Exam Analog Integrated Circuit Design (ET 4252) August 30, 2007 14:00-17:00h

This exam consists of three main questions. Please start on a new sheet of paper for each main question.

You are allowed to use a calculator and one piece of A4-sized paper with handwritten, non-copied personal notes.

Prefixes:

I ICHACS.		
Giga	(G)	$= 10^{9}$
Mega	(M)	$=10^{6}$
kilo	(k)	$=10^{3}$
milli	(m)	$= 10^{-3}$
micro	(μ)	$= 10^{-6}$
nano	(n)	$= 10^{-9}$
pico	(p)	$= 10^{-12}$
femto	(f)	$= 10^{-15}$
atto	(a)	$= 10^{-18}$

 $k = 1.38 \cdot 10^{-23}$ J/K (Boltzmann's constant) $q = 1.60 \cdot 10^{-19}$ C (elementary charge) $V_T = \frac{kT}{q} = 25.9$ mV at T = 300K

Do not forget to put your name and study number on all material you hand in. And please turn off your mobile phone.

Good luck!

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Question 1: Design of a Voltage-Controlled Oscillator (VCO) for an Impulse-Radio Ultra-Wideband (UWB) Quadrature Downconverter

A negative resistance LC voltage-controlled oscillator is shown in Fig. 1.



Figure 1: LC voltage-controlled oscillator.

The oscillator consists of a resonating LC tank, a cross-coupled transconductance amplifier (Q_1 and Q_2), and a bias current source (Q_{CS}). *L* stands for the tank inductance, Q_L for its quality factor, C_V for the varactor capacitance, Q_C for its quality factor, *C* for the additional tank capacitance ($C=C_V$ at the oscillation central frequency) with a quality factor $Q=2Q_C$, and I_{TAIL} for the bias tail current. For the bias resistor *R* it holds: R >> 1.

Determine the circuit parameter values of this oscillator in order to meet the requirements of the impulse-radio UWB quadrature downconverter.

The oscillator requirements for the impulse-radio UWB quadrature downconverter are:

- oscillation central frequency of 5.7GHz
- phase noise better than -80dBc/Hz at 1MHz offset from the oscillation central frequency
- peak amplitude of a differential oscillation voltage signal across the LC-tank around 400 mV
- power consumption drawn from a supply voltage of V_{CC} =1.8V as low as possible

For a silicon technology chosen, inductors with quality factors of 30 and varactors with quality factors of 40 are available. The noise factor of the oscillator active part equals A=4.

Provide the following:

- a) (5%) Derived expression for the LC-tank impedance (Z) at an offset angular frequency ($\Delta \omega$) from the oscillation angular frequency without considering inductor and capacitor losses.
- b) (15%) Derived expression for the LC-tank conductance (G_{TK}) at the oscillation frequency (f_0) .
- c) (5%) Expression for the oscillation frequency and oscillation condition.
- d) (10%) Derived expression for the phase noise of the oscillator. Model the noise contribution of the LC-tank to the phase noise by its loss resistance (R_{TK}) , and the active part noise contribution by a factor AG_{TK} , A being its noise factor.
- e) (35%) Values of inductance L, varactor capacitance C_V , and tail current I_{TAIL} for the oscillator requirements at the central oscillation frequency, using the results obtained in a)-d).
- f) (15%) Values of minimum $(C_{V,MIN})$ and maximum $(C_{V,MAX})$ varactor capacitances to overcome the effects of 10% absolute tolerance on the inductors, varactors and capacitors used.
- g) (15%) Ways to reduce the power consumption (at the expense of phase noise, which is acceptable in this application) by changing the active circuit (not the LC-tank configuration).

Question 2: Translinear and biasing circuits

a) A bridge rectifier can be viewed as a translinear loop. Assuming identical diodes, what are the four diode current values I_1 , I_2 , I_3 and I_4 in the figure below?



b) Analyze the output current I_o in terms of the input currents I_1 and I_2 for the circuit below. All transistors are equivalent.



c) What restrictions hold for the magnitudes of the input currents I_1 , I_2 and I_o in the above circuit? Write them in the form of inequalities, such as $I_y > 0$.

We will now concentrate on the design of a current source that delivers I_1 . Assume its output current to be constant and equal to 2mA. Also, assume I_2 to be equal to 1mA.

- d) What is the load impedance of the current source, i.e., what is the value of the (low-frequency) impedance seen by the current source that delivers I_1 ?
- e) Design a single-transistor (i.e., having one transistor only and possibly a few passive components, such as resistors, capacitors, etc.) current source to implement I_1 .
- f) What is the value of its (low-frequency) output impedance?
- g) Give two possible ways to improve the power-supply rejection of your current source implementation.

- h) Now redesign the above translinear circuit, having the same input-output relation, employing PNP and NPN (thus not only NPN or only PNP) transistors, for operation from a 2-V supply. The parameters $I_{S,PNP}$ and $I_{S,NPN}$ are different and subject to absolute tolerances. The transistor's current-gain factor *BF* is large, but finite (i.e., not infinite).
 - i. First choose a correct translinear loop topology.
 - ii. Subsequently assign the correct collector currents (i.e., choose which current flows through which transistor).
 - iii. Finally, take care of appropriate biasing. Assume ideal biasing and input sources.

Question 3: Dynamic translinear and biasing circuits

Consider the dynamic translinear circuit (DTL) below. The circuit behaves as a non-ideal integrator.

a) Analyze its input-output relation in terms of I_z , I_p , C, I_{in} and I_{out} . All NPN transistors are identical.



b) Now redesign the above non-ideal integrator in such a way that its inputoutput relation becomes that of an ideal integrator:

$$I_{in} = \frac{CU_T}{I_z} \frac{dI_{out}}{dt}, \text{ or } I_{out} = \frac{I_z}{CU_T} \int I_{in} dt$$

NB. The (quiescent) current through Q_1 should be always positive.

- c) If we wish to make the above integrator temperature independent what type of current source I_z do we need?
 - A resistor
 - A peaking current source
 - A proportional-to-absolute-temperature current source
 - A bandgap current reference

Give also a motivation for this.

- d) Design the chosen current source at transistor level, using BJT (NPN and/or PNP) transistors and resistors, operating from a 2-V supply and delivering 1mA at room temperature.
- e) **Bonus question.** If the output resistance (due to the Early effect) of the transistors in the current source designed above is low, give ways (the more the better) to reduce the dependence of I_z on the supply voltage.