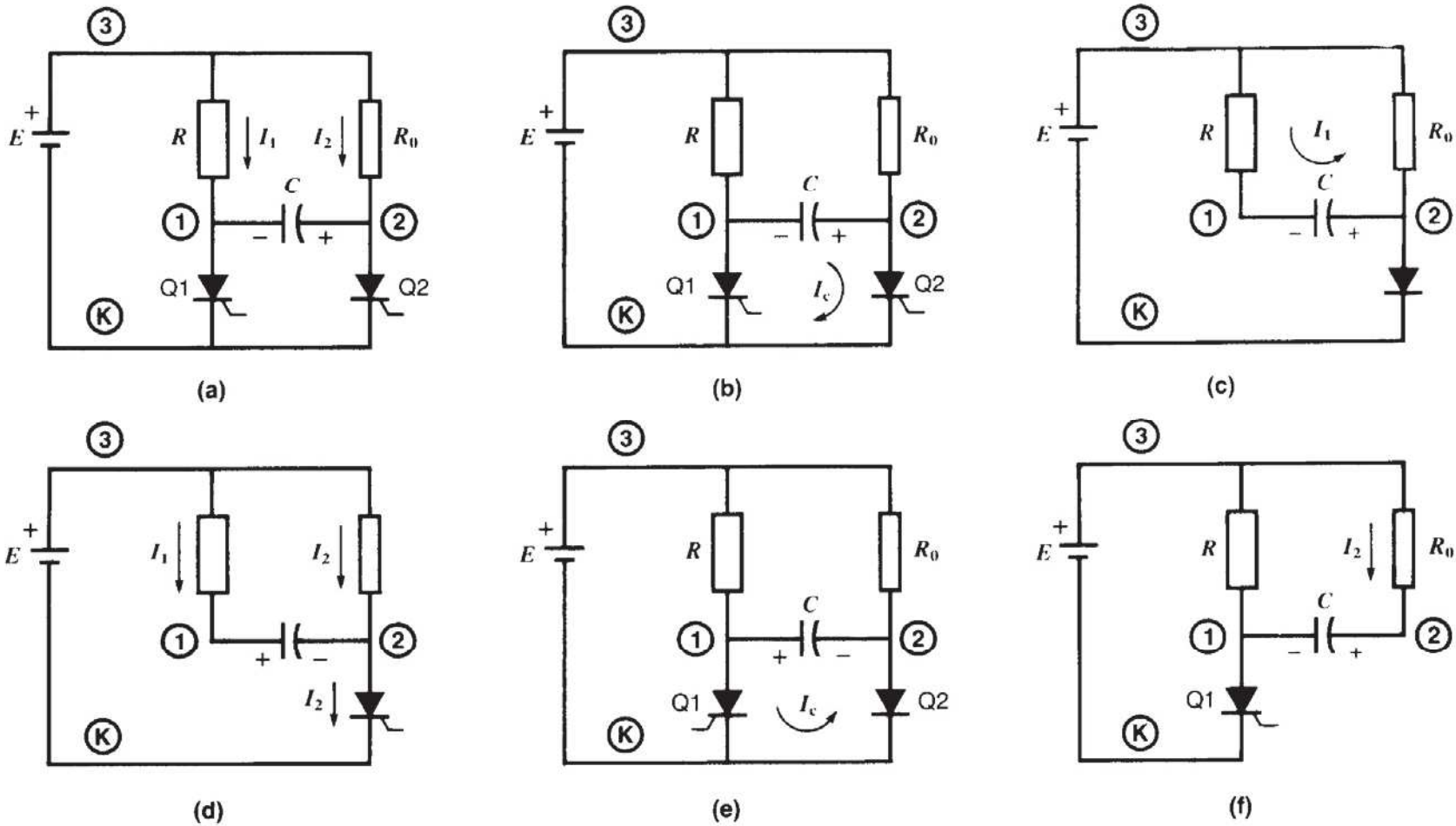
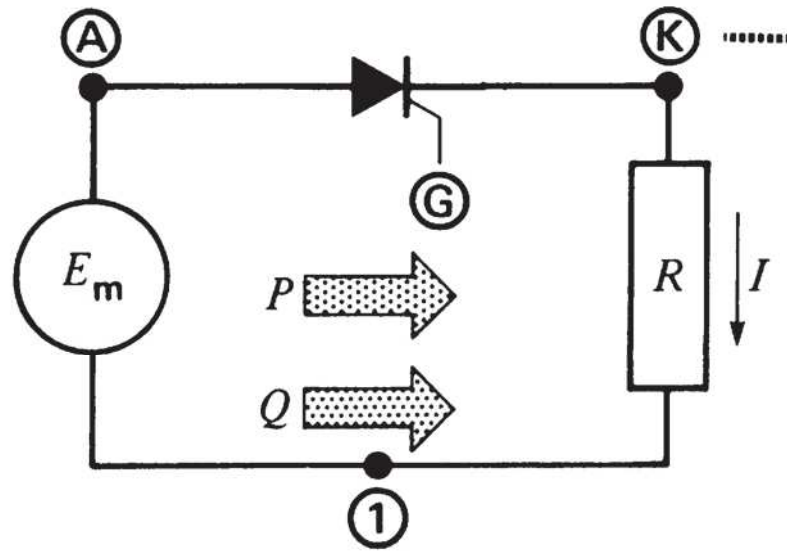
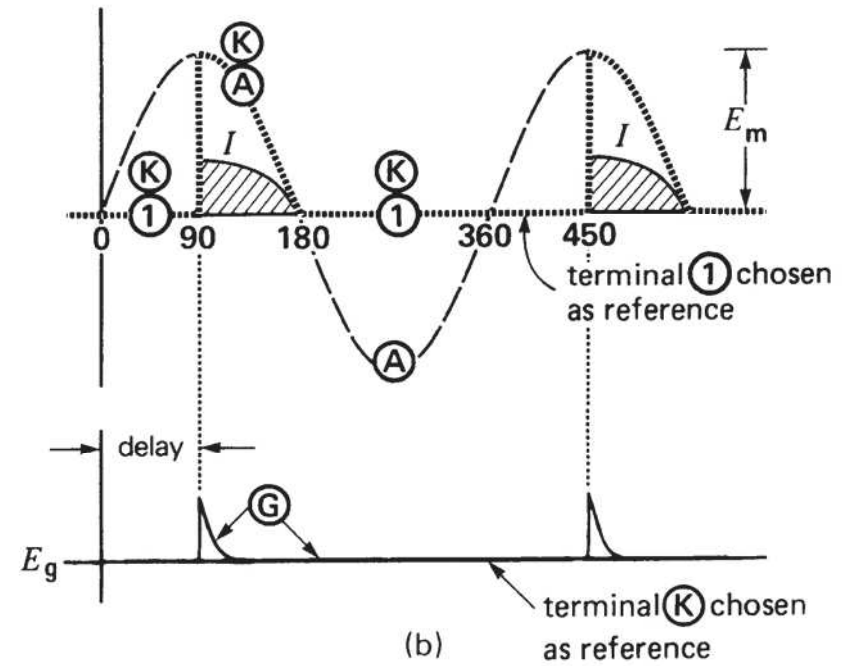


Figure 21.30 a. SCR supplying a passive load. b. Voltage and current waveforms.

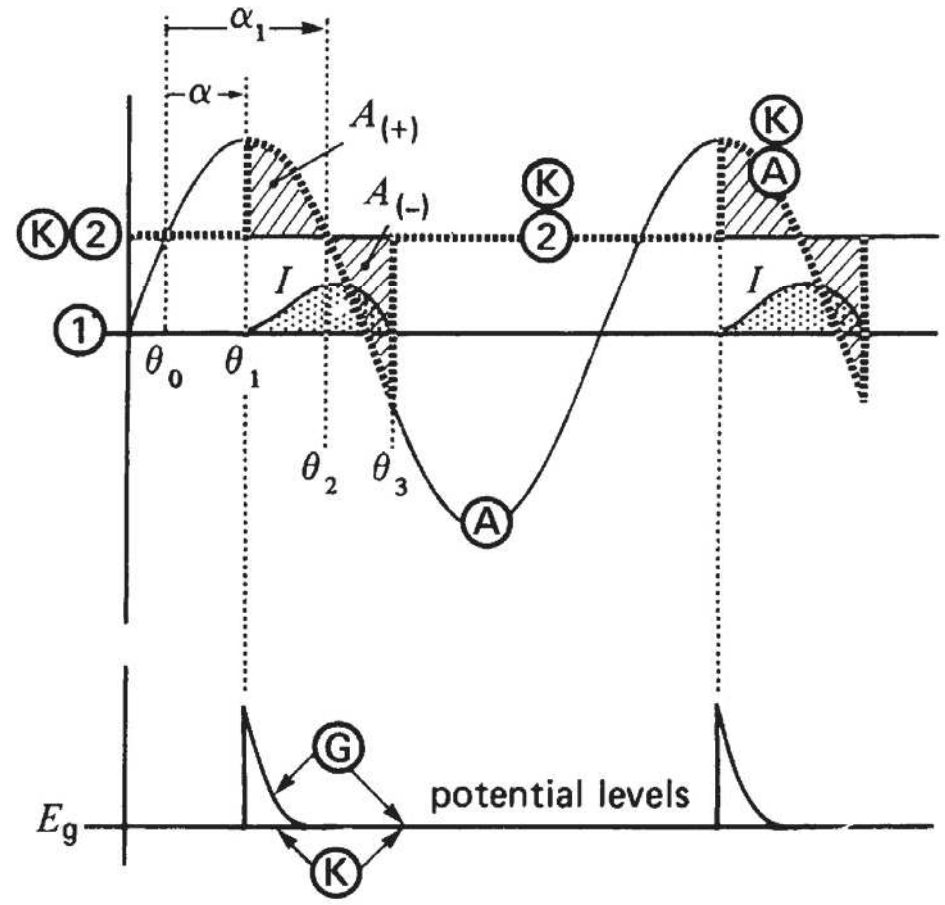
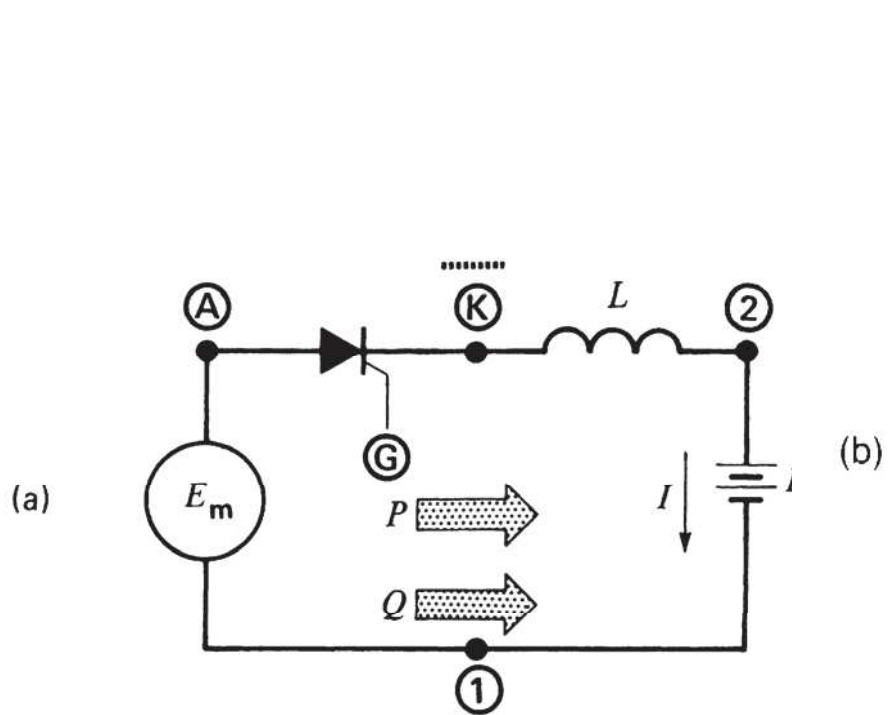


(a)



(b)

Figure 21.31 a. SCR supplying an active load. b. Voltage and current waveforms.



Line commutated inverter

Figure 21.32 a. Line-commutated inverter. b. Voltage and current waveforms

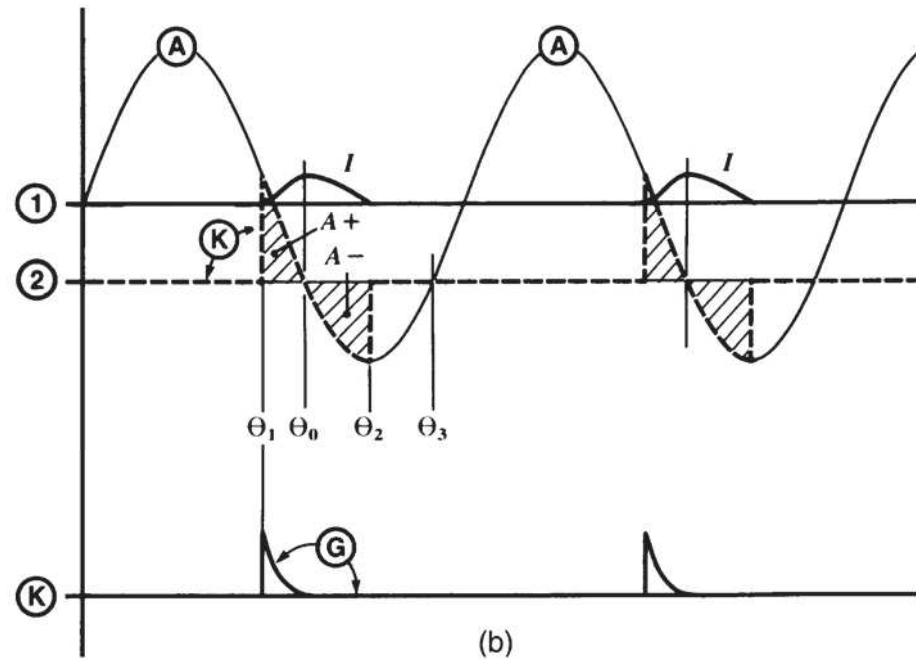
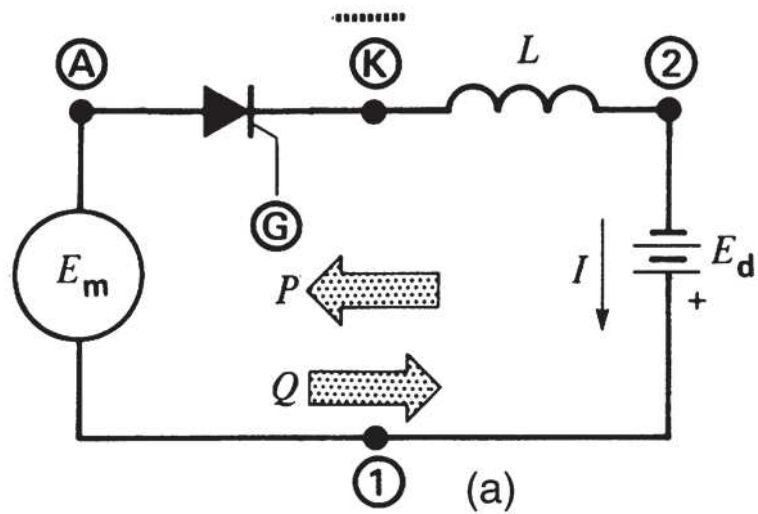
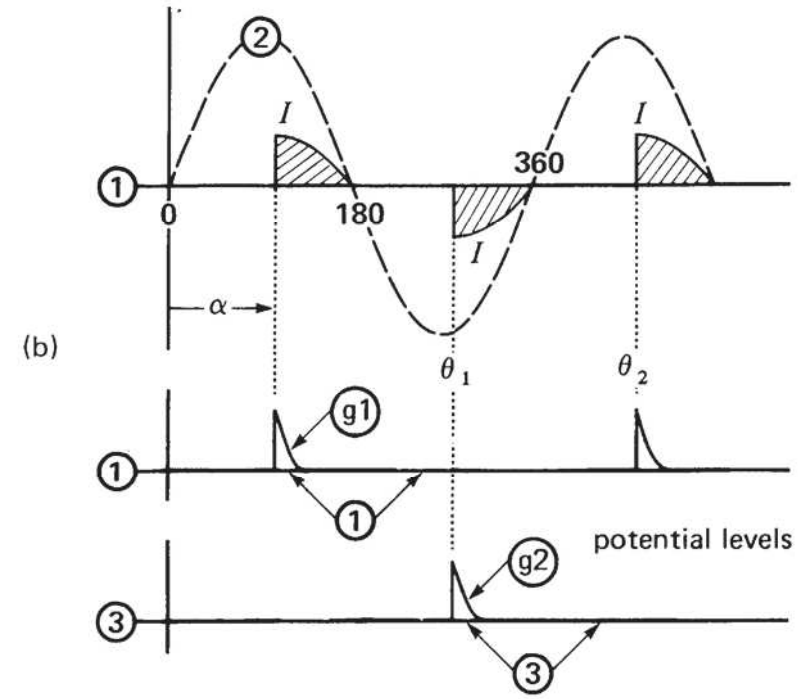
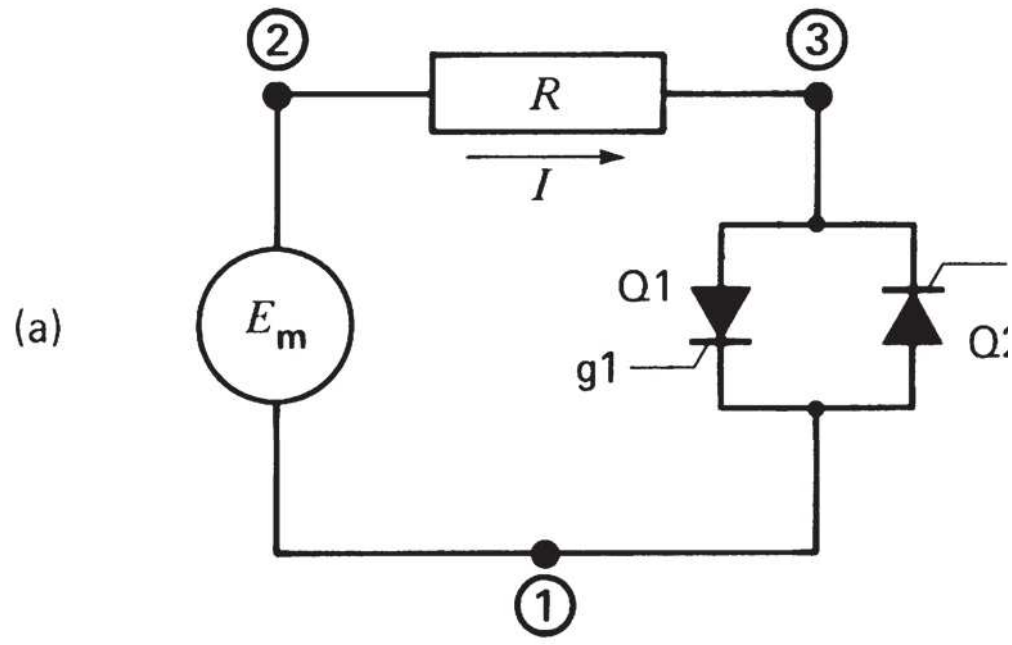


Figure 21.33 a. Electronic contactor. b. Waveforms with a resistive load.



Cycloconverter

Figure 21.34 Elementary cycloconverter.

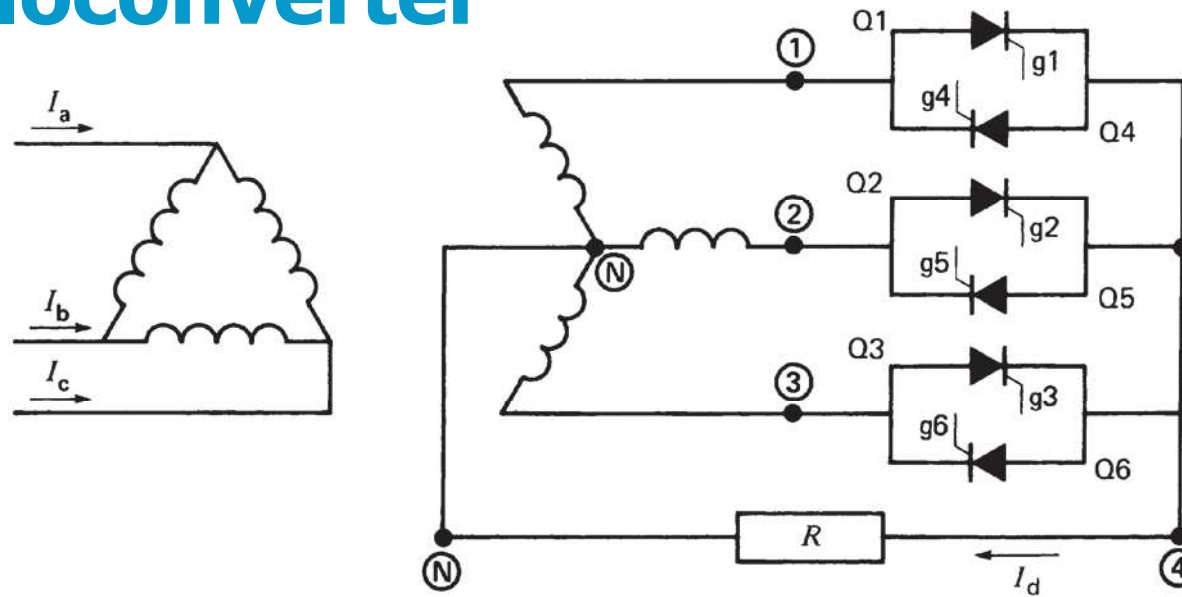
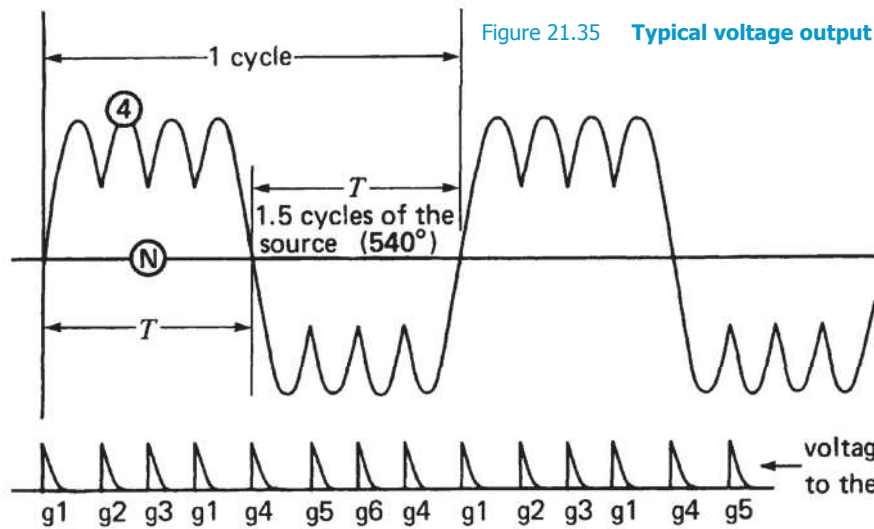


Figure 21.35 Typical voltage output of a cycloconverter.



3 phase 6 pulse contr. converter

Figure 21.36 Three-phase, 6-pulse thyristor converter.

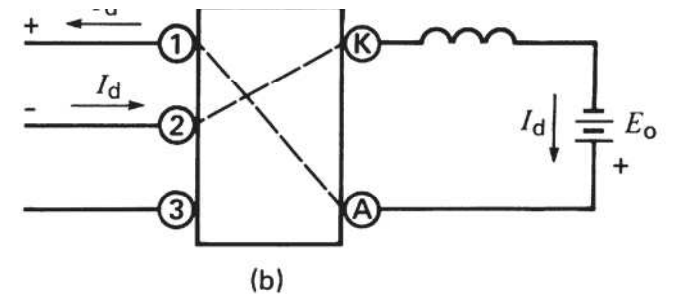
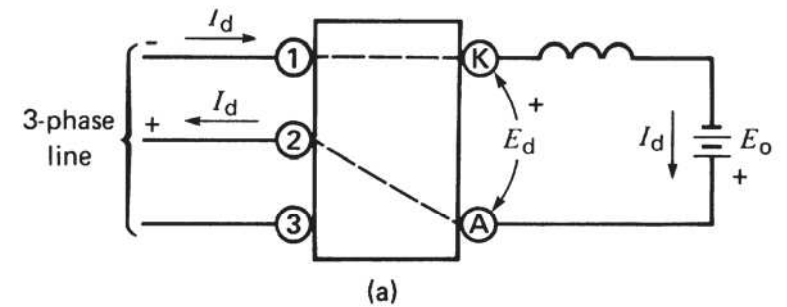
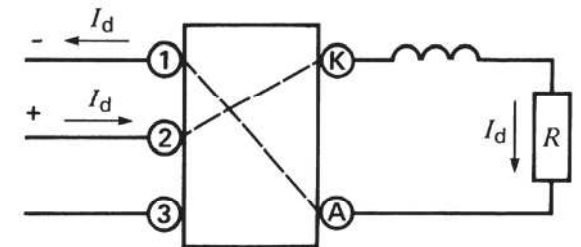
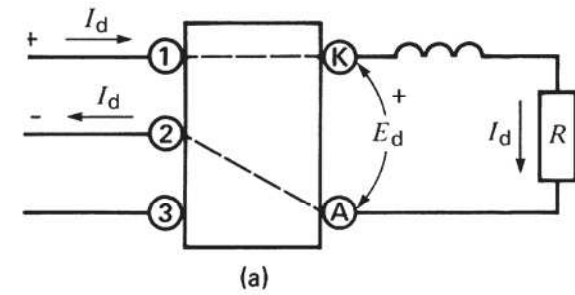
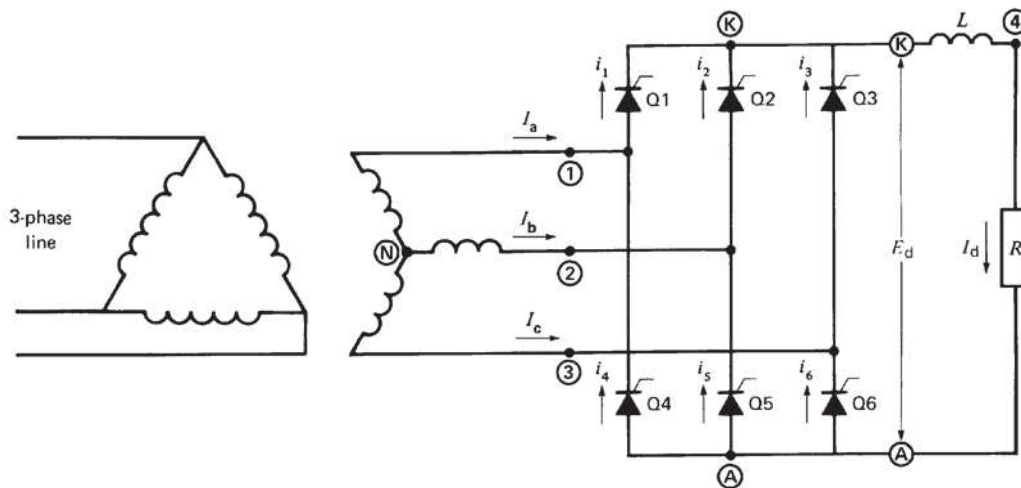


Figure 21.40a Delay angle: zero.

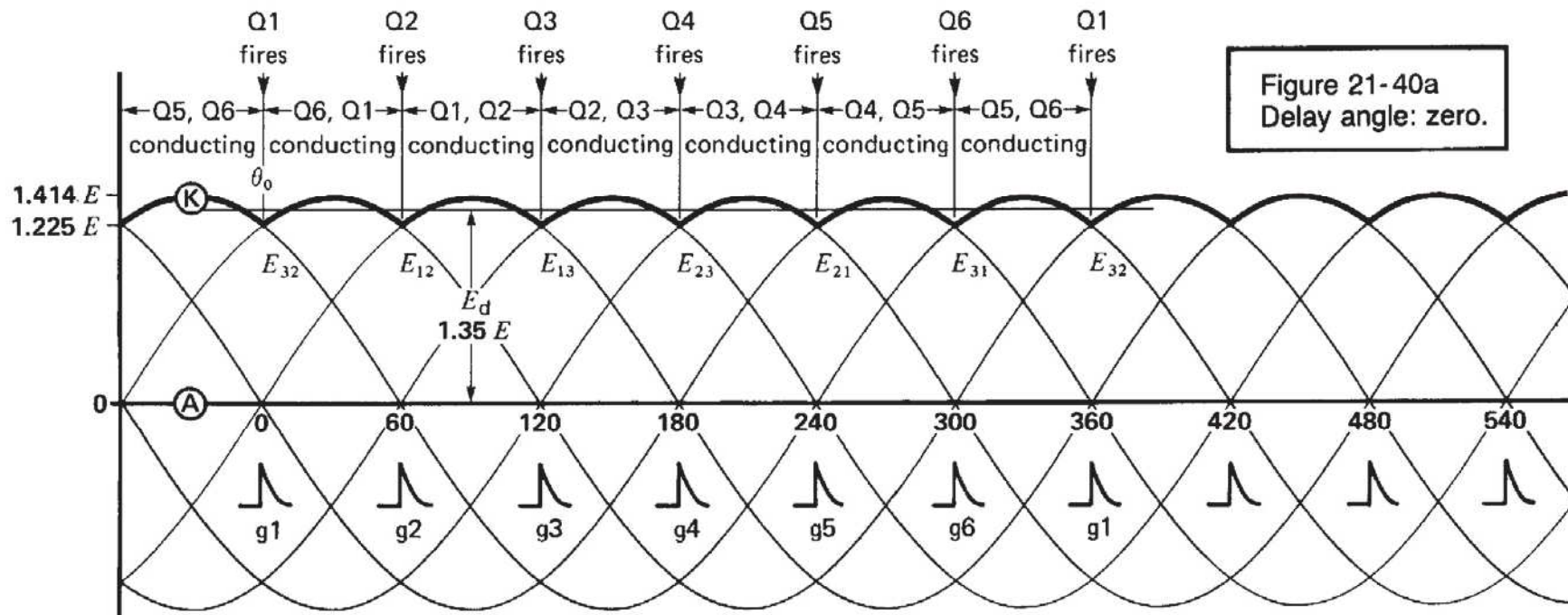
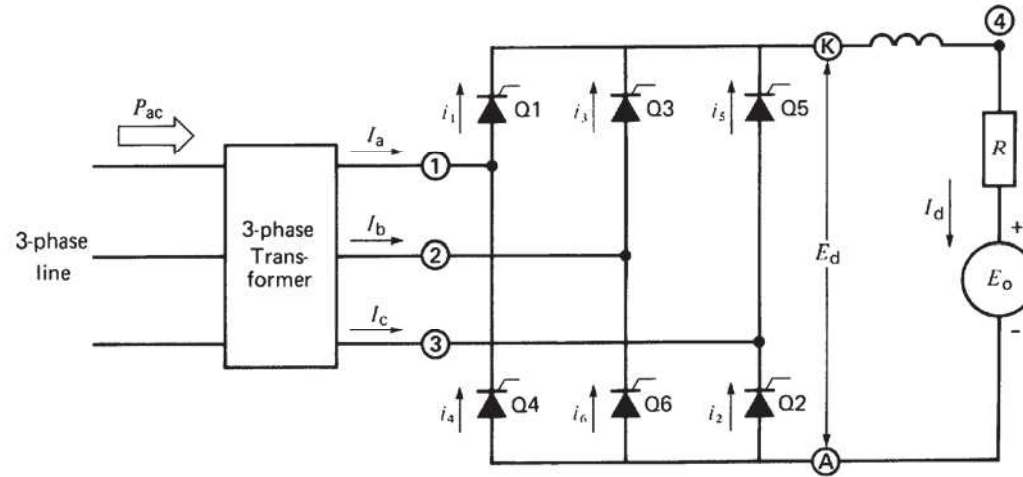


Figure 21.40b Delay angle: 15°.

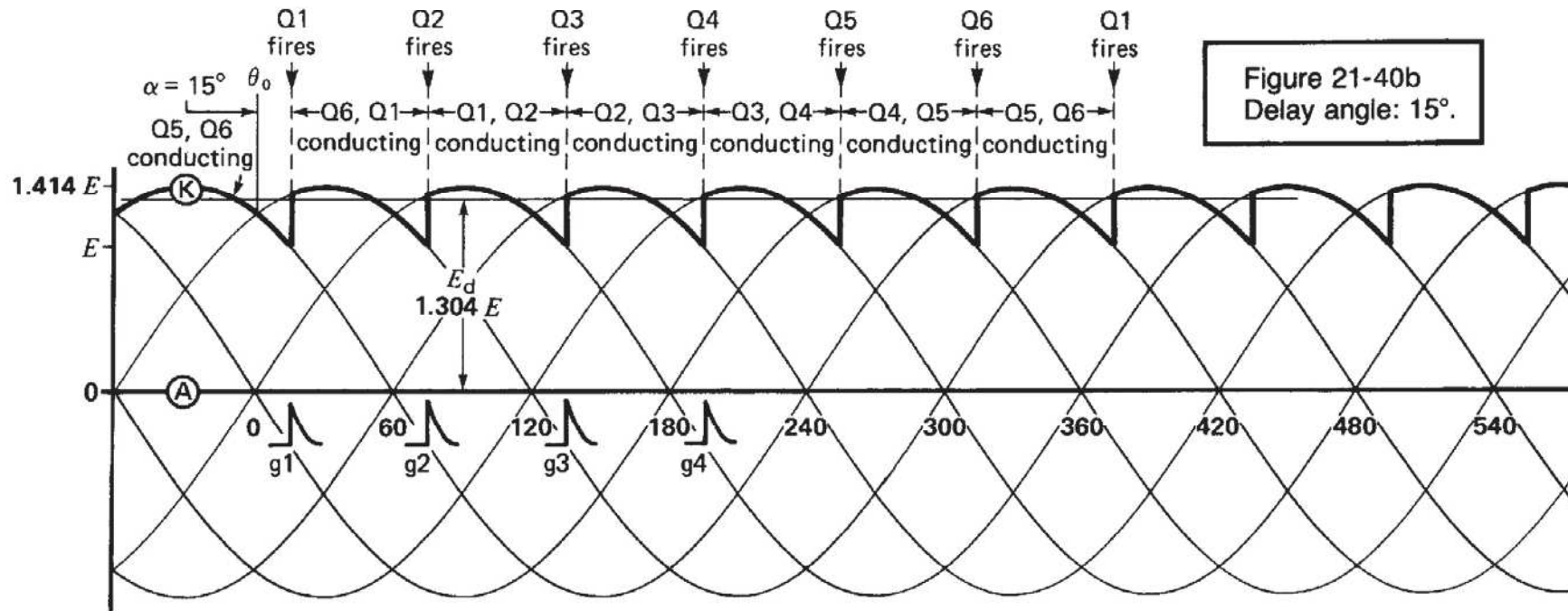
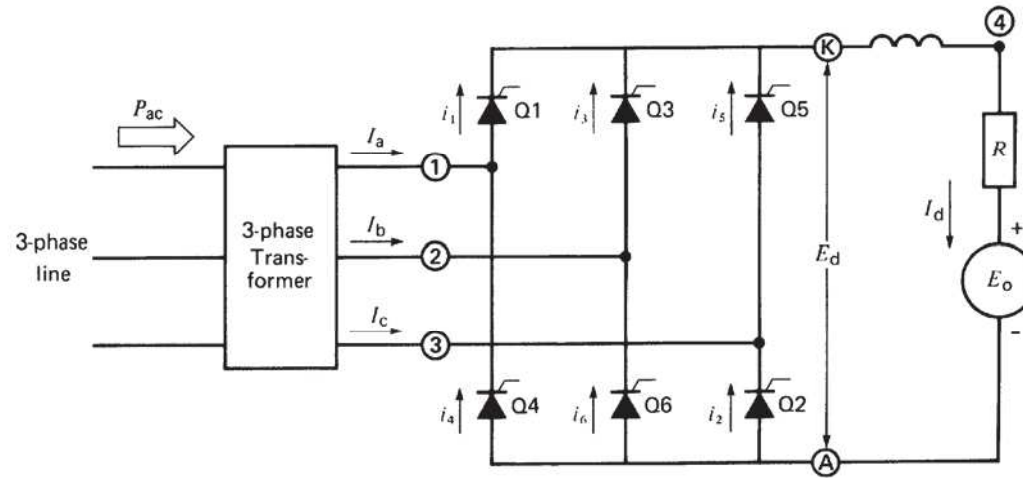


Figure 21.40c Delay angle: 45° .

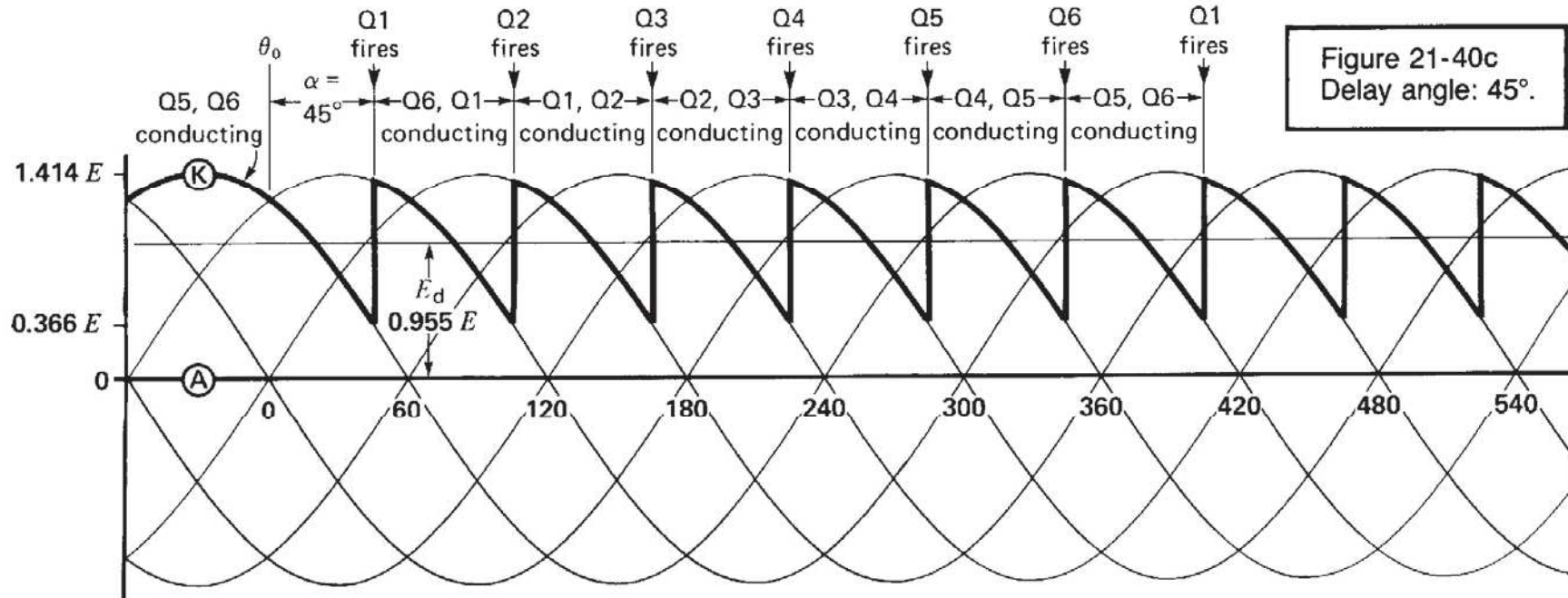
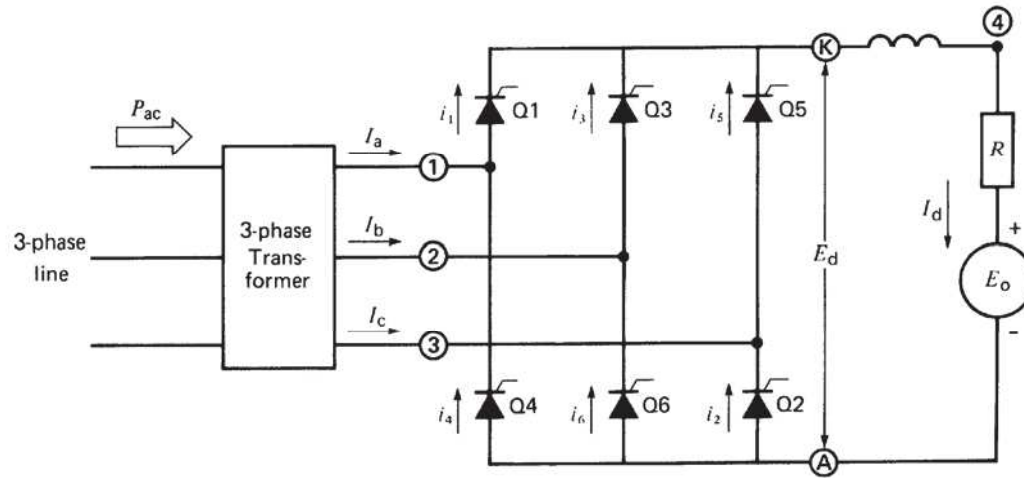
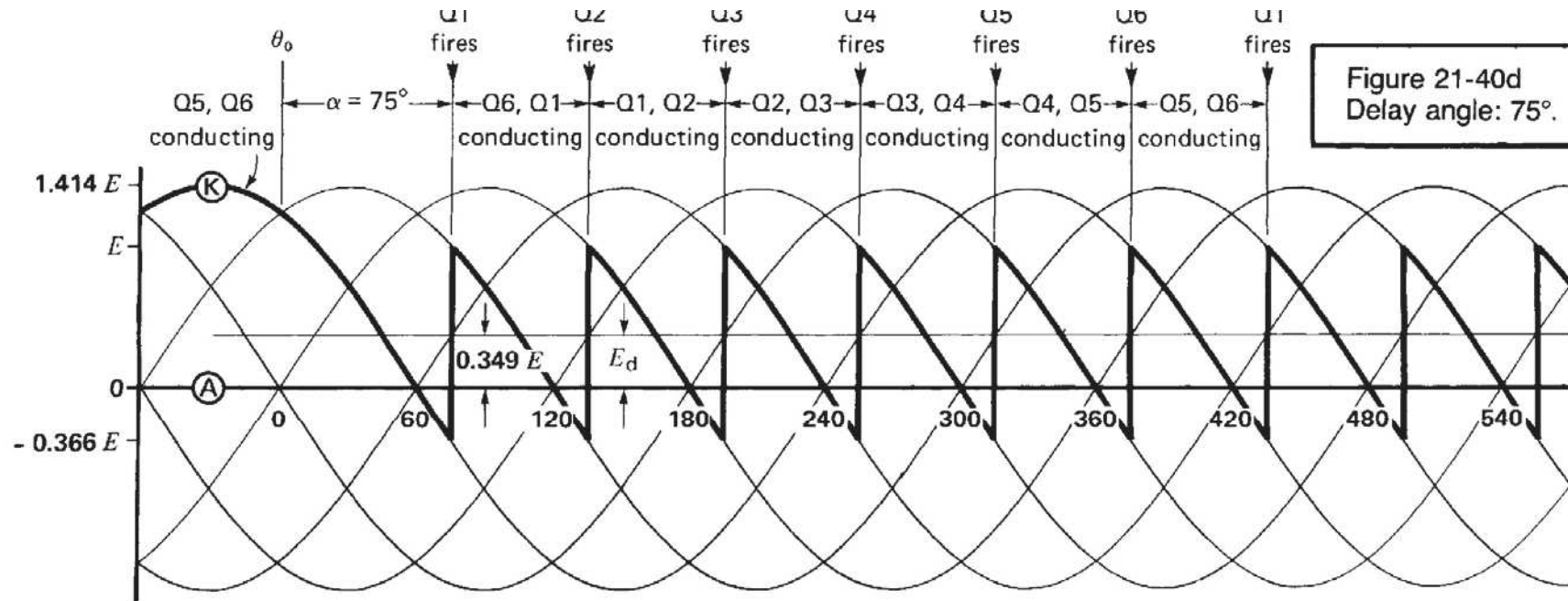
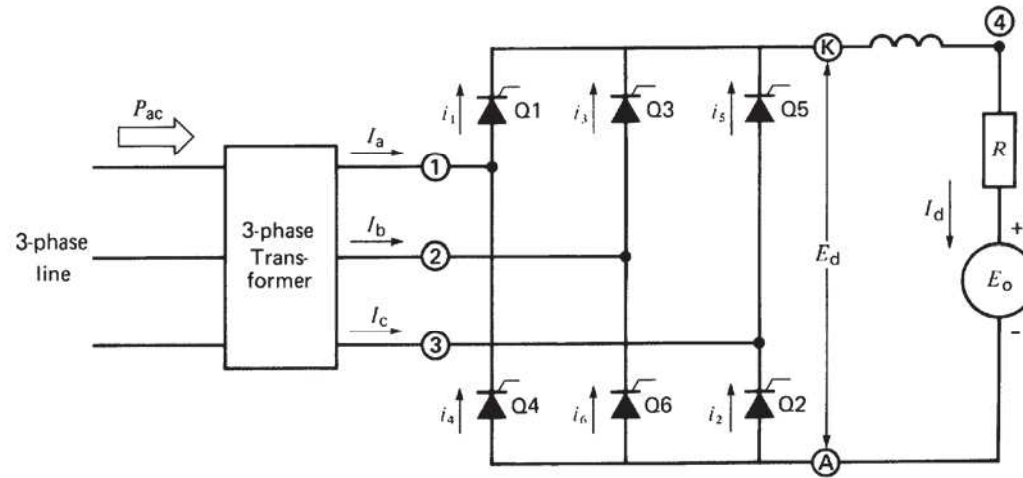


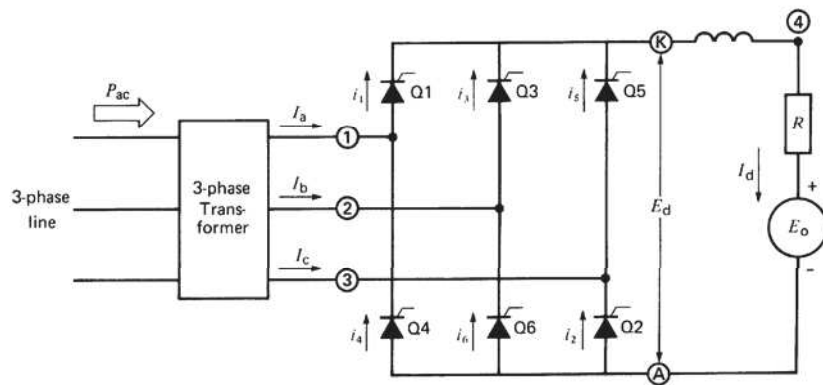
Figure 21-40c
Delay angle: 45° .

Figure 21.40d Delay angle: 75°.



Example 21.17

- The 3 phase converter is connected to 3 phase 480 V 60 Hz source, Load 500 V dc resistance 2 ohm. Calculate the power supplied to the load for delays of 15 and 75.



- $E_d = 1,35 E \cos \alpha$

voltage drop on R

- $E = E_d - E_o$

- $I_d = E/R$

- $P = E_d I_d$

Figure 21.41 Three-phase, 6-pulse converter in the inverter mode.

Inverter mode

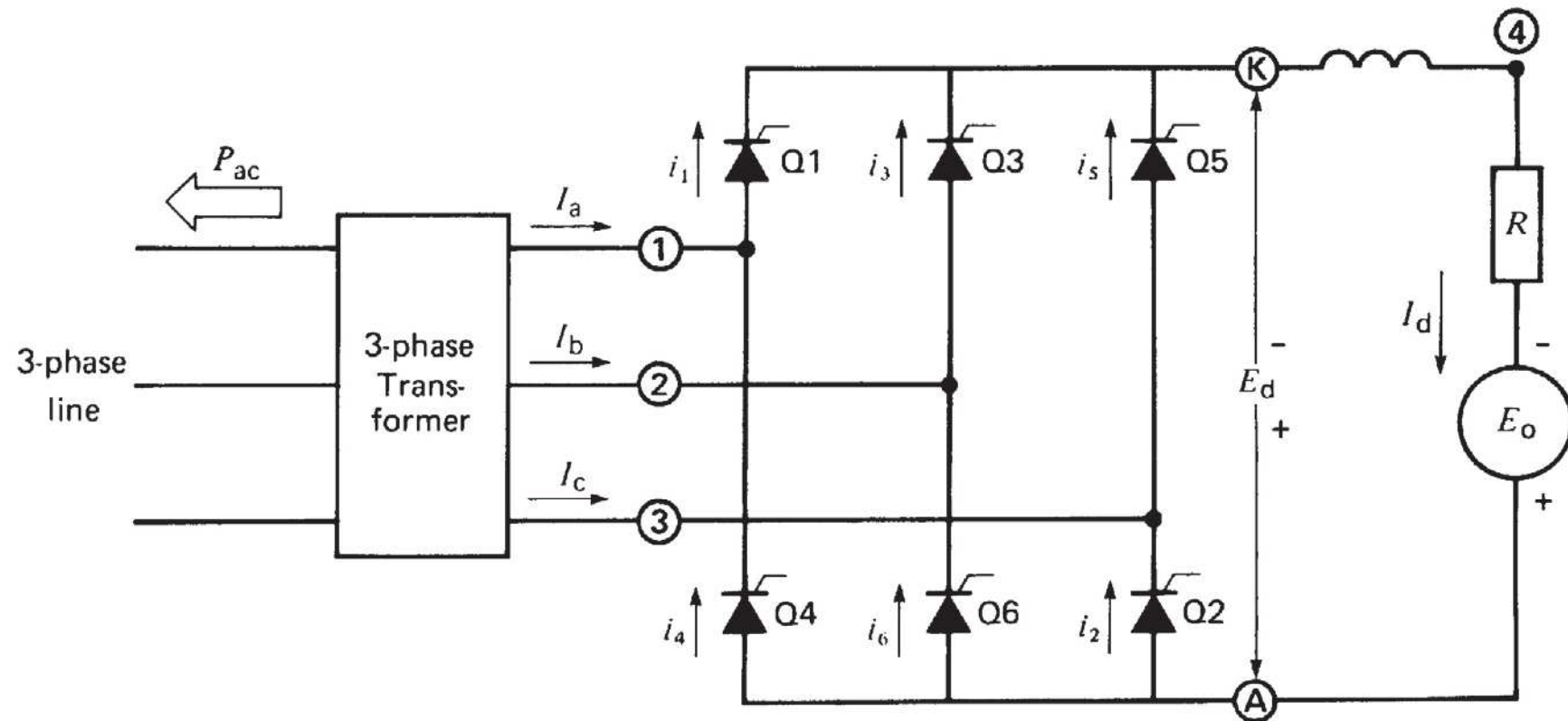


Figure 21.42a Triggering sequence and waveforms with a delay angle of 105° .

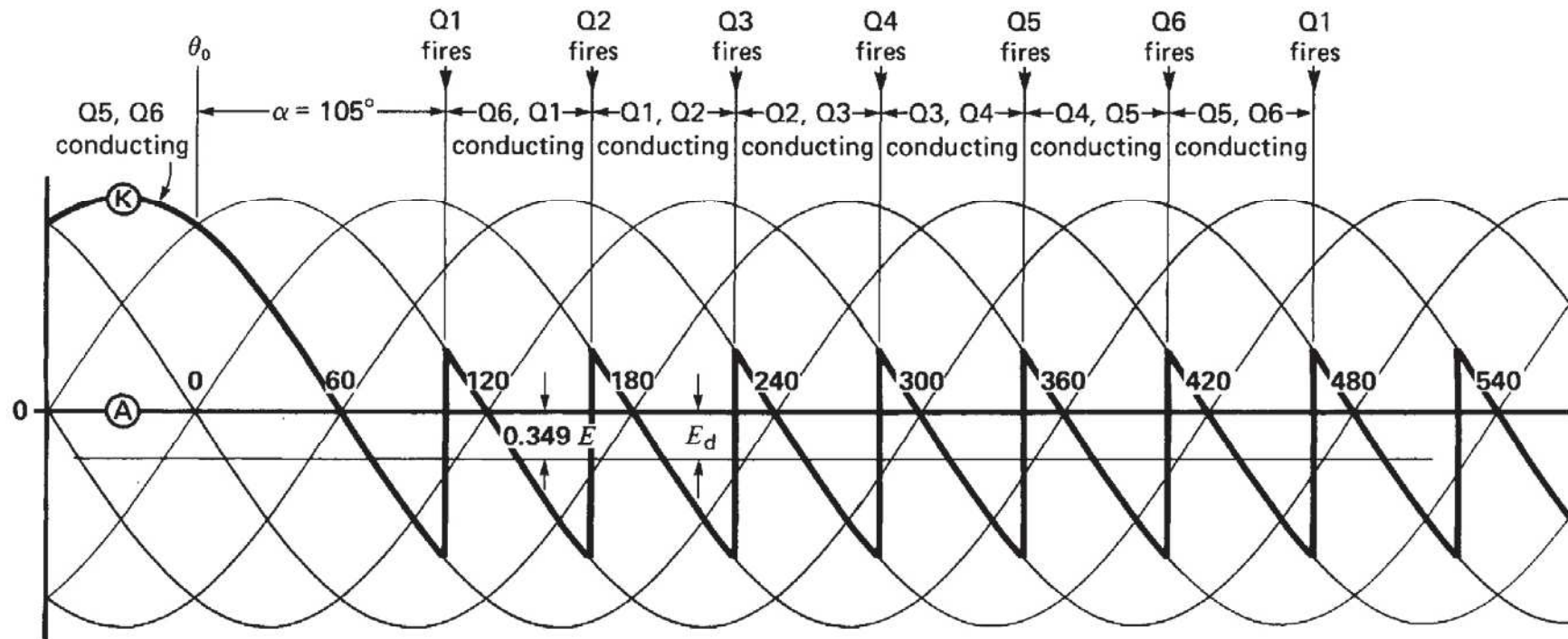


Figure 21.42b Triggering sequence and waveforms with a delay angle of 135°.

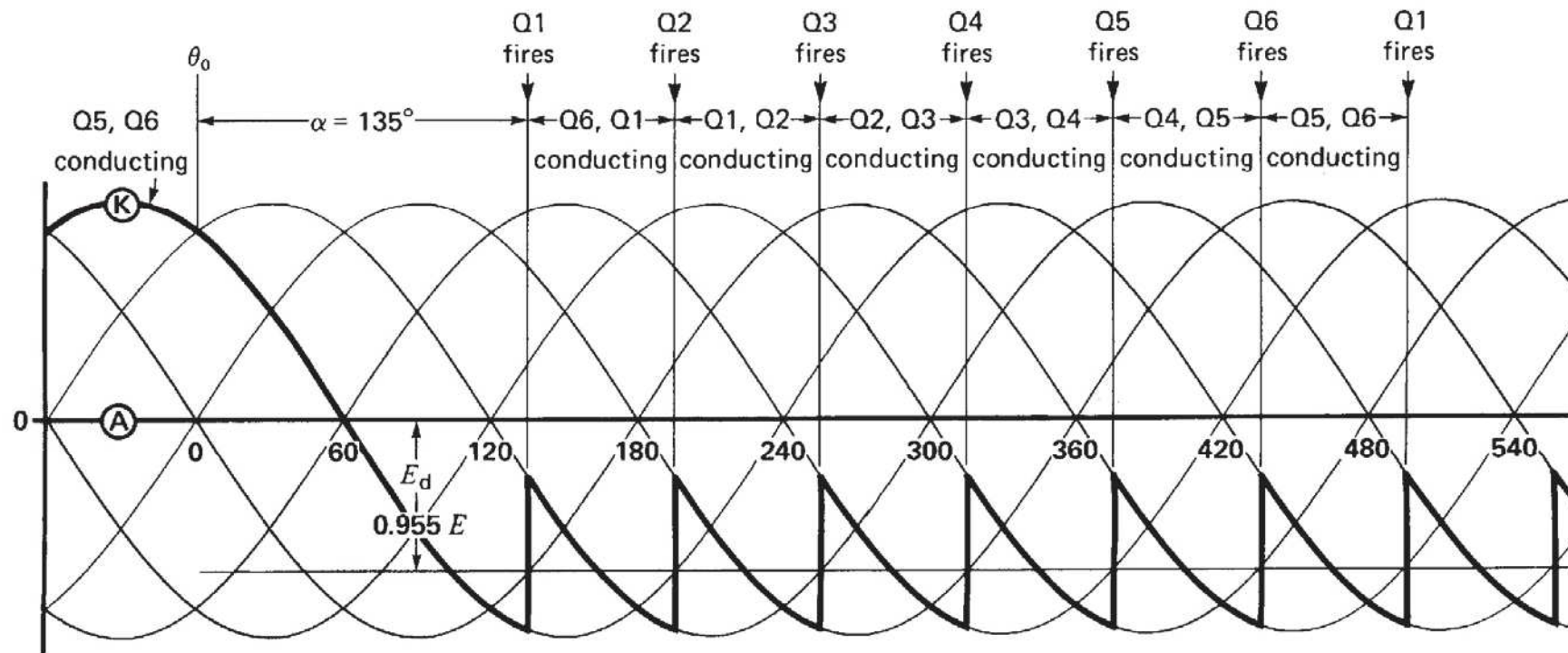


Figure 21.42c Triggering sequence and waveforms with a delay angle of 165°.

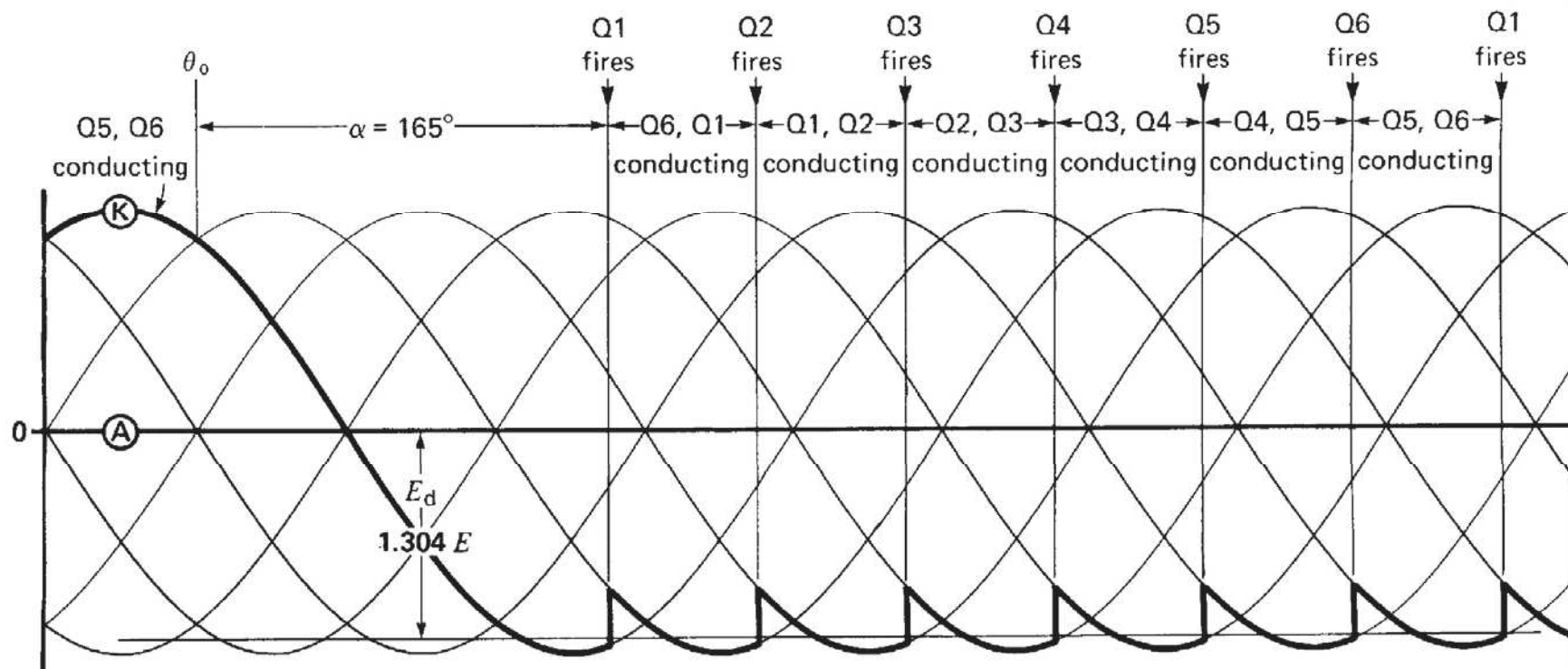


Figure 21.43 Permitted gate firing zones for thyristor Q1.

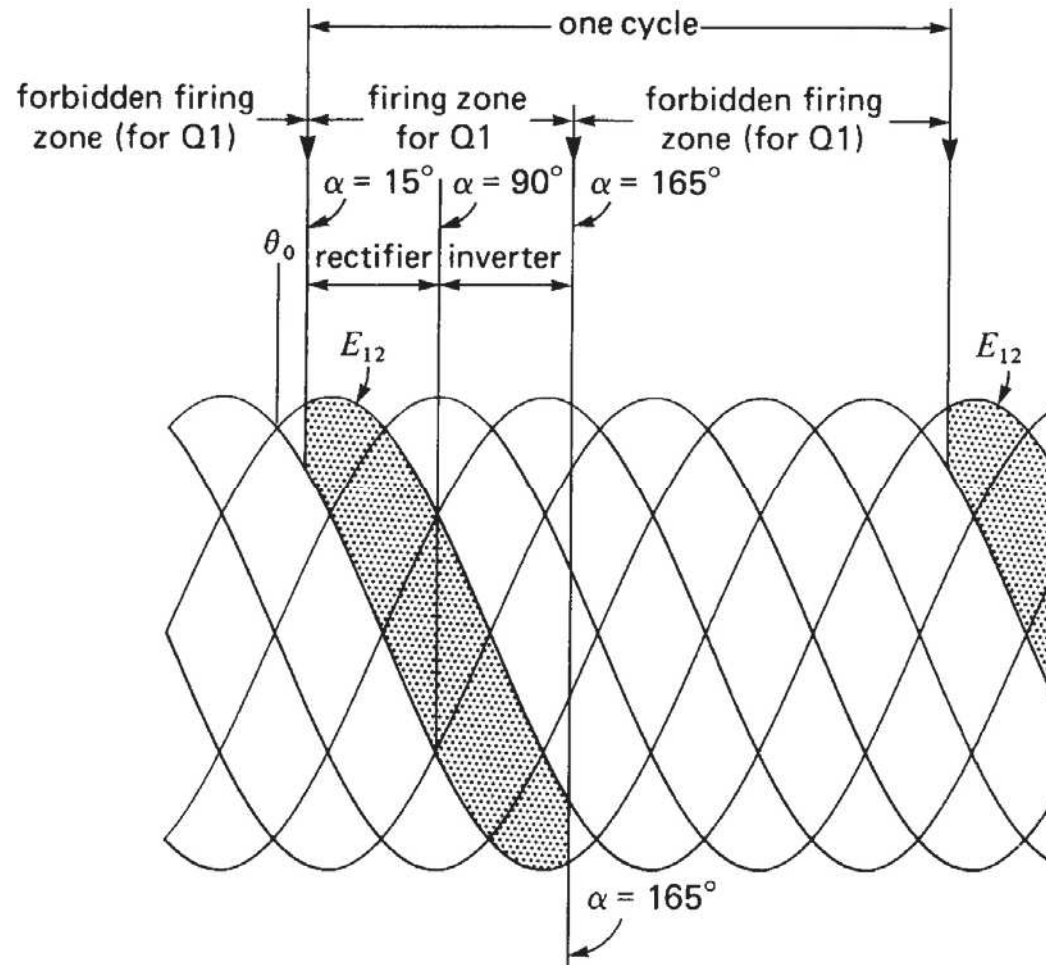


Figure 21.44 Equivalent circuit of a thyristor converter.

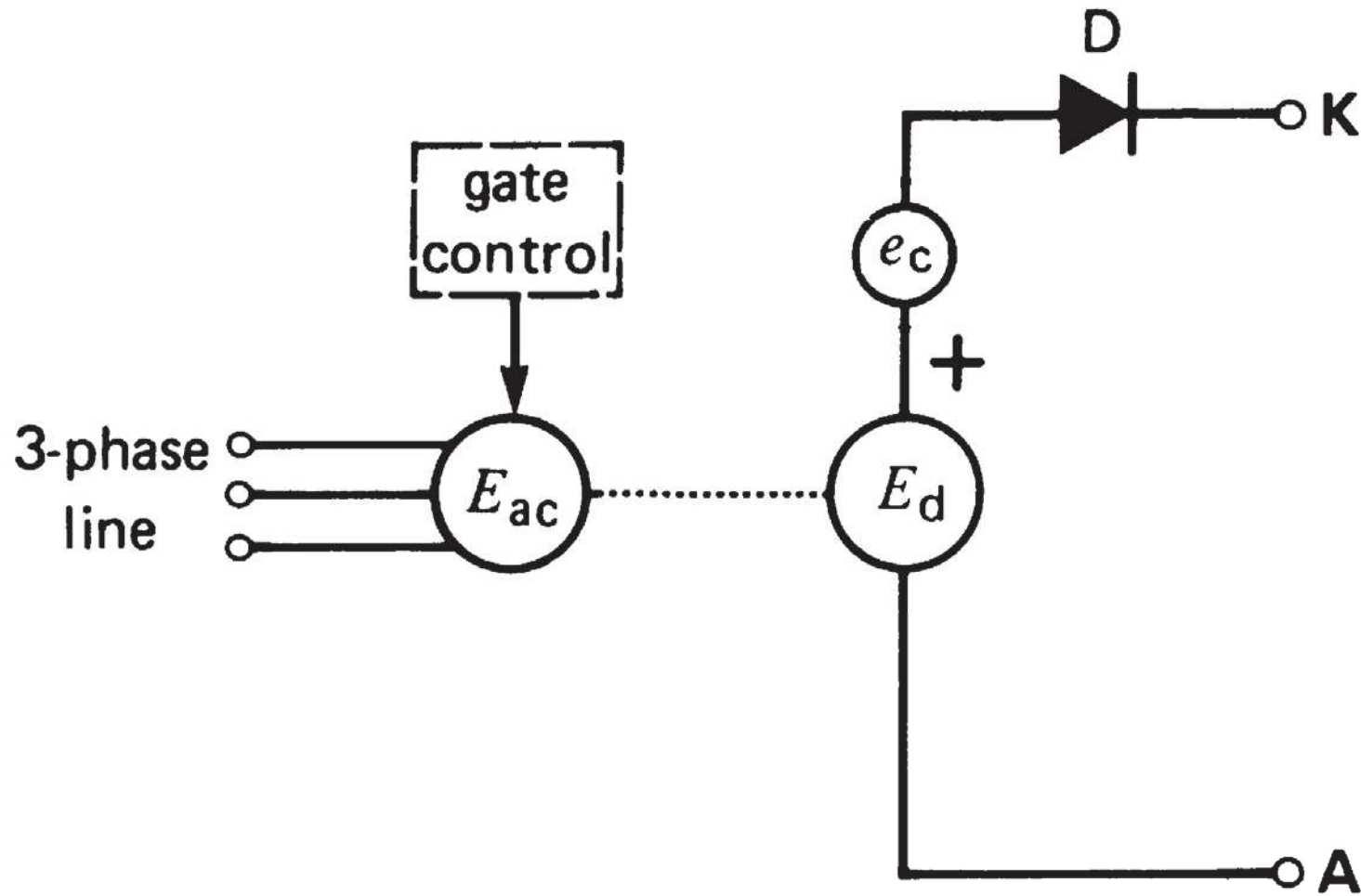


Figure 21.45 Equivalent circuit of a 3-phase converter in the rectifier mode.

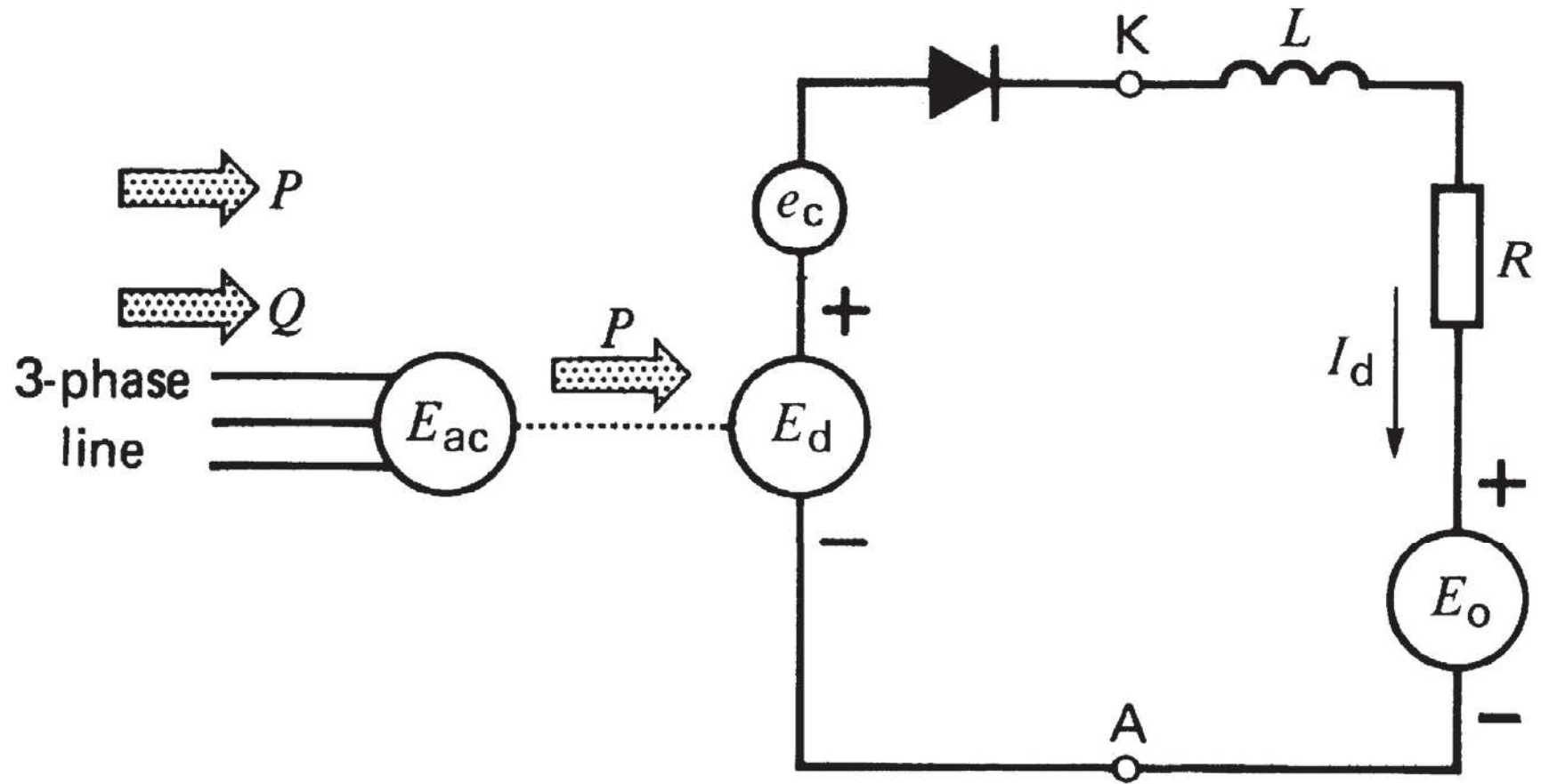


Figure 21.46 Equivalent circuit of a 3-phase thyristor converter in the inverter mode.

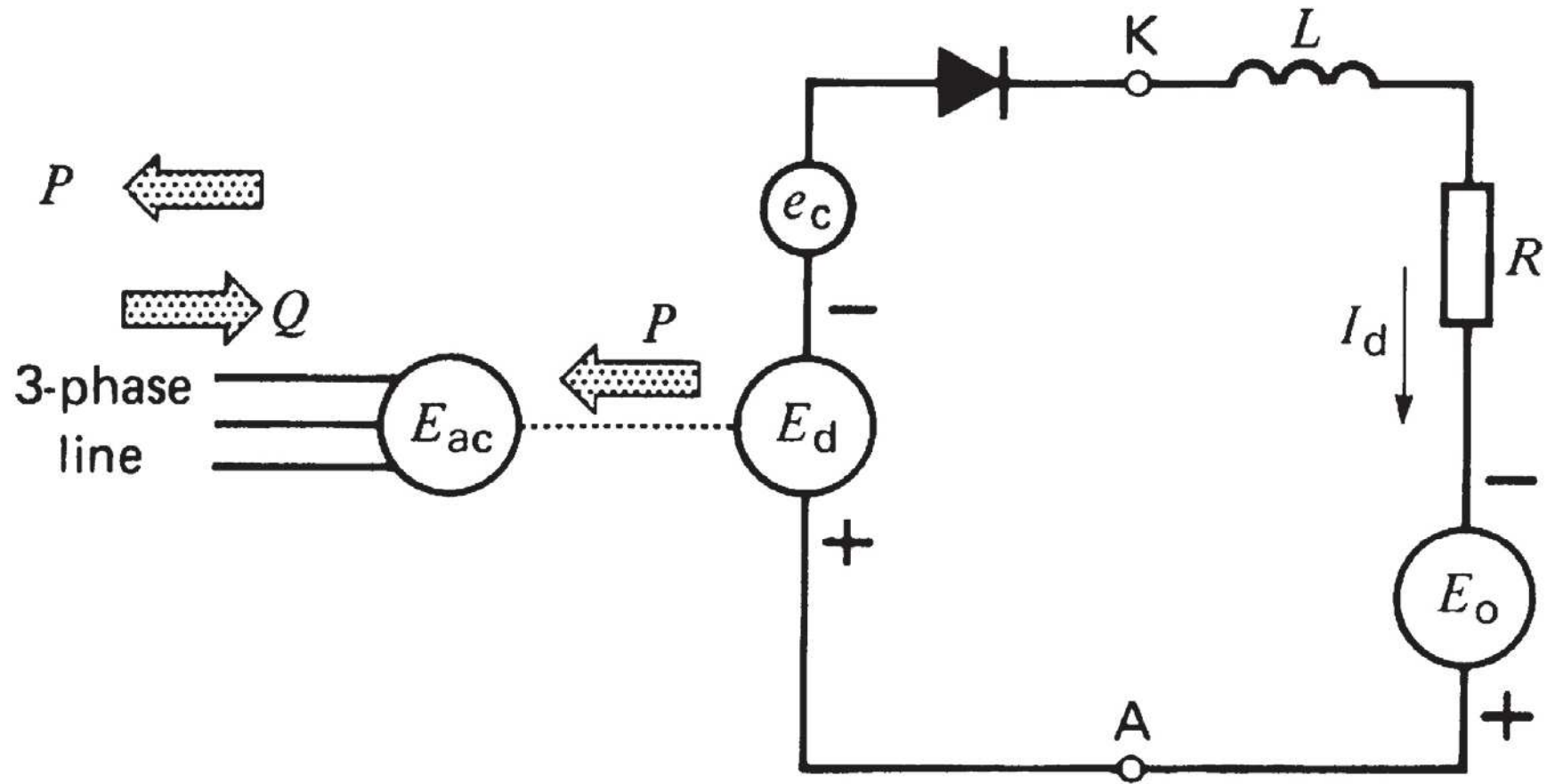


Figure 21.47 Voltage and current waveforms in the thyristor converter of Fig. 21.39 with a delay angle of 45° .

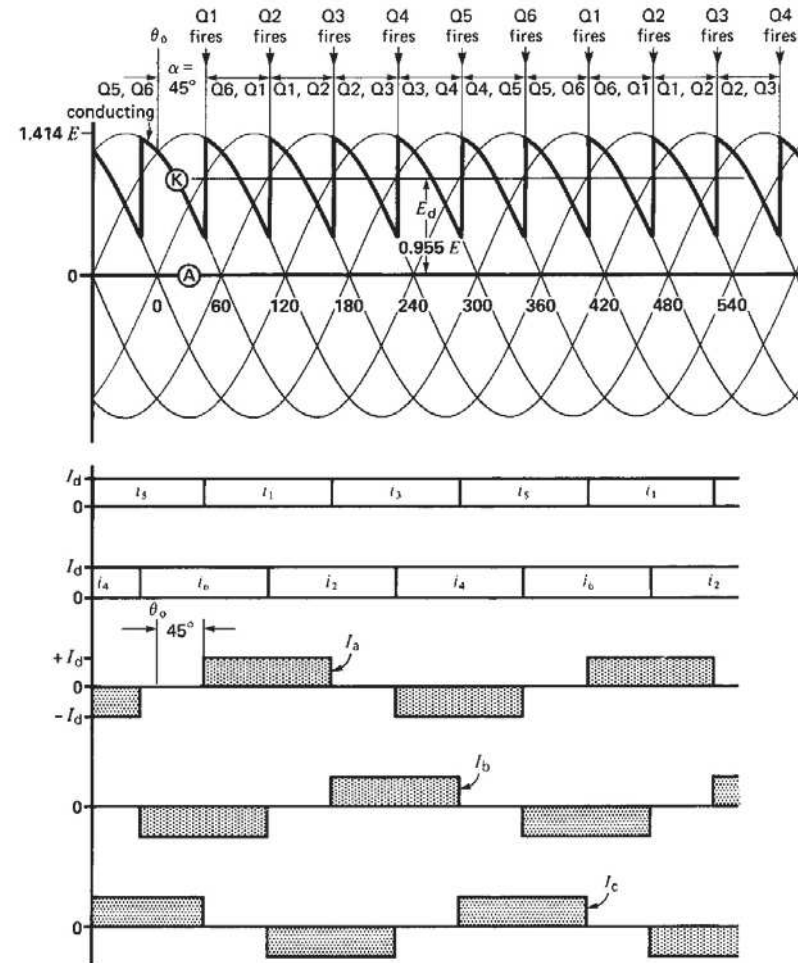


Figure 21.48 See Example 21-11.

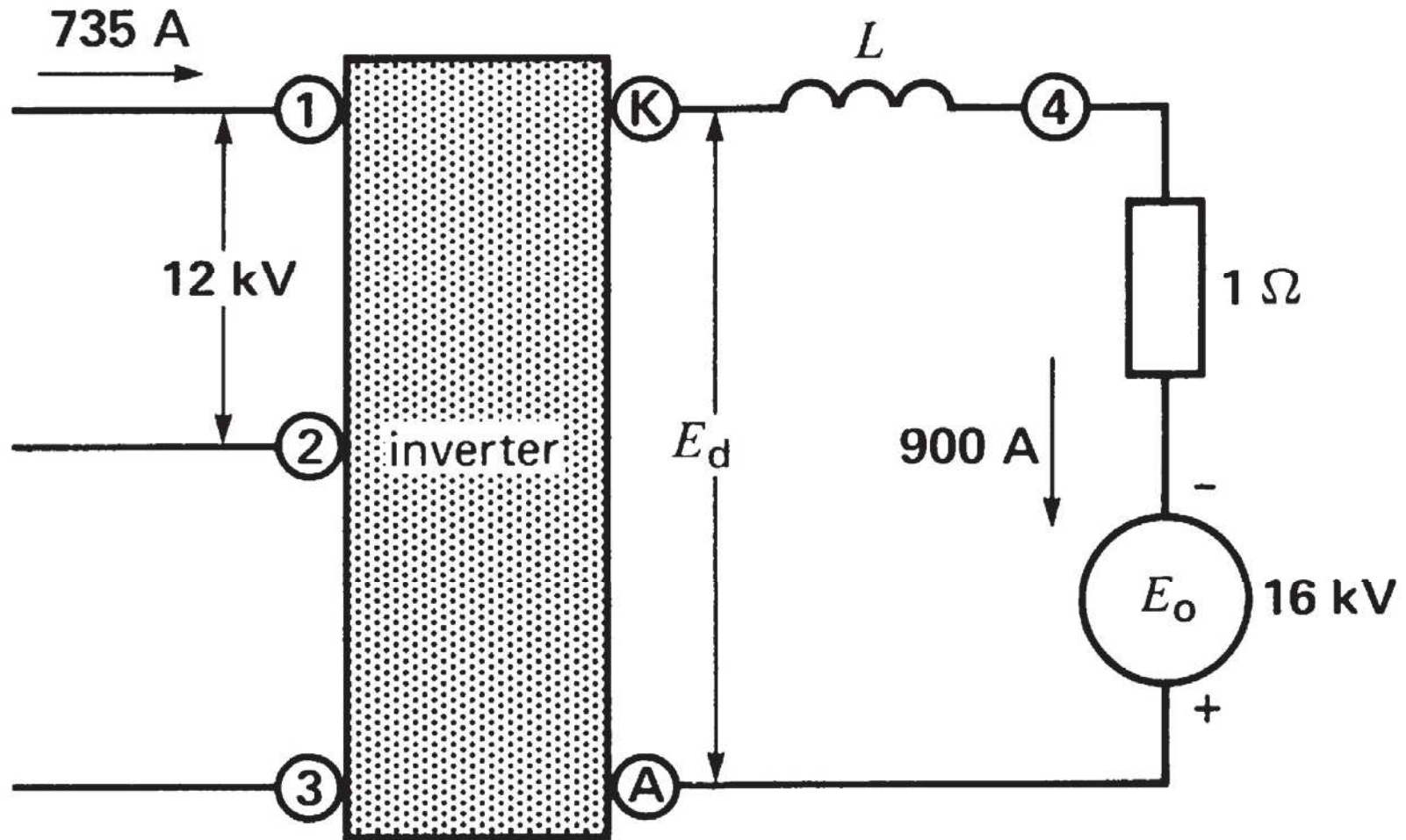


Figure 21.49 a. Instantaneous commutation in a rectifier when $\alpha = 45^\circ$ (see Fig. 21.58). b. Same conditions with commutation overlap of 30° , showing current waveshapes in Q1, Q3, Q5.

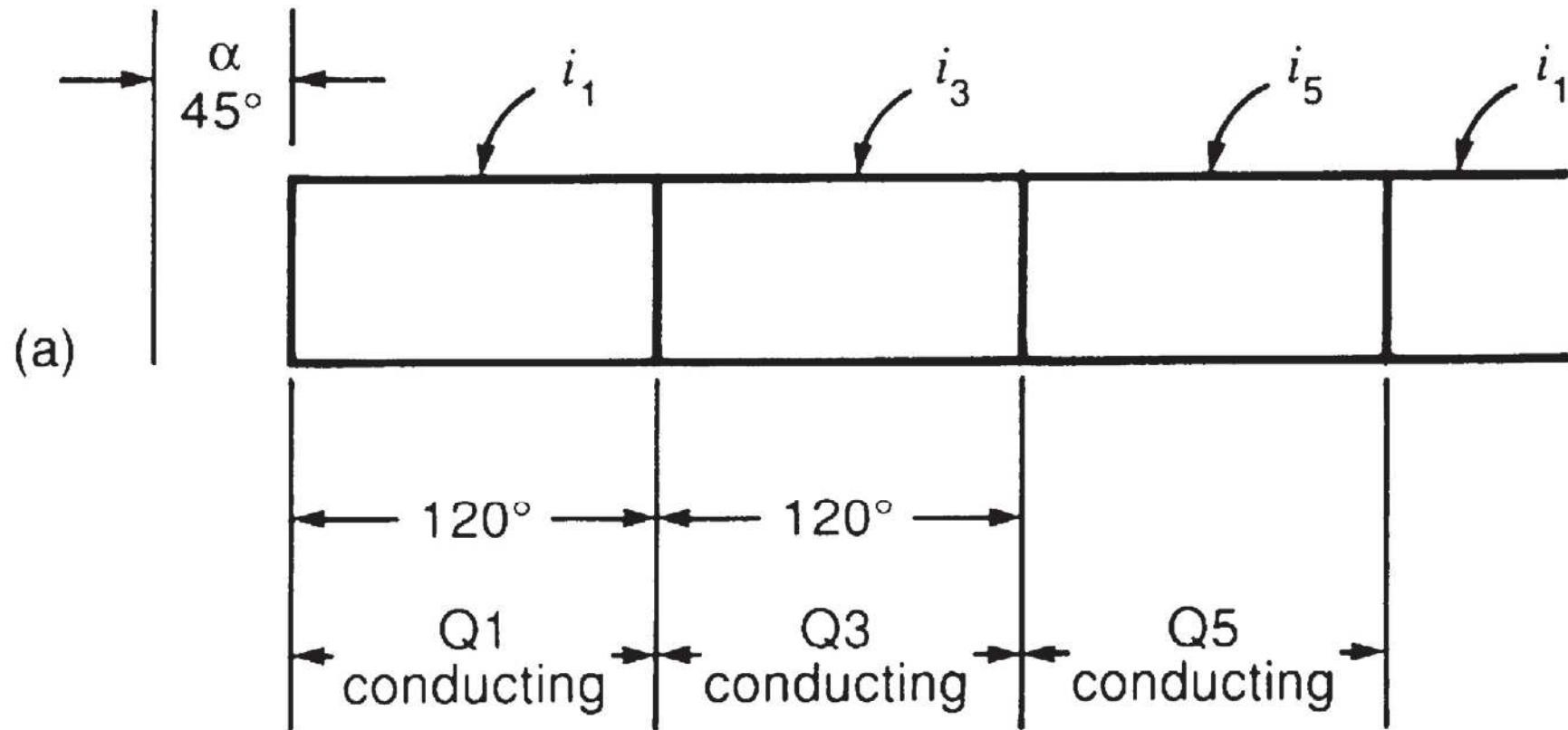


Figure 21.49 (continued) a. Instantaneous commutation in a rectifier when $\alpha = 45^\circ$ (see Fig. 21.58). b. Same conditions with commutation overlap of 30° , showing current waveshapes in Q1, Q3, Q5.

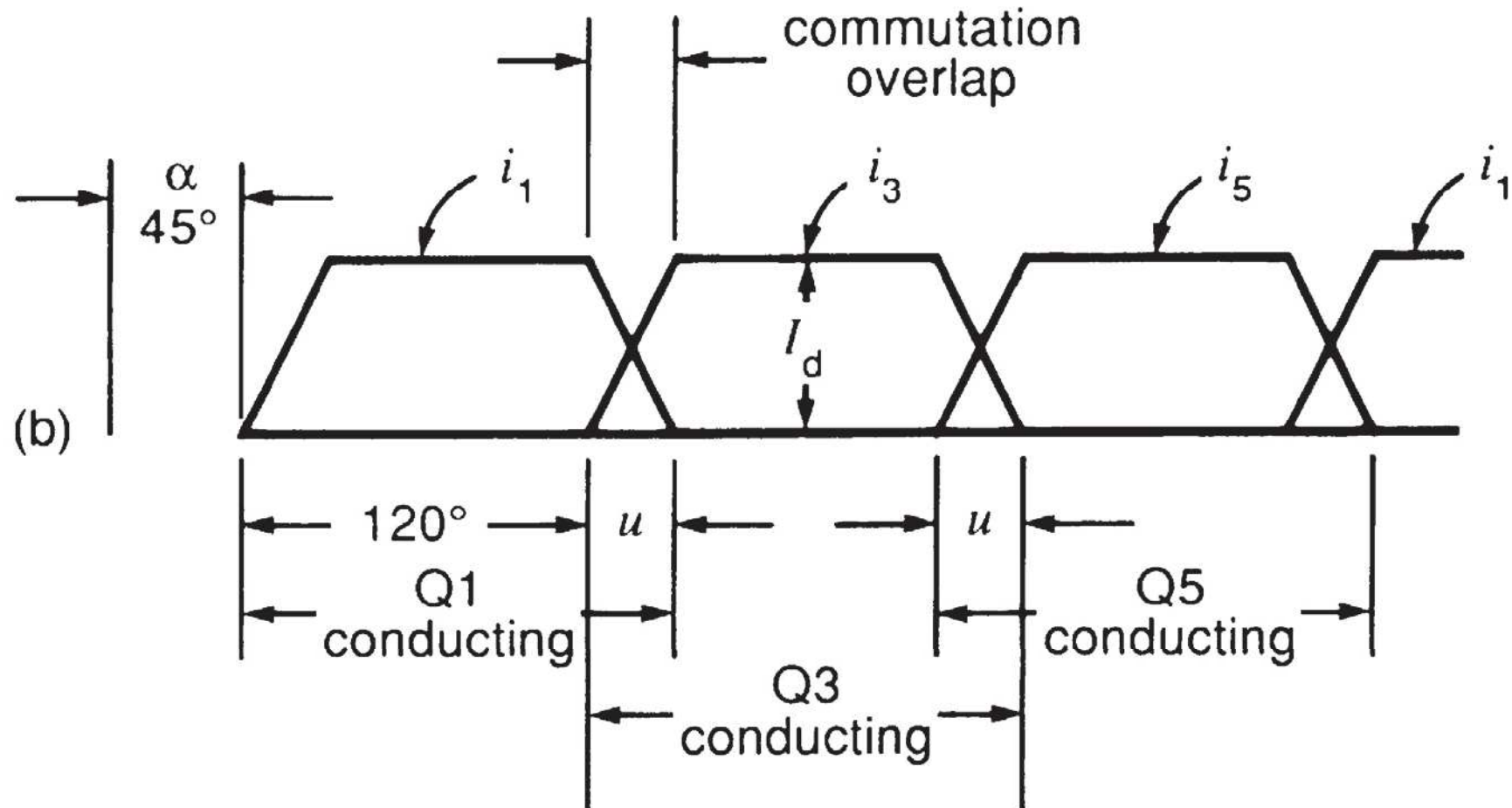


Figure 21.50 Waveshape of i_1 in thyristor Q1 for a delay angle α . The extinction angle γ permits Q1 to establish its blocking ability before the critical angle of 300° is reached. At 300° the anode of Q1 becomes positive with respect to its cathode. The figure also shows the relationship between angles α , β , γ , and u .

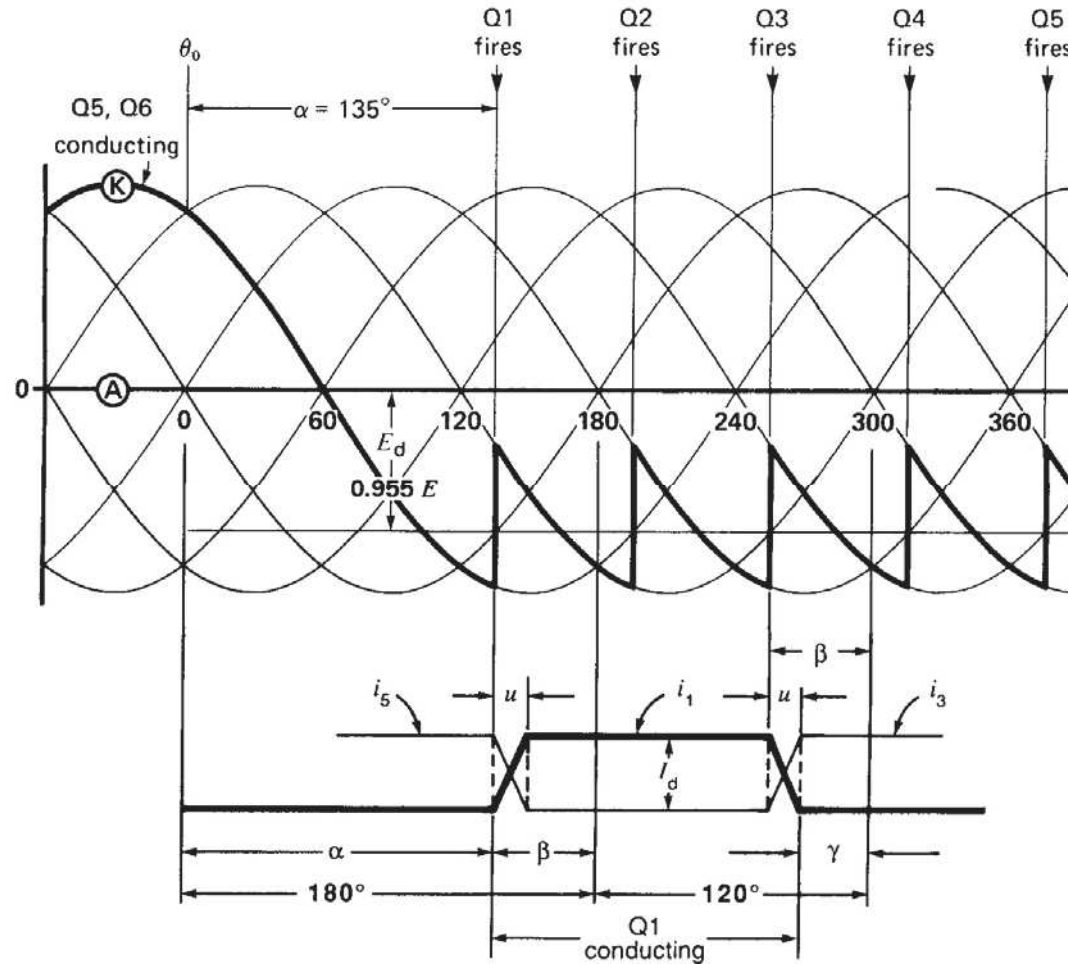


Figure 21.51 Typical properties and approximate limits of GTOs and thyristors in the on and off states.

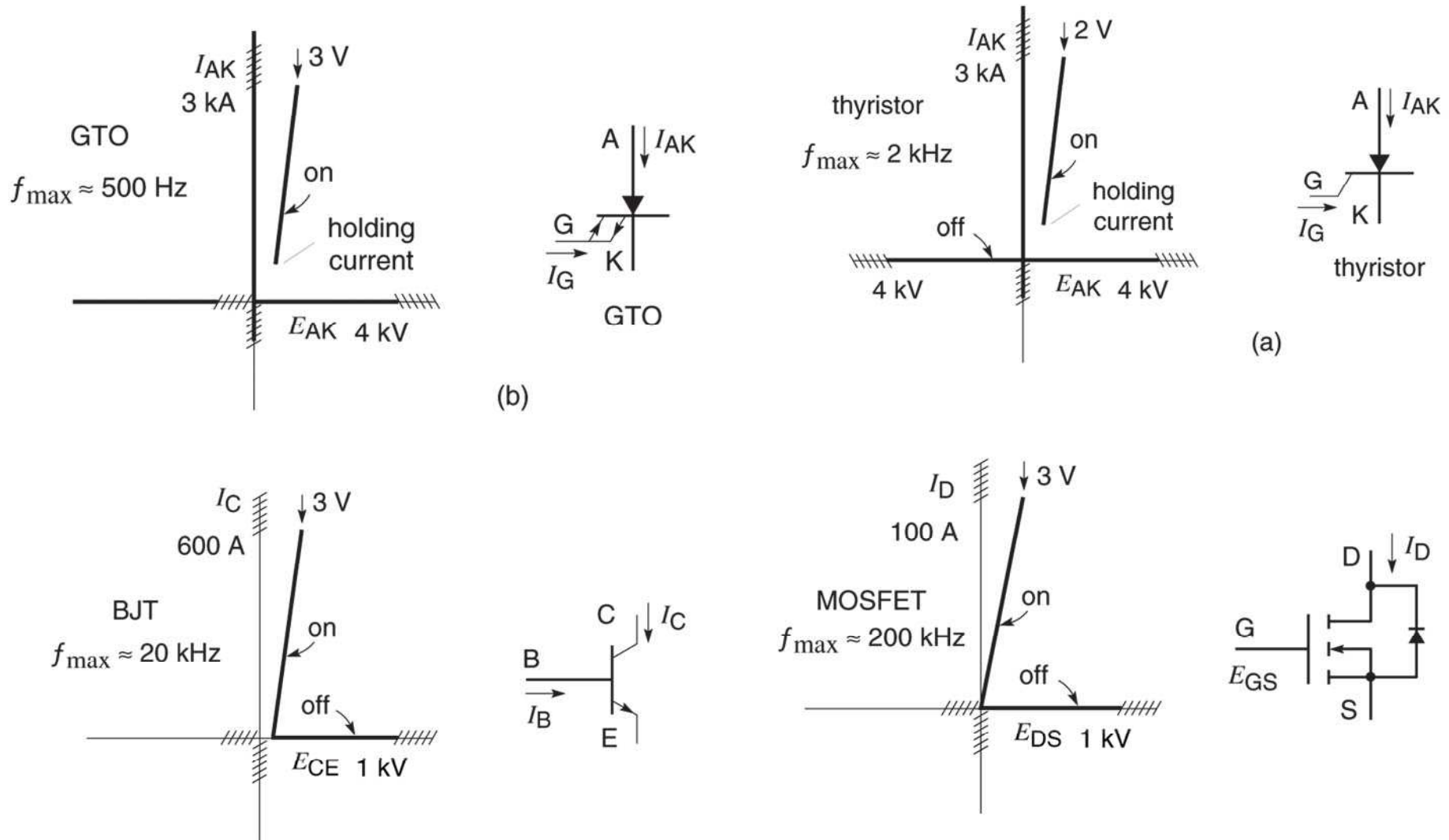
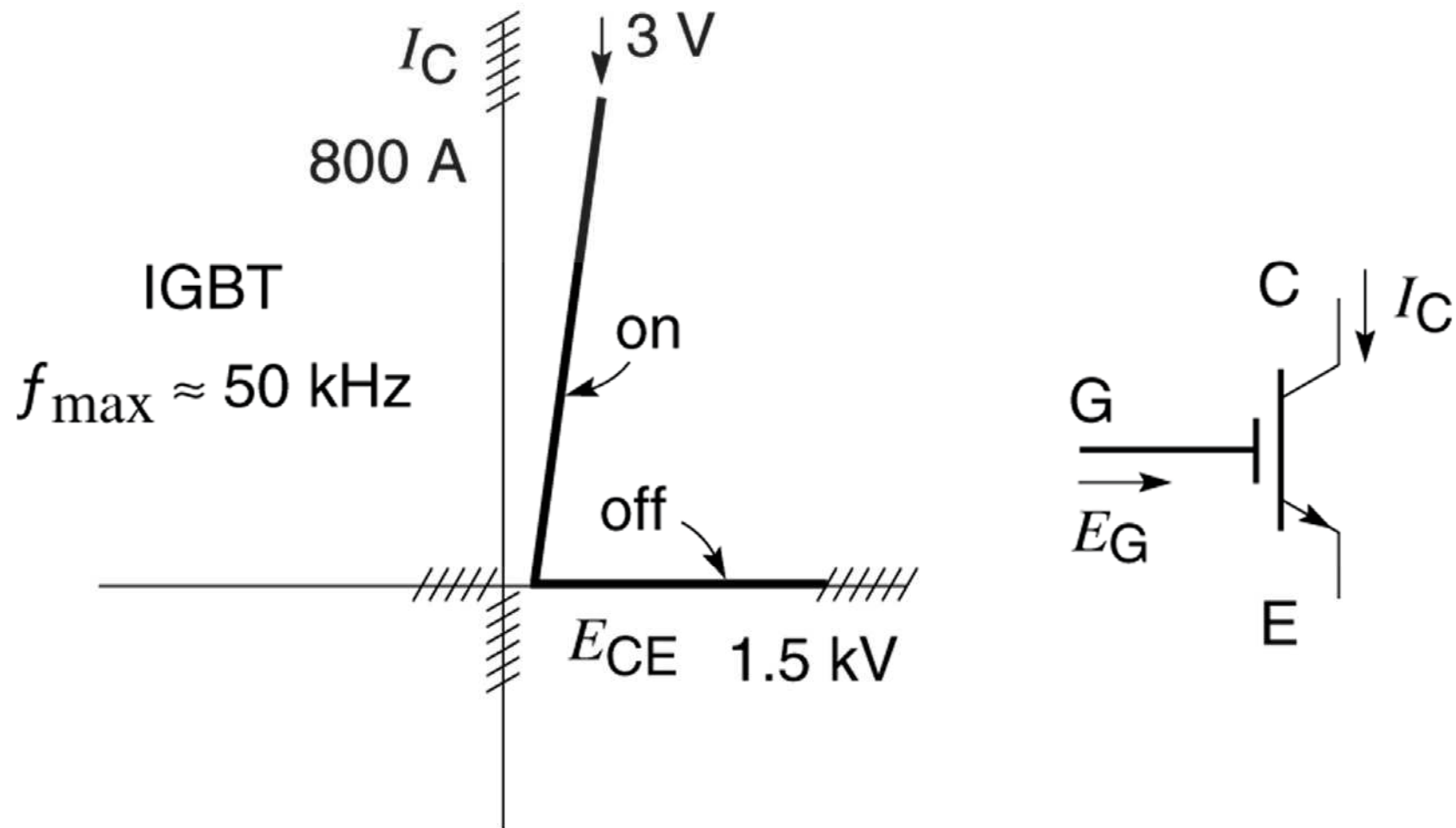


Figure 21.54 Typical properties and approximate limits of IGBTs.



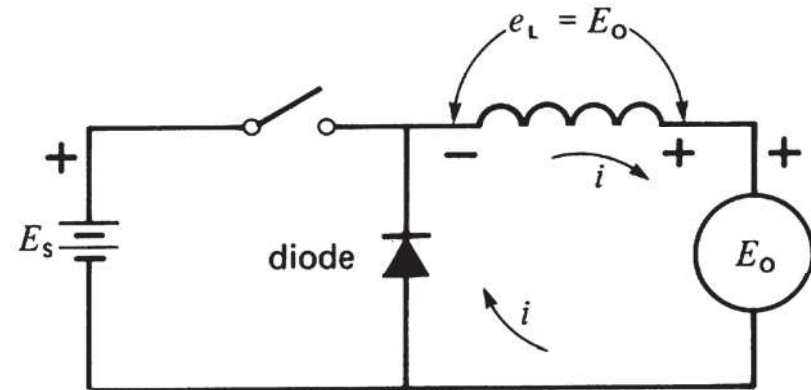
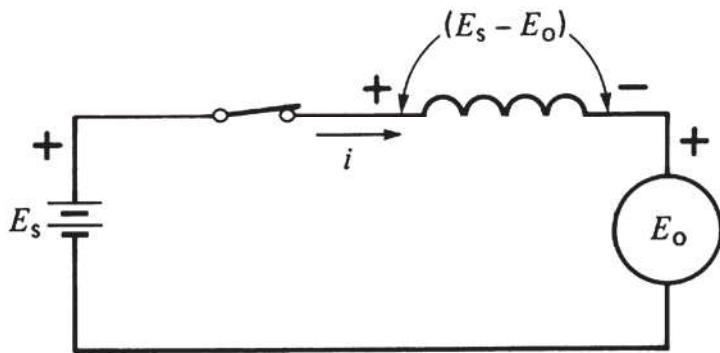
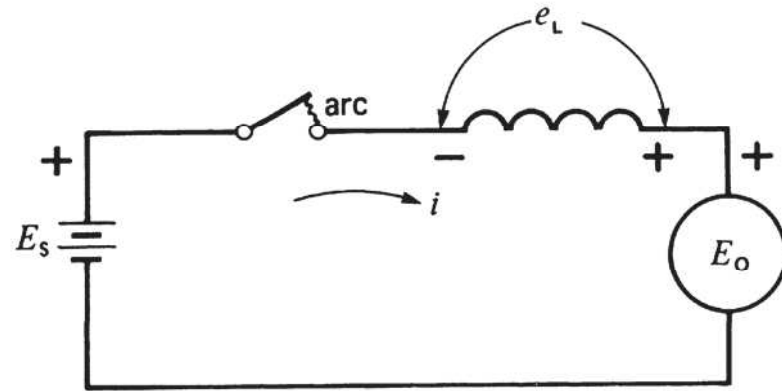
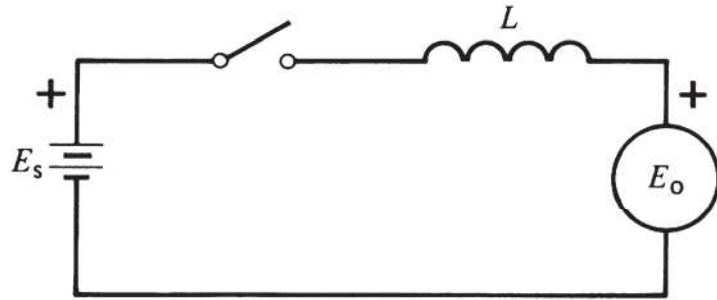
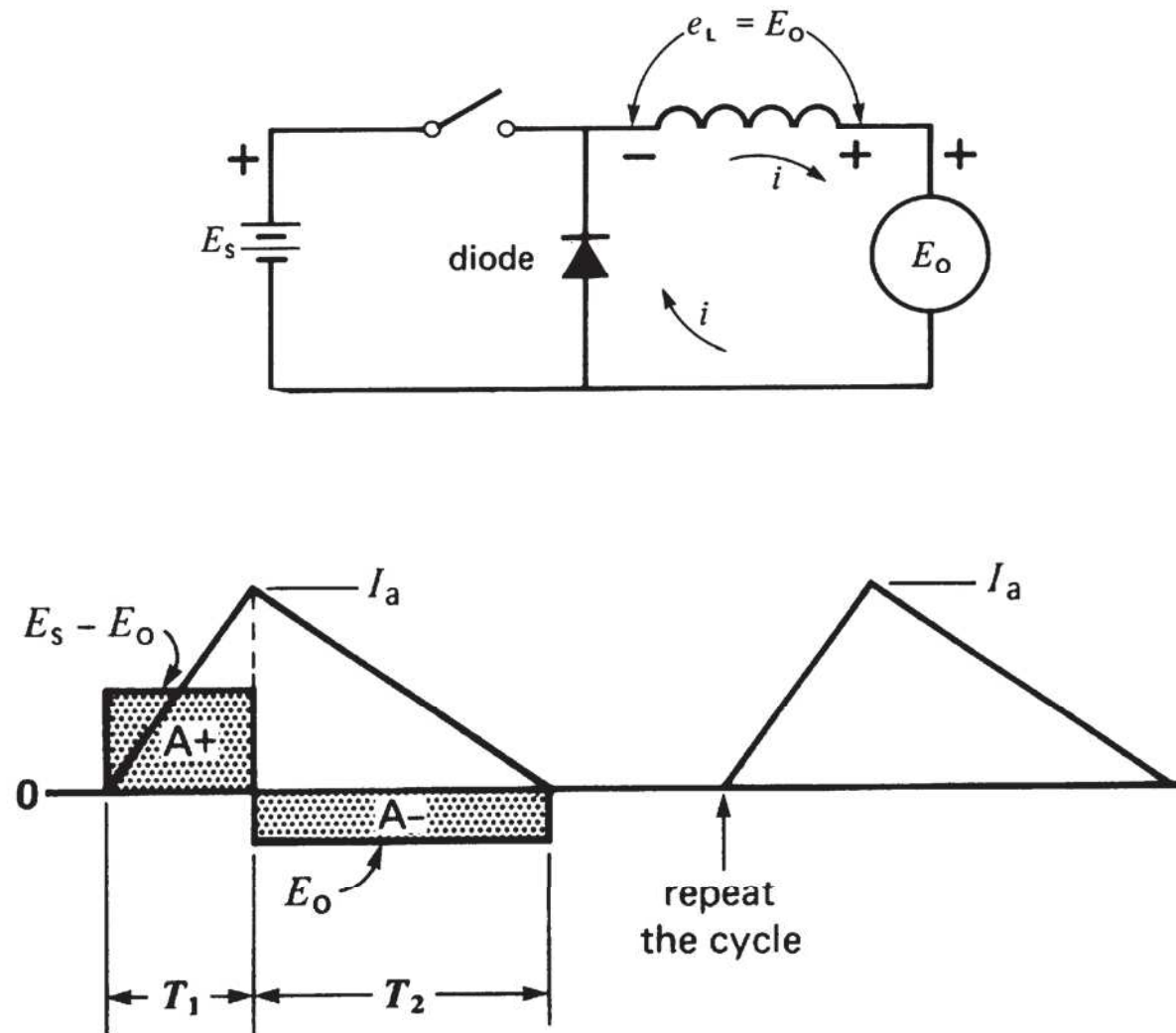
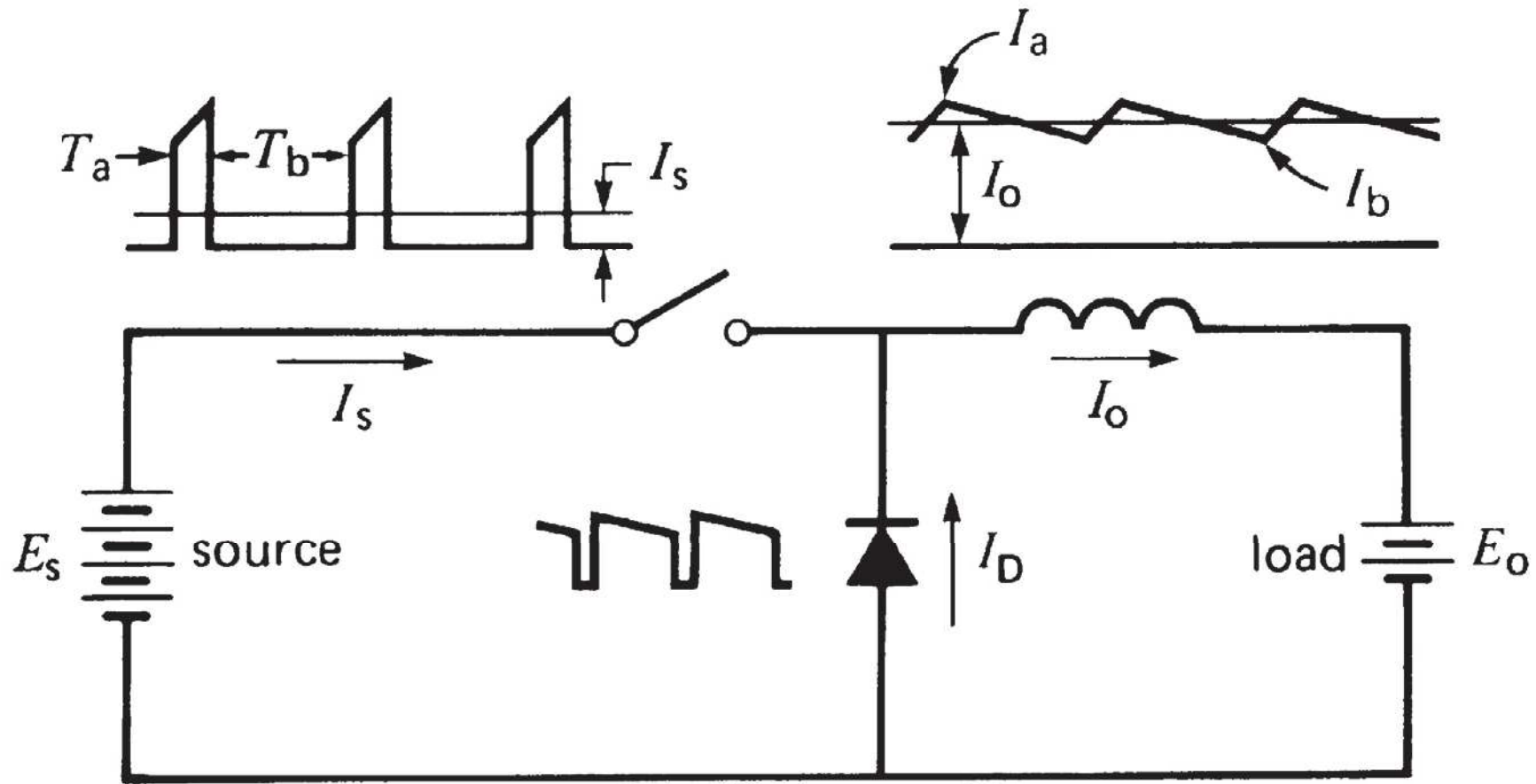


Figure 21.59 E and I in the inductor of Fig. 21.58.



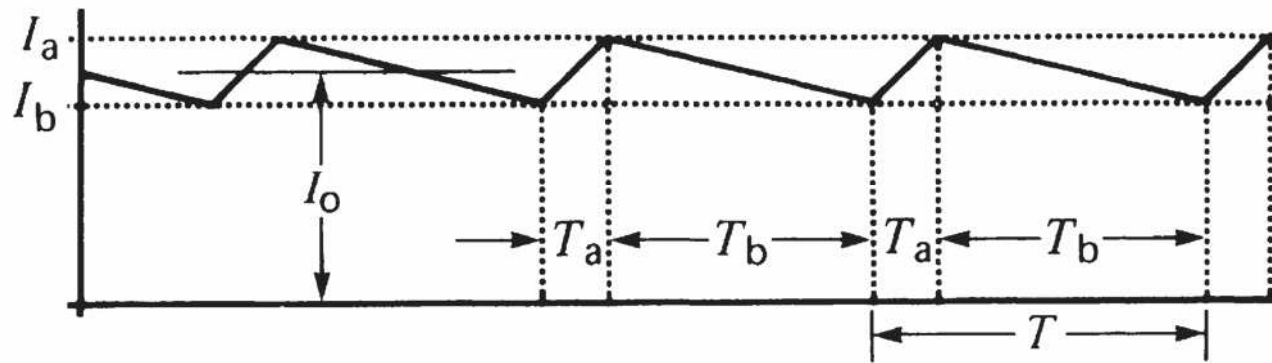


- $I_o = (I_a + I_b)/2$

- $I_s = I_o (T_a/T)$

- $I_s = I_o D$

Figure 21.60b Current in the load



- $E_s I_s = E_o I_o$

- $E_o = E_s I_s / I_o$

- $E_o = D E_s$

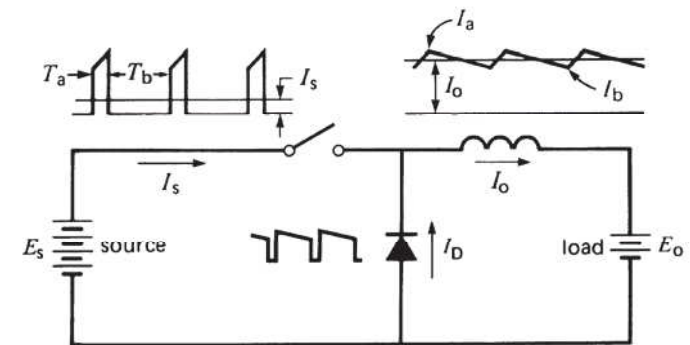
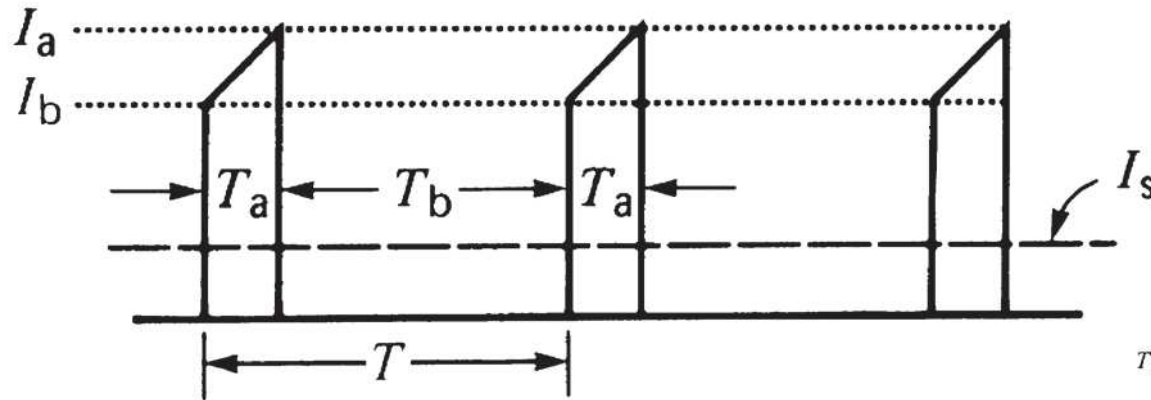
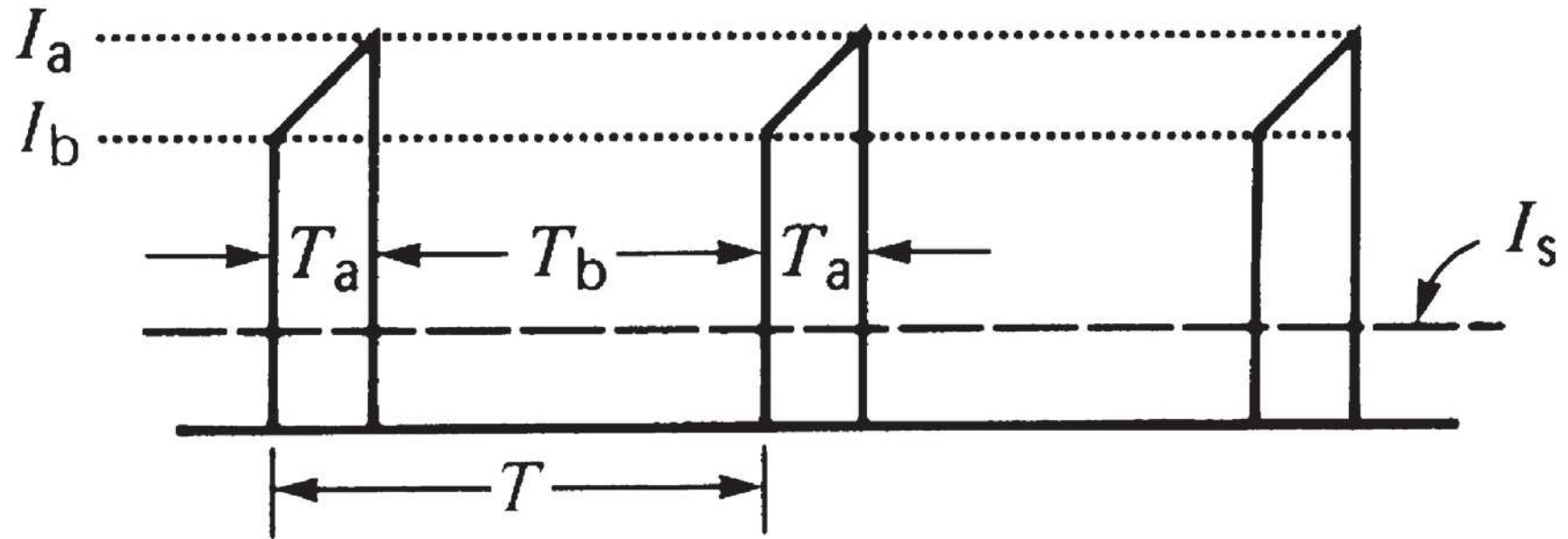


Figure 21.60c Current pulses provided by the source.



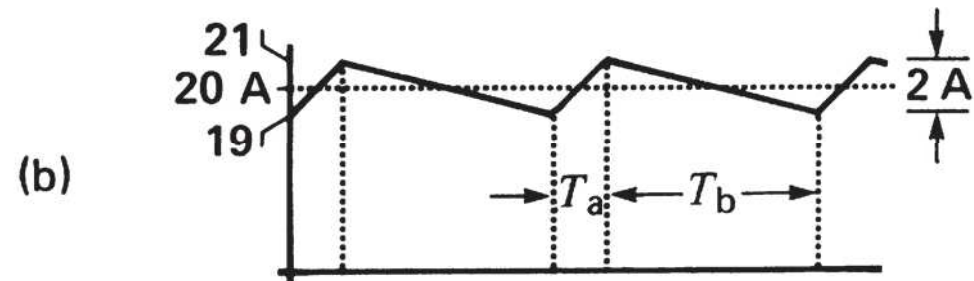
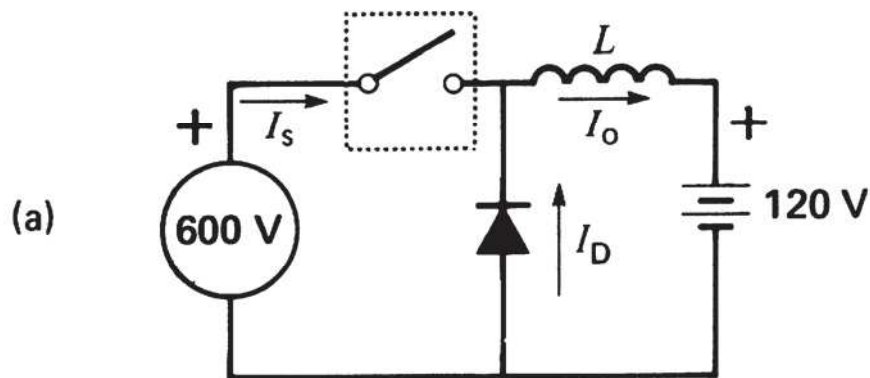
Example 21-11

Charge 120 V battery from 600 V dc source using a dc chopper, average current 20 A, ripple 2 A, $f = 200\text{Hz}$

- dc current from the source
- dc current in the diode
- the duty cycle
- inductance of the inductor

- $P = E_o I_o$

- $I_s = P / E_s$



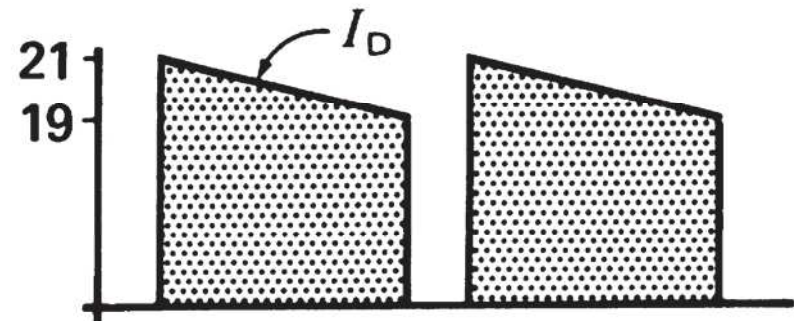
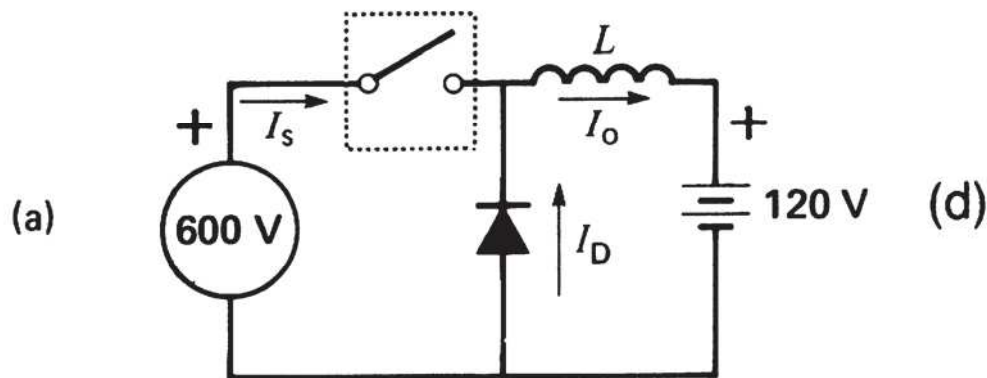
Example 21-11

Charge 120 V battery from 600 V dc source using a dc chopper, average current 20 A, ripple 2 A, $f = 200\text{Hz}$

- dc current from the source
- dc current in the diode
- the duty cycle
- inductance of the inductor

- $I_D = I_o - I_s$

- $D = E_o / E_s$

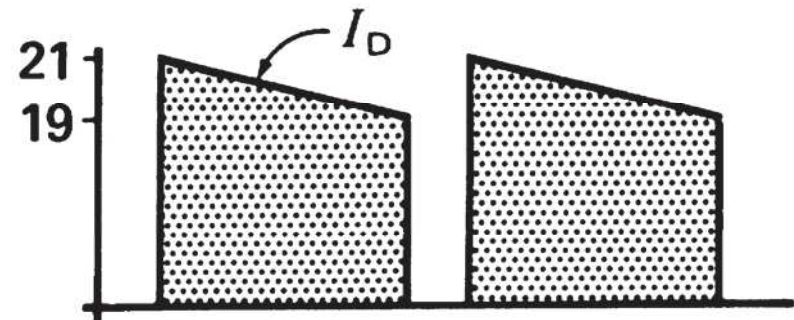
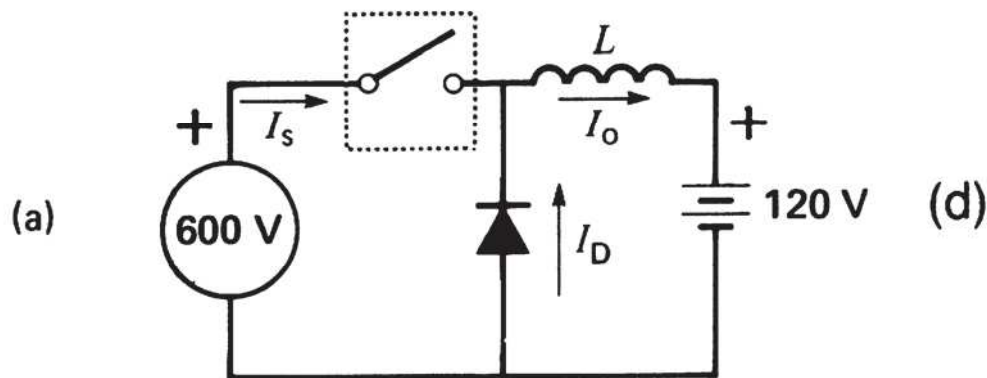


Example 21-11

Charge 120 V battery from 600 V dc source using a dc chopper, average current 20 A, ripple 2 A, $f = 200\text{Hz}$

- dc current from the source
- dc current in the diode
- the duty cycle
- inductance of the inductor

- $I_D = I_o - I_s$
- $D = E_o / E_s$



2 quadrant DC-DC converter

- $E_L = D E_H$

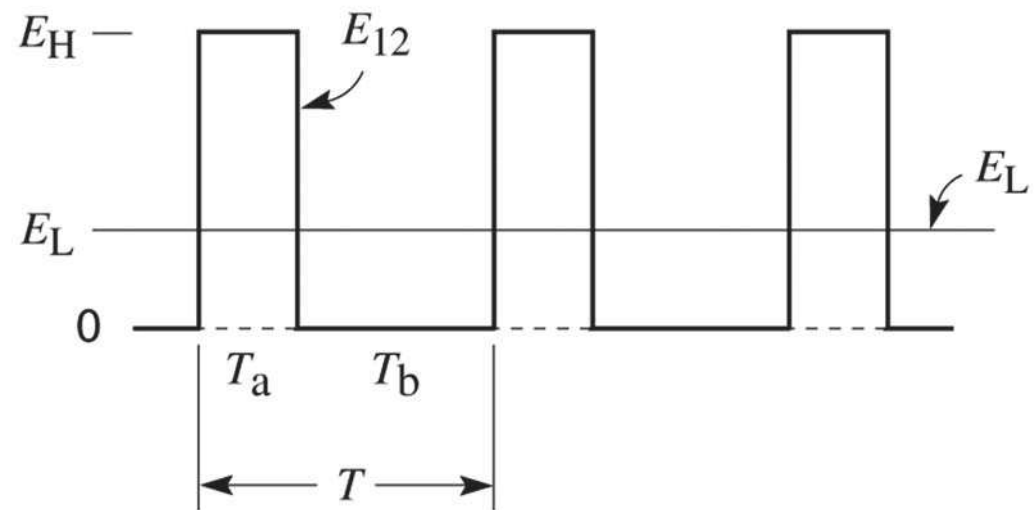
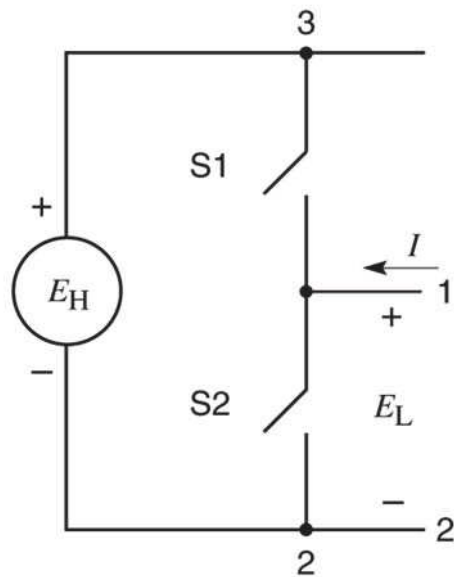
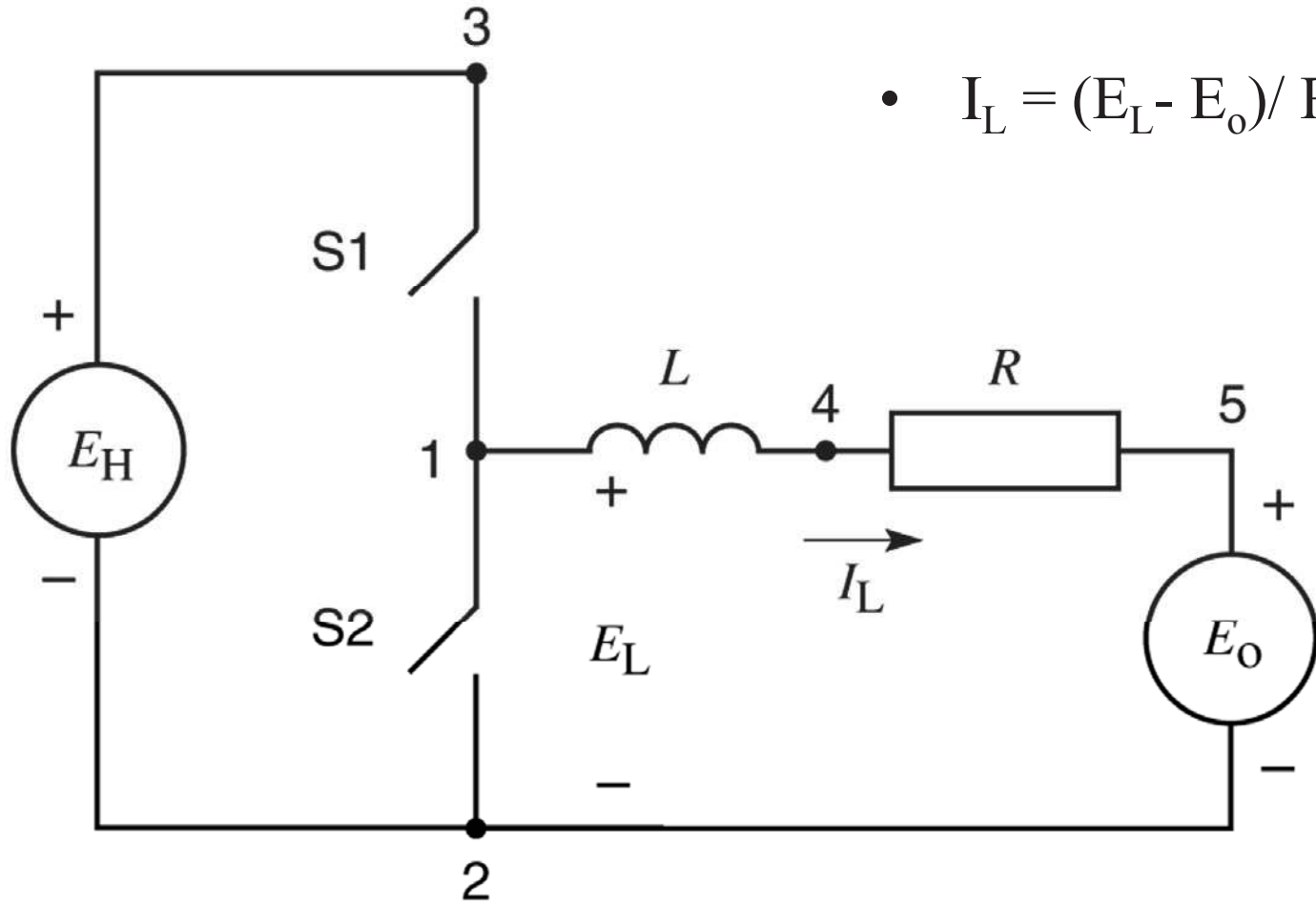


Figure 21.64 Power can flow from E_H to E_O and vice versa.

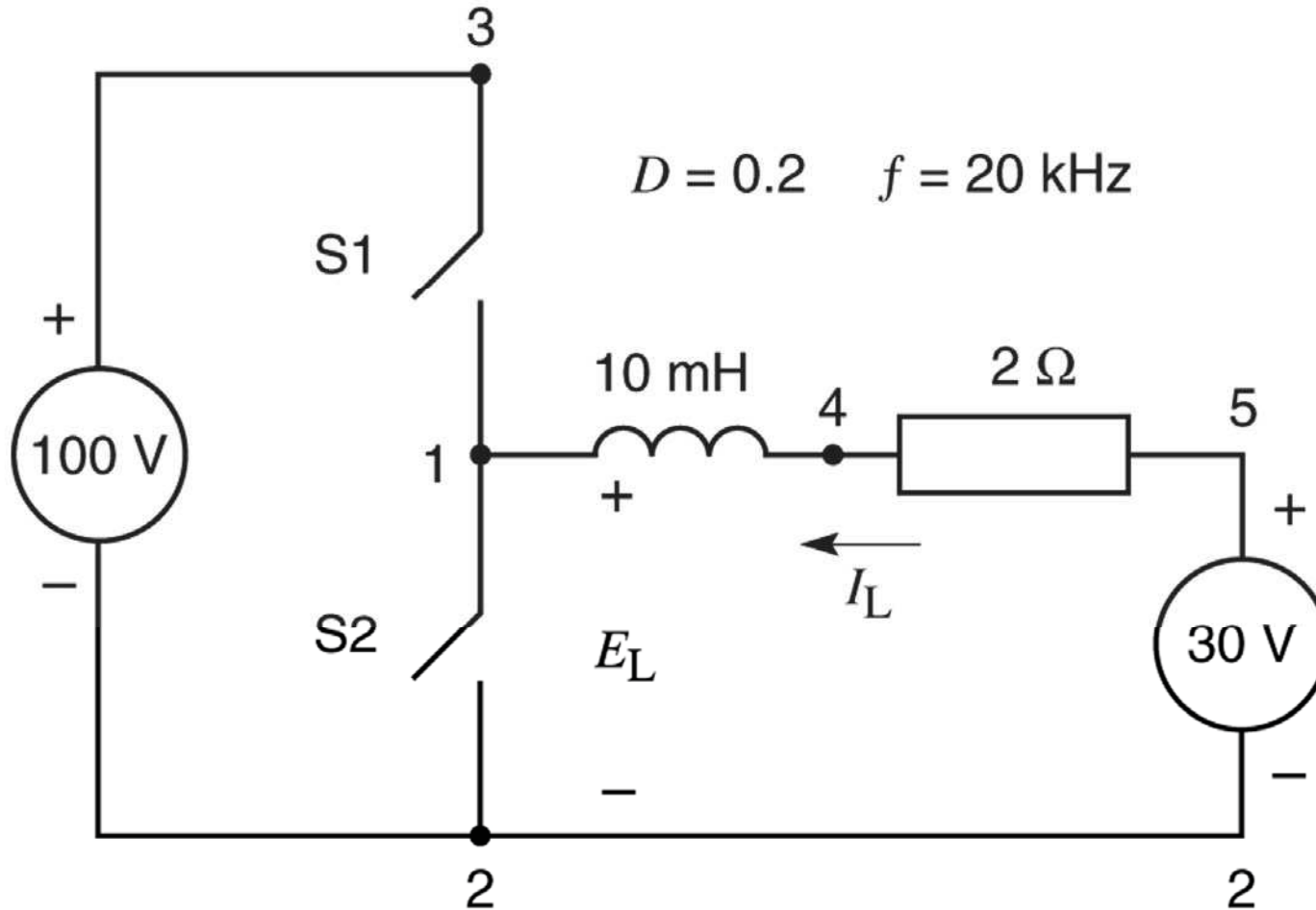
$$E_L > E_O$$



- $I_L = (E_L - E_O) / R$

Figure 21.65 Circuit of Example 21-13.

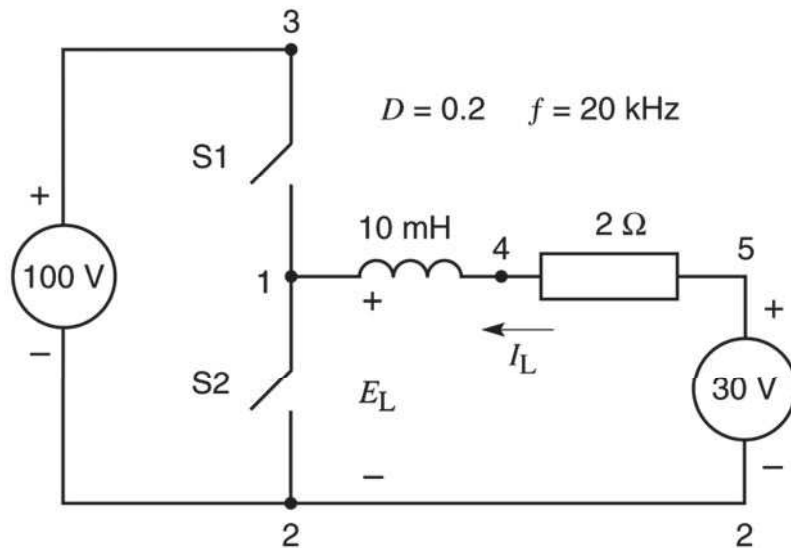
$$E_L < E_0$$



Example 21-13.

100 V, 30 V, S ohm, 10 mH, 20 kHz, $D=0,2$

Value and direction of I_L
Pp ripple



- $E_L = D E_H = 20\text{V}$
- $I_L = (E_o - E_L) / R$
- $T = 1/f$

Figure 21.66 See Example 21-13.

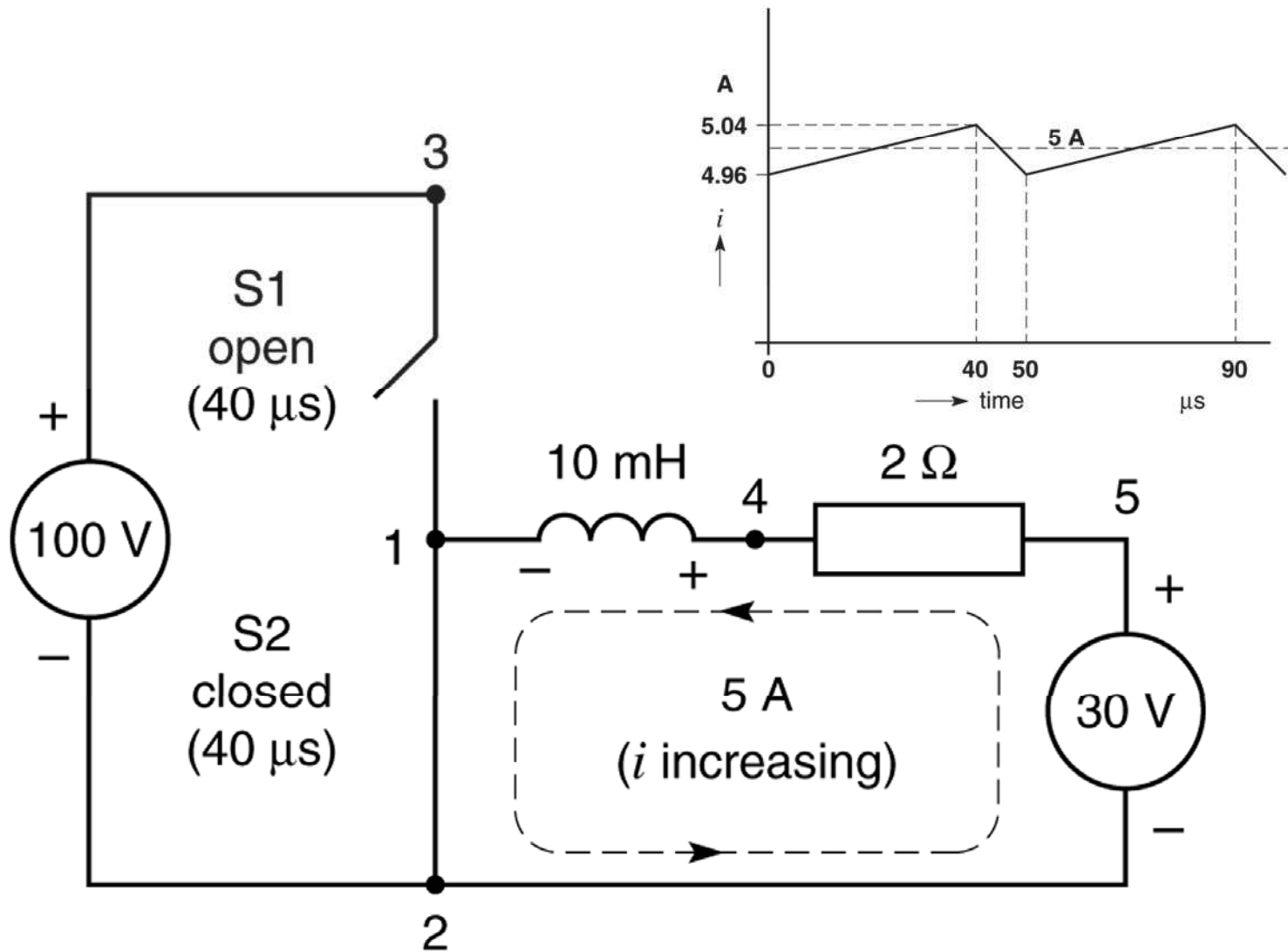


Figure 21.67 See Example 21-13.

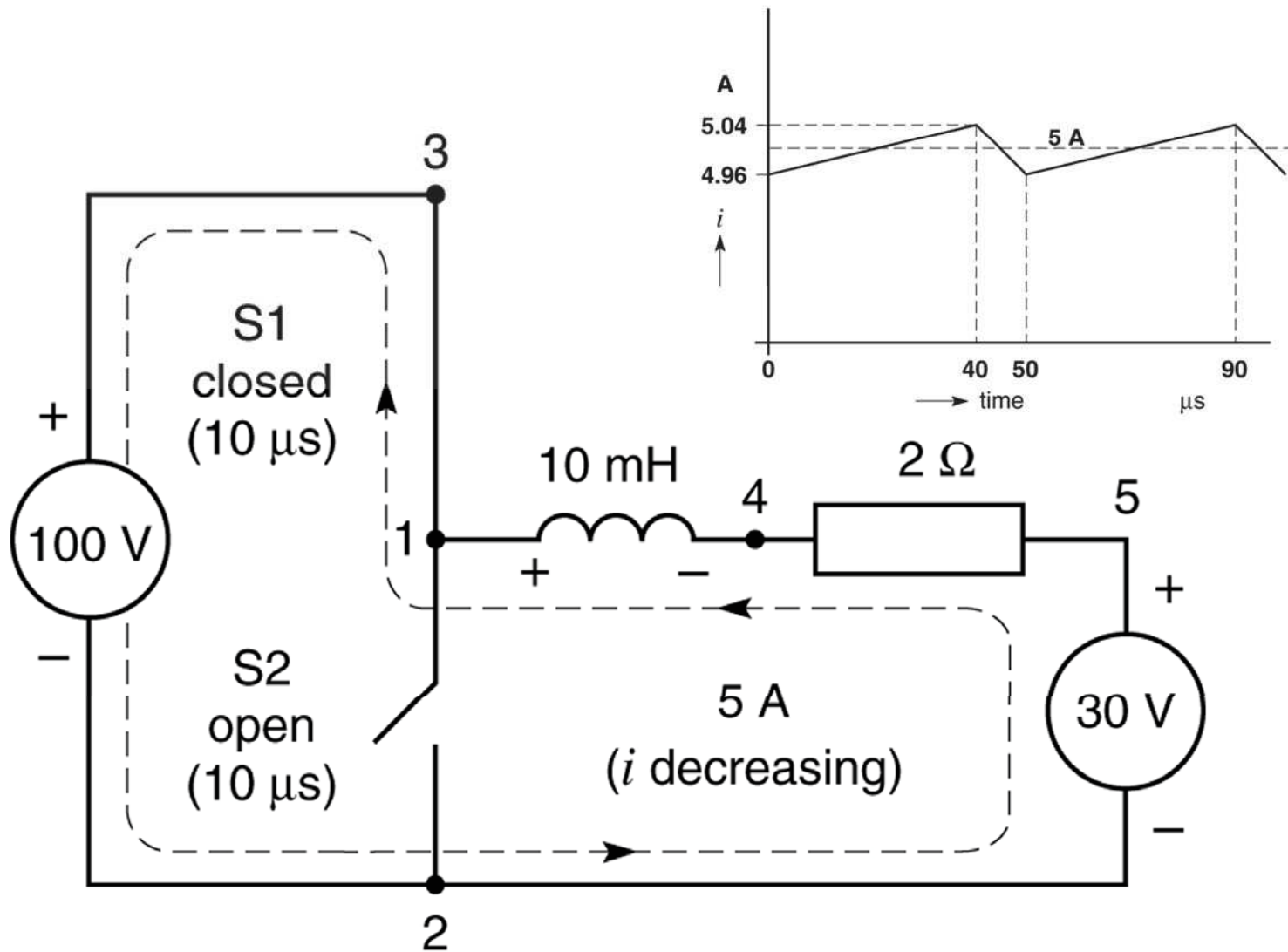


Figure 21.69 Two-quadrant electronic converter.

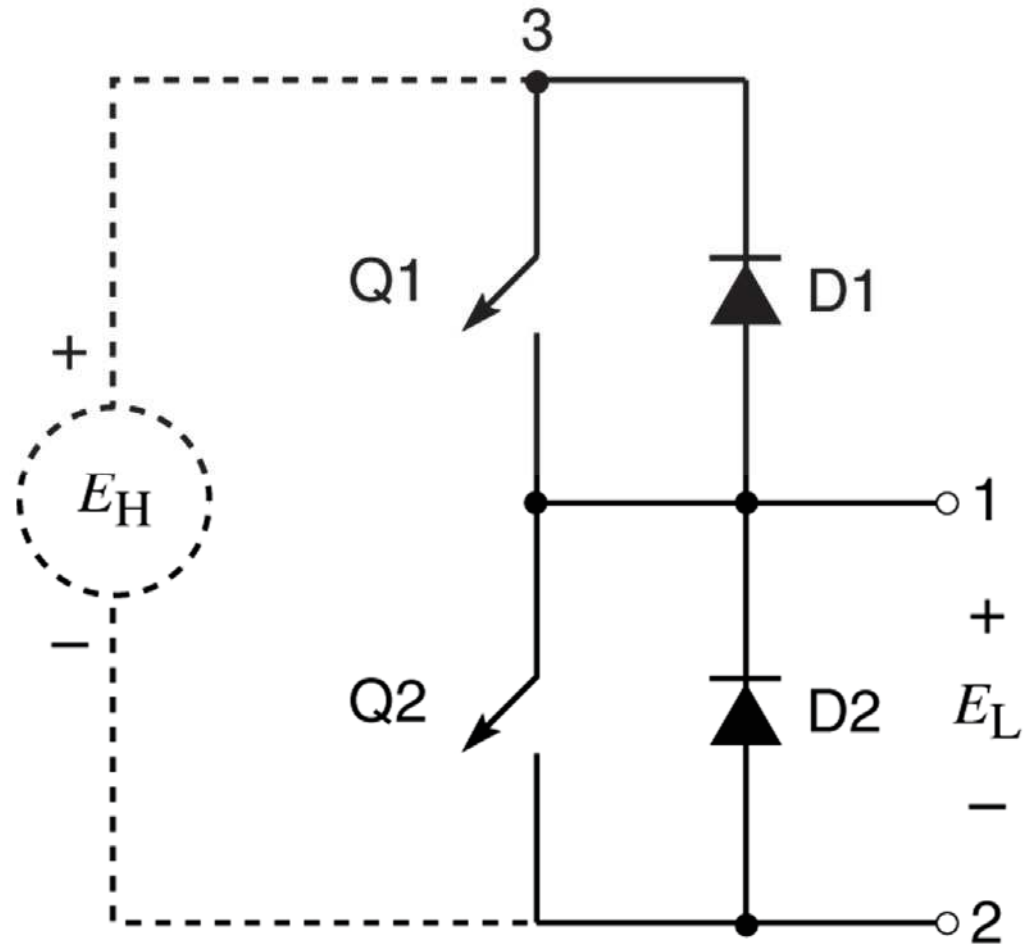
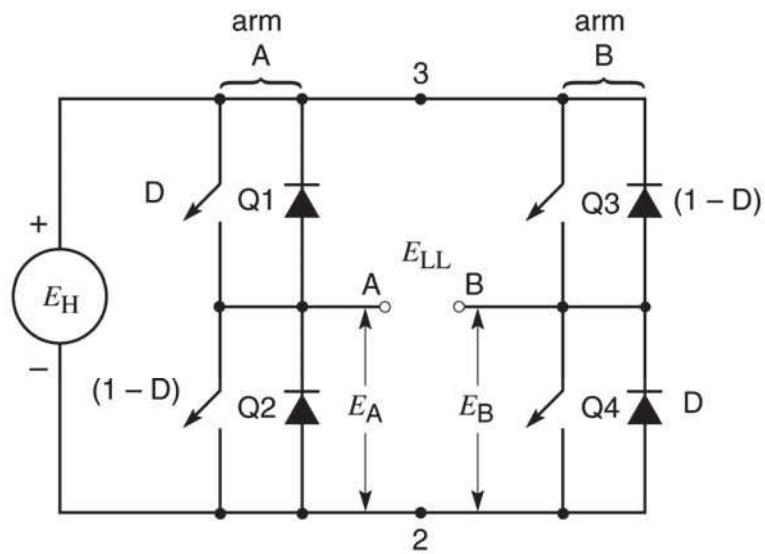


Figure 21.70 Four-quadrant dc-to-dc converter.



- $E_L = D E_H = 20V$

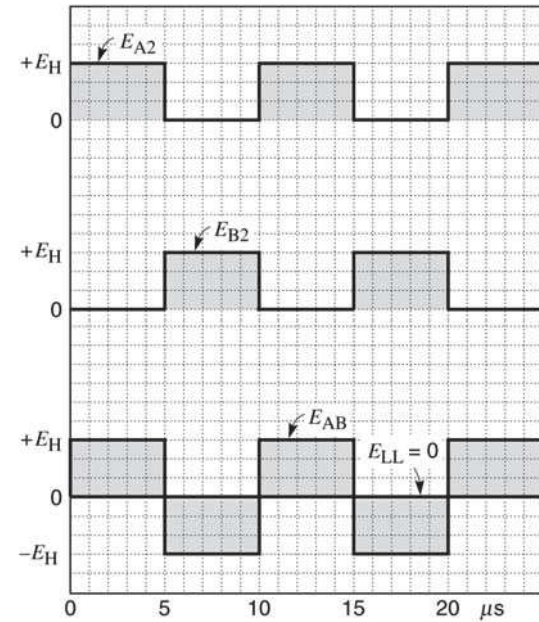
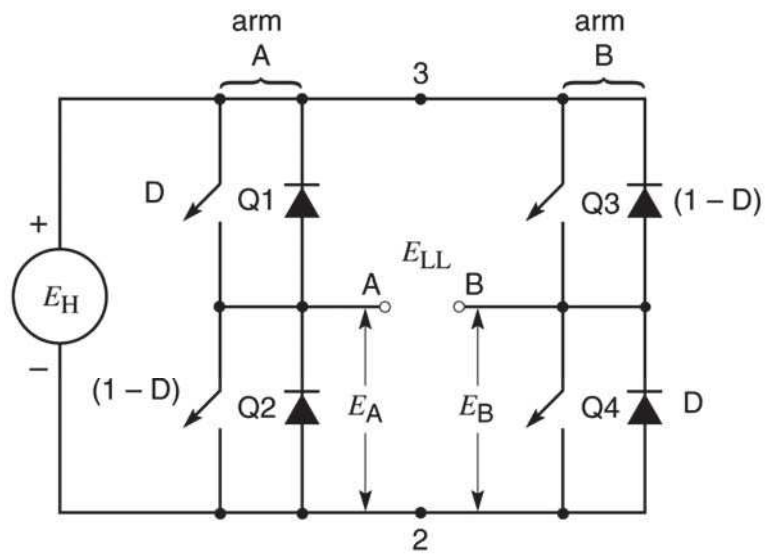


Figure 21.70 Four-quadrant dc-to-dc converter.



- $E_{LL} = E_H (2D-1)$

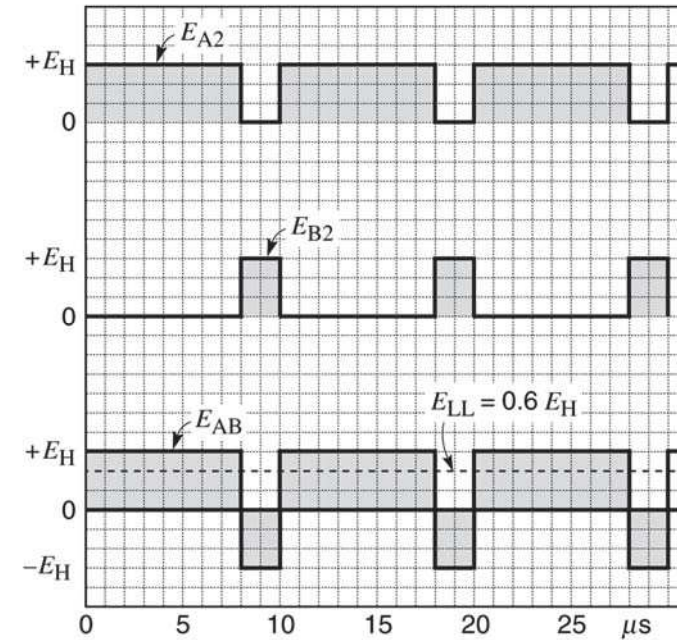


Figure 21.73 Four-quadrant dc-to-dc converter feeding a passive dc load R .

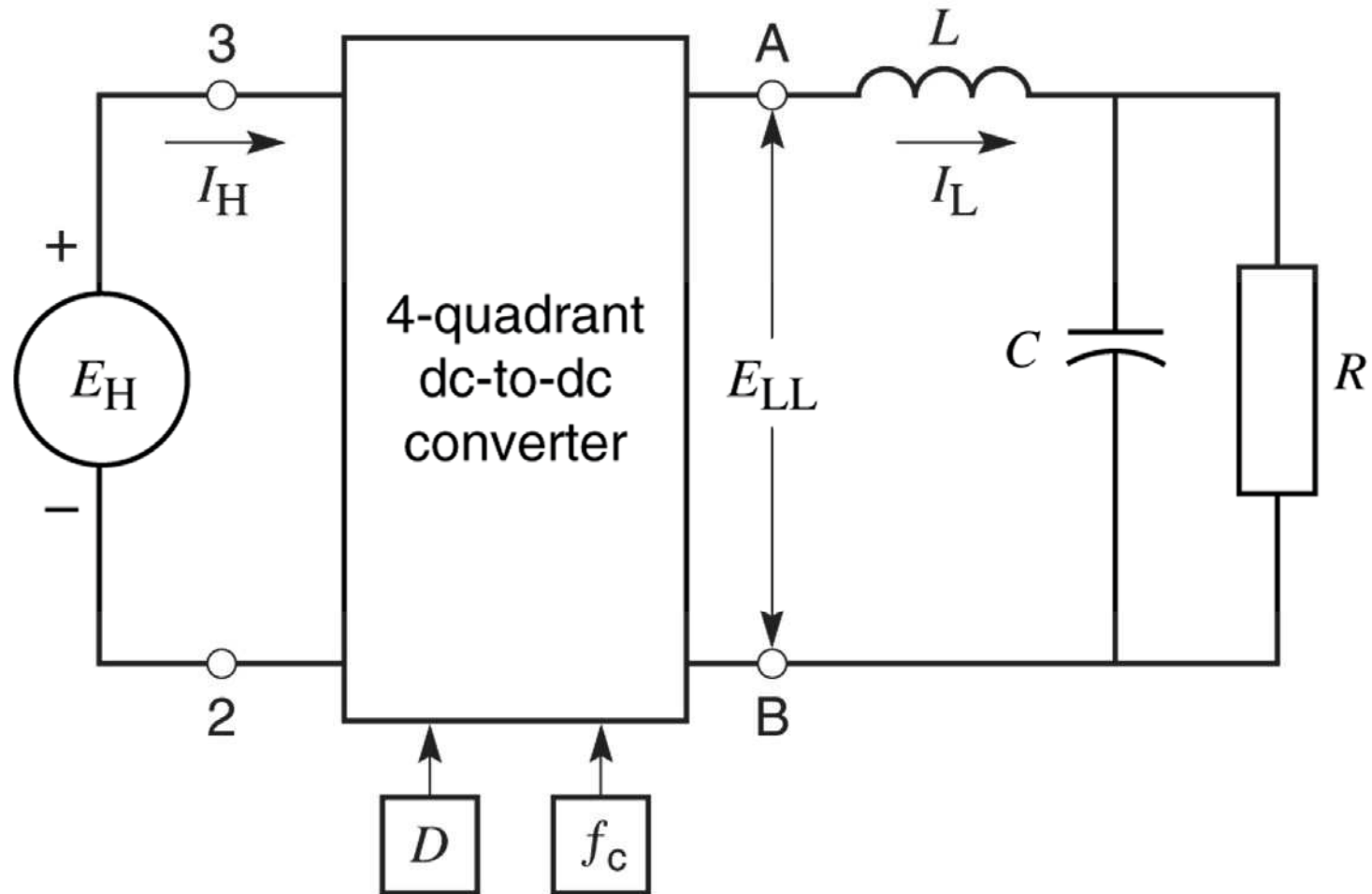


Figure 21.74 Four-quadrant dc-to-dc converter feeding an active dc source/sink E_o .

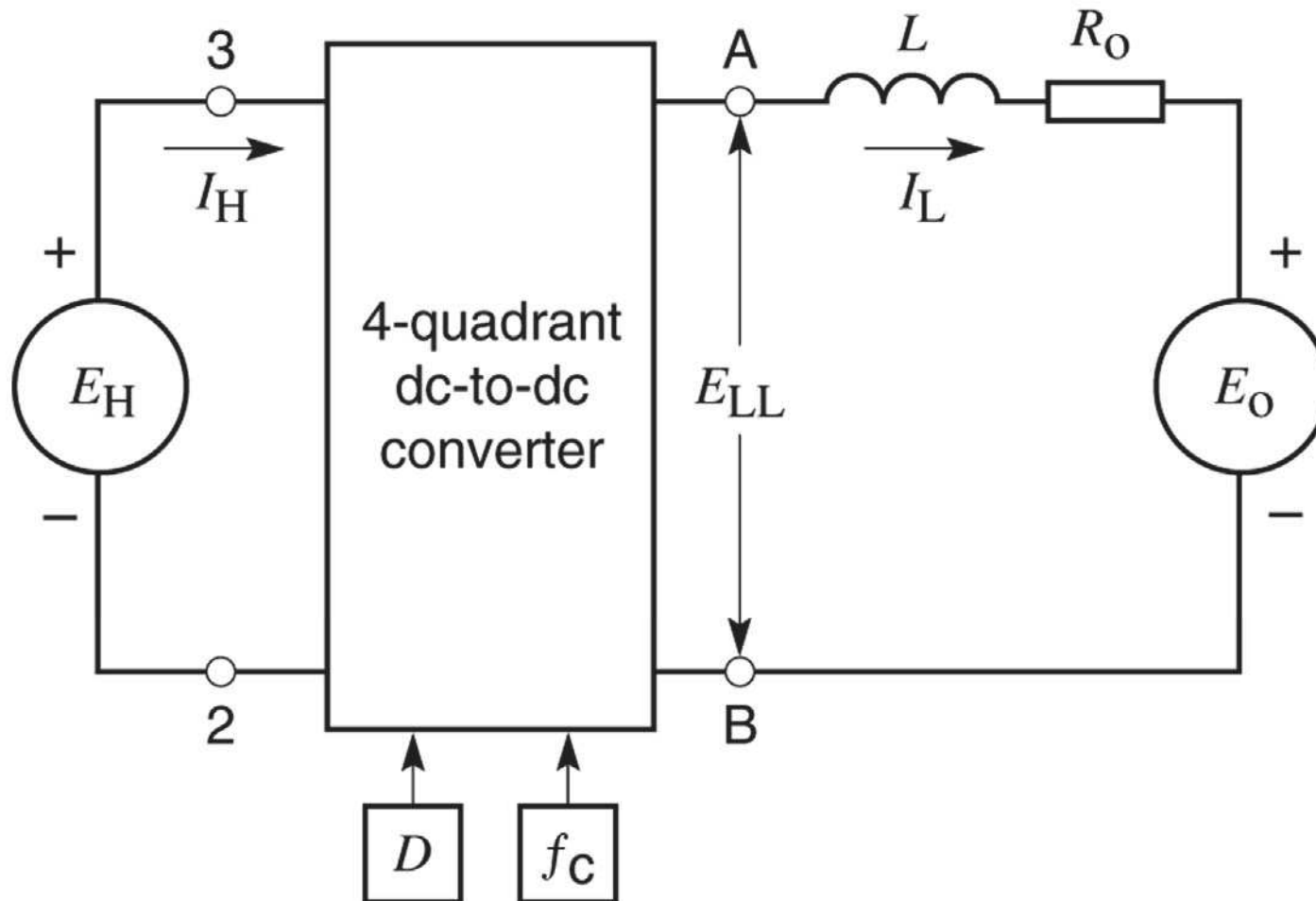
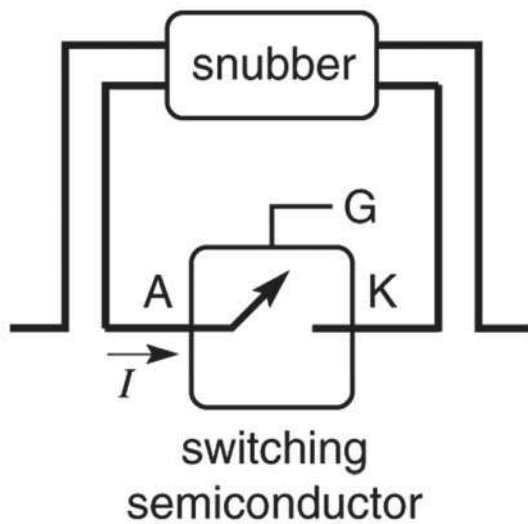


Figure 21.75a Switching semiconductor and snubber.



T_1 = turn-on time

T_2 = on-state time

T_3 = turn-off time

T_4 = off-state time

$$D = \text{duty cycle} = \frac{T_2}{T}$$

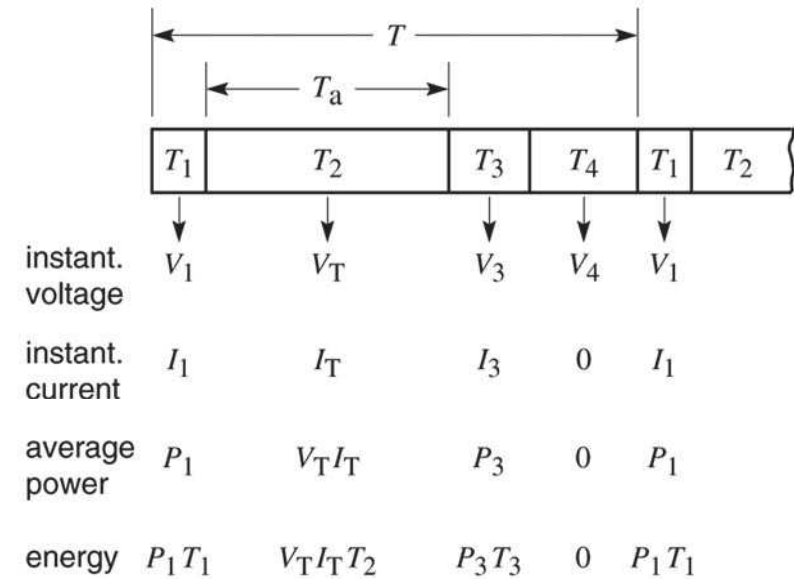


Figure 21.76a The square wave contains a fundamental sinusoidal component.

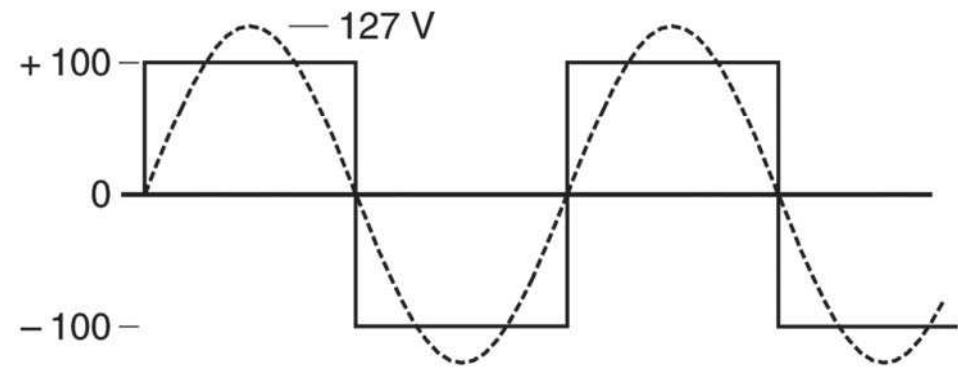
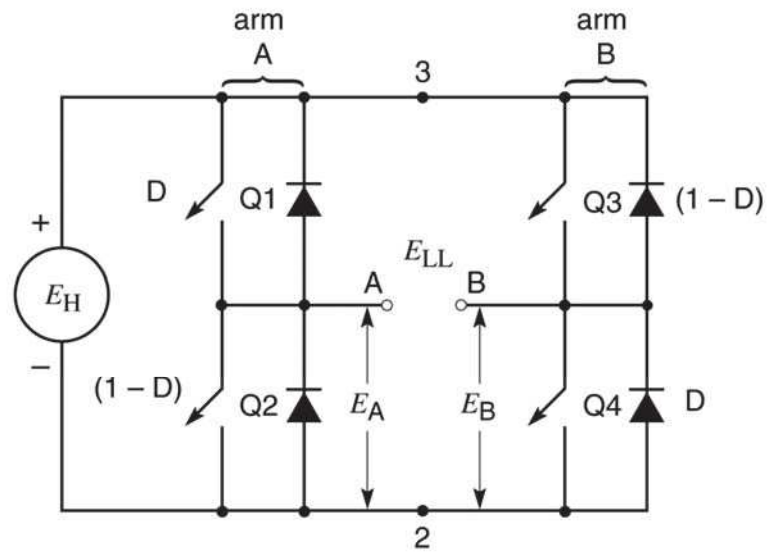


Figure 21.76b Single-phase dc-to-ac switching converter in which $D = 0.5$ and f can be varied.

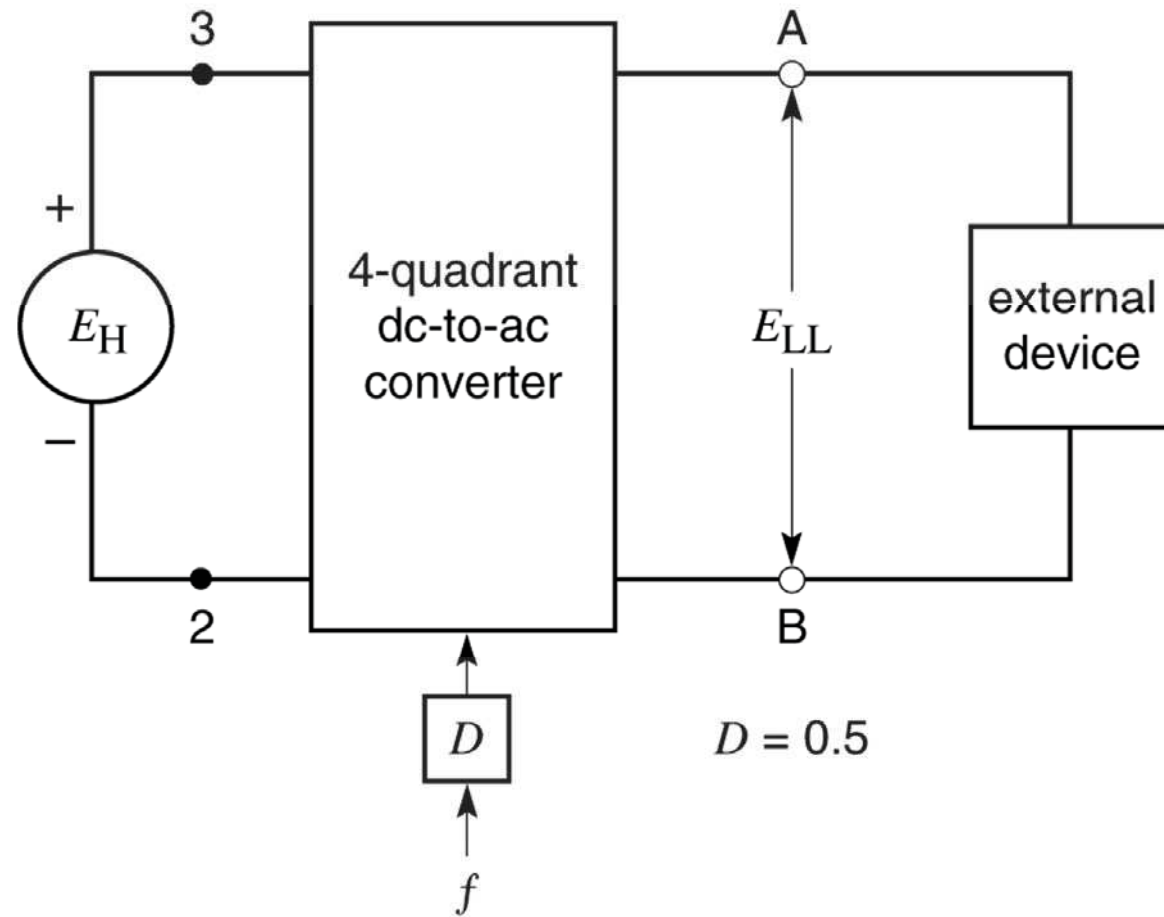
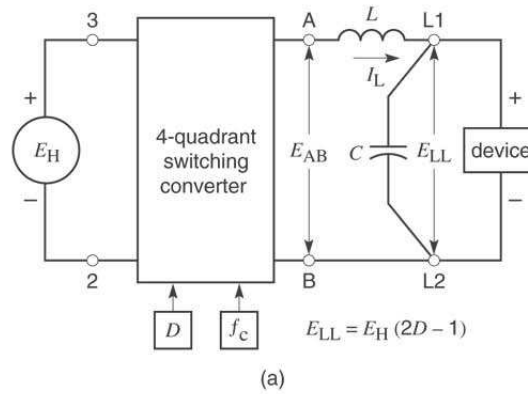


Figure 21.77 Four-quadrant dc-to-ac switching converter



- $E_{LL} = E_H (2D - 1)$

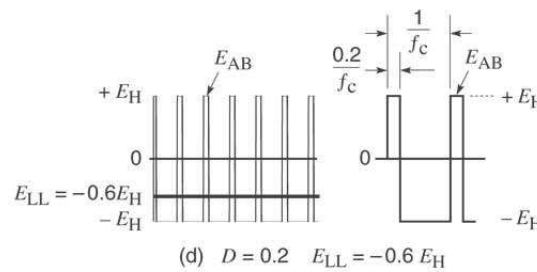
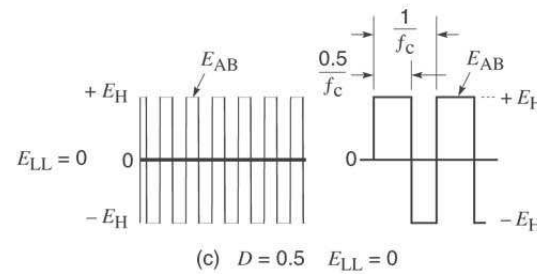
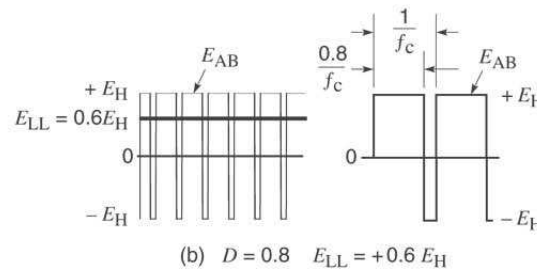


Figure 21.78 Frequency and amplitude control by varying D .

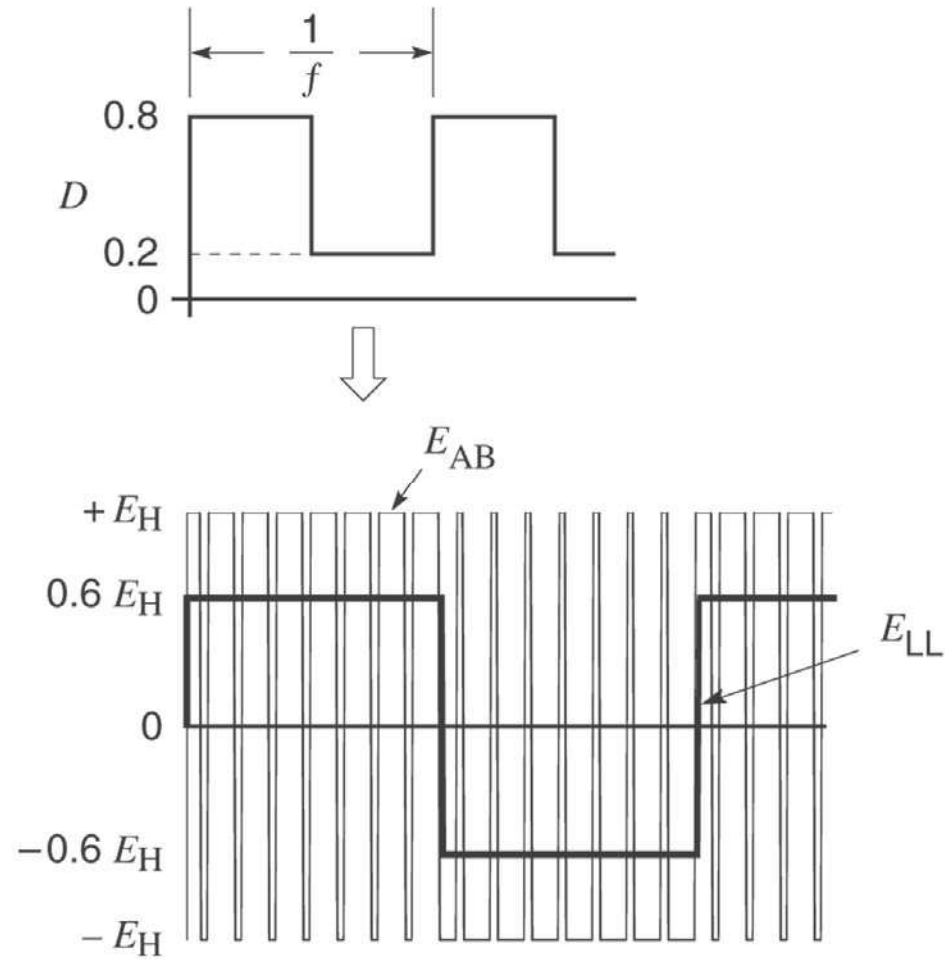


Figure 21.79 Frequency, amplitude, and phase control by varying D .

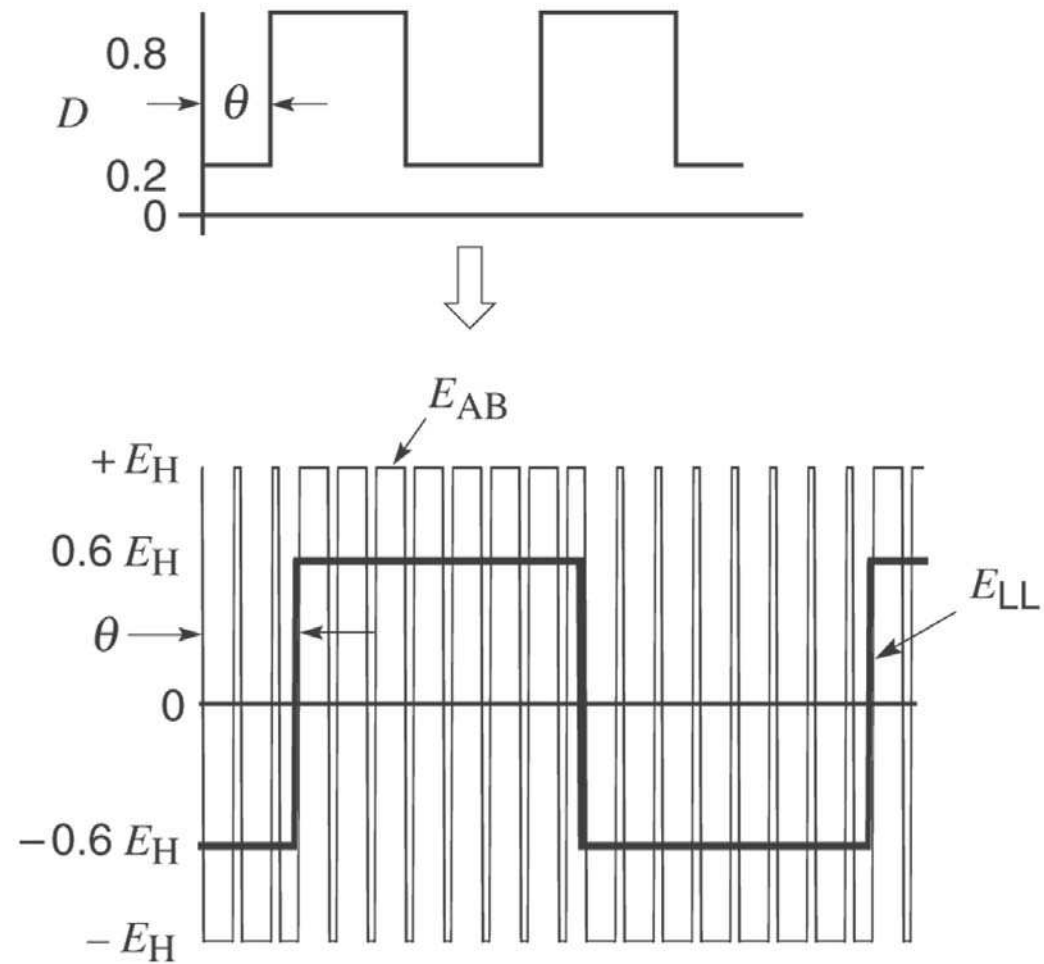


Figure 21.80 Waveshape control by varying D .

