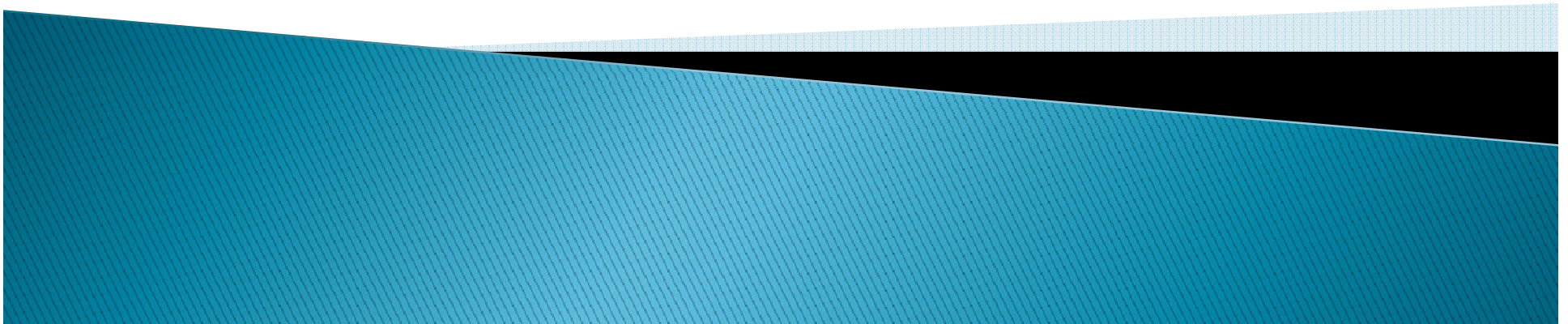


Propulsion & Resistance 1 – lecture 1

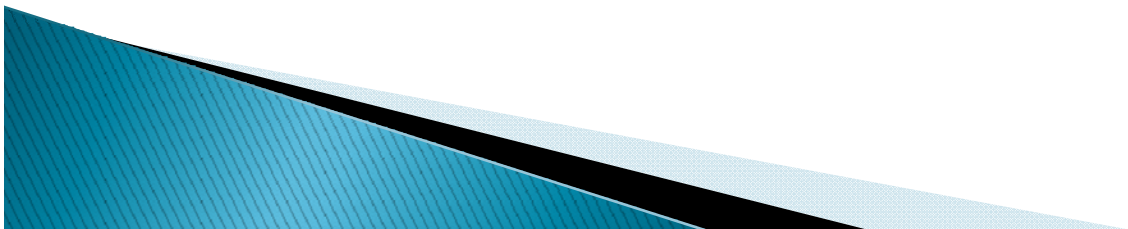
Mt 527

1. Introduction
2. Governing physics
3. Decomposition of resistance
4. Similarity laws and scaling



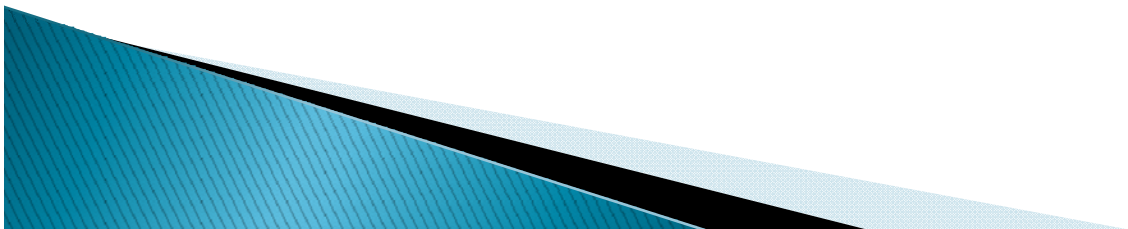
Introduction to the course

- ▶ Importance of proper power–speed prediction
- ▶ Resistance, prop. efficiency, power
- ▶ Wake field
- ▶ Experimental, empirical or numerical prediction
- ▶ Propeller design and cavitation

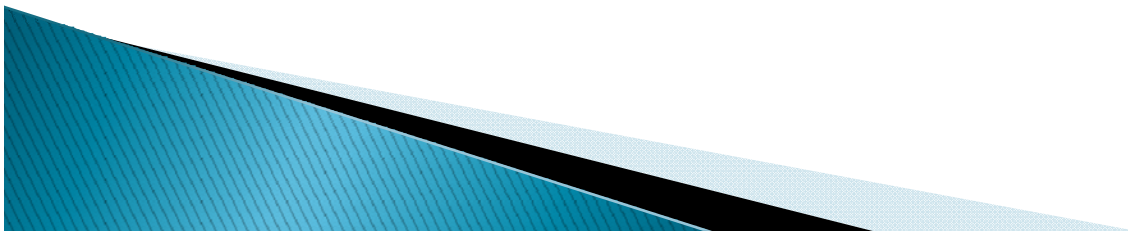


Study goals

- ▶ Understand the *mechanisms for ship resistance and extrapolation* to another scale.
- ▶ Understand the *principles of ship propulsion* (actuator disk, ideal efficiency)
- ▶ Master a *first propeller design* capability based on systematic series
- ▶ Understand *cavitation nuisance* and have a first understanding of the principles.



Historic Perspective



Experimental Prediction

– History

▶ Earliest model tests

1500 approx. – Leonardo da Vinci

Tests on 3 different models with variations in fore– aft displacement distribution

1650 approx. Samuel Fortrey

Towing tests with small wooden models in tank

1770 approx. Pieter van Zwijndrecht Pauluszoon

Towing tests with different waterline models

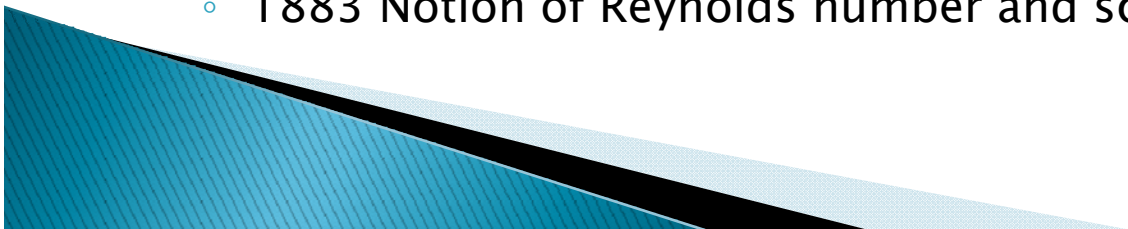
1871 First purpose built Tow Tank by Froude in Torquay (UK)

1873 Model tests by Bruno Tideman with naval cruiser “Atjeh” at the Rijkswerf in Amsterdam

1932 Opening of the “Nederlandsch Scheepsbouwkundig Proefstation (NSP)” in Wageningen (currently MARIN)

▶ But how to scale these models and tests?

- William Froude 1868 – Decomposition of total resistance
- $R_T = R_F + R_R$?
 - R_F = flat plate frictional resistance
 - R_R = residuary resistance
- 1883 Notion of Reynolds number and scaling



Computational Techniques

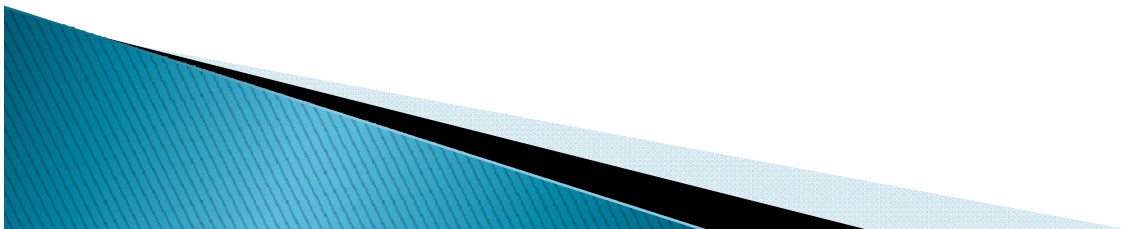
– History

1687 – Newton’s “Philosophiae Naturalis Principia Mathematica”

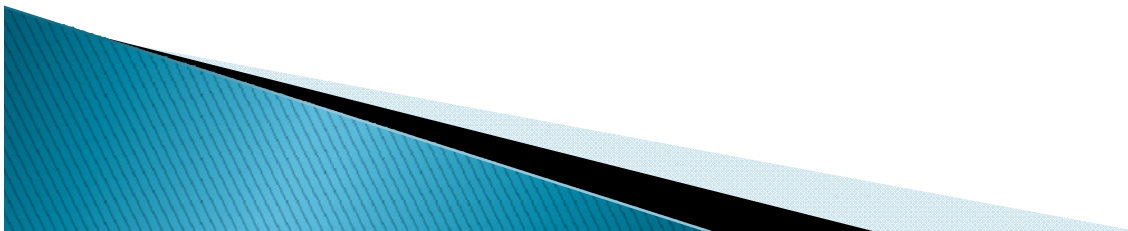
1752 – d’Alembert published what is now called “D’Alembert’s paradox” in response of a contest organized by the French “Academie des Sciences”

1757 – Euler (Swiss mathematician) published an important equation governing an inviscid flow

1822–1840 Development Navier–Stokes equations

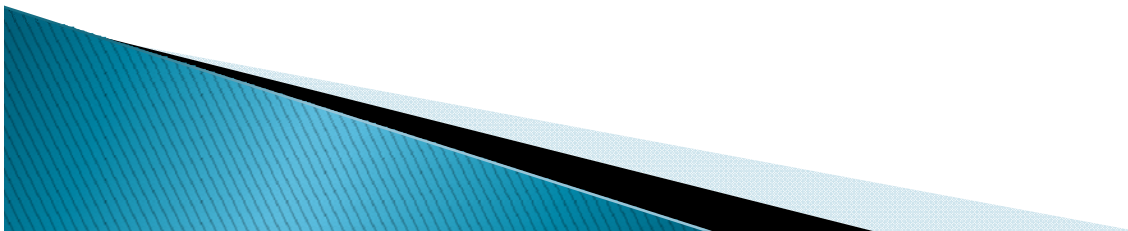


Underlying Principles

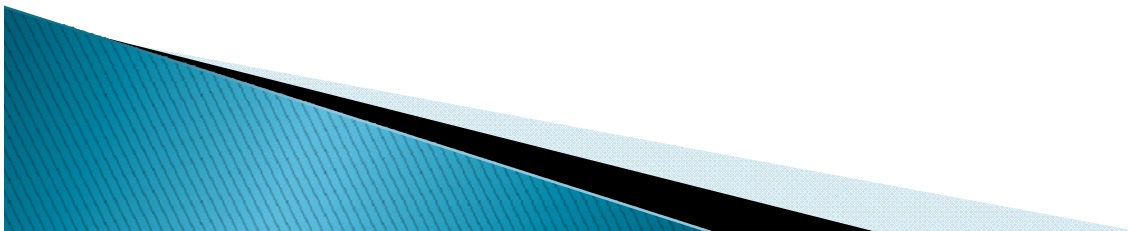


Introduction to continuity, Navier–Stokes and Euler eq's

- ▶ What are the principles of the fluid dynamic equations – The conservation laws

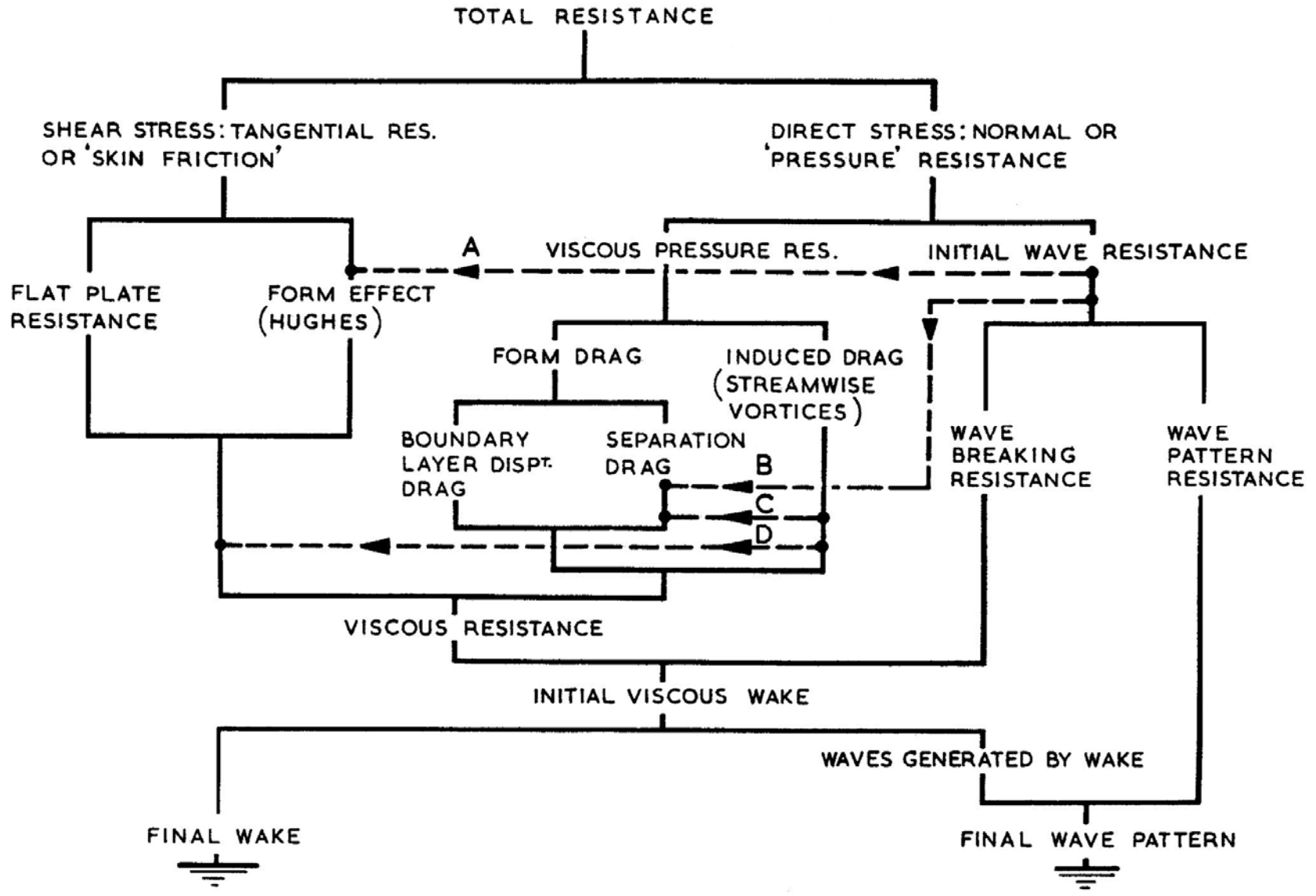


The Resistance Breakdown



Decomposition of Resistance

Source: ITTC 1972 Res. Committee



Decomposition of Resistance

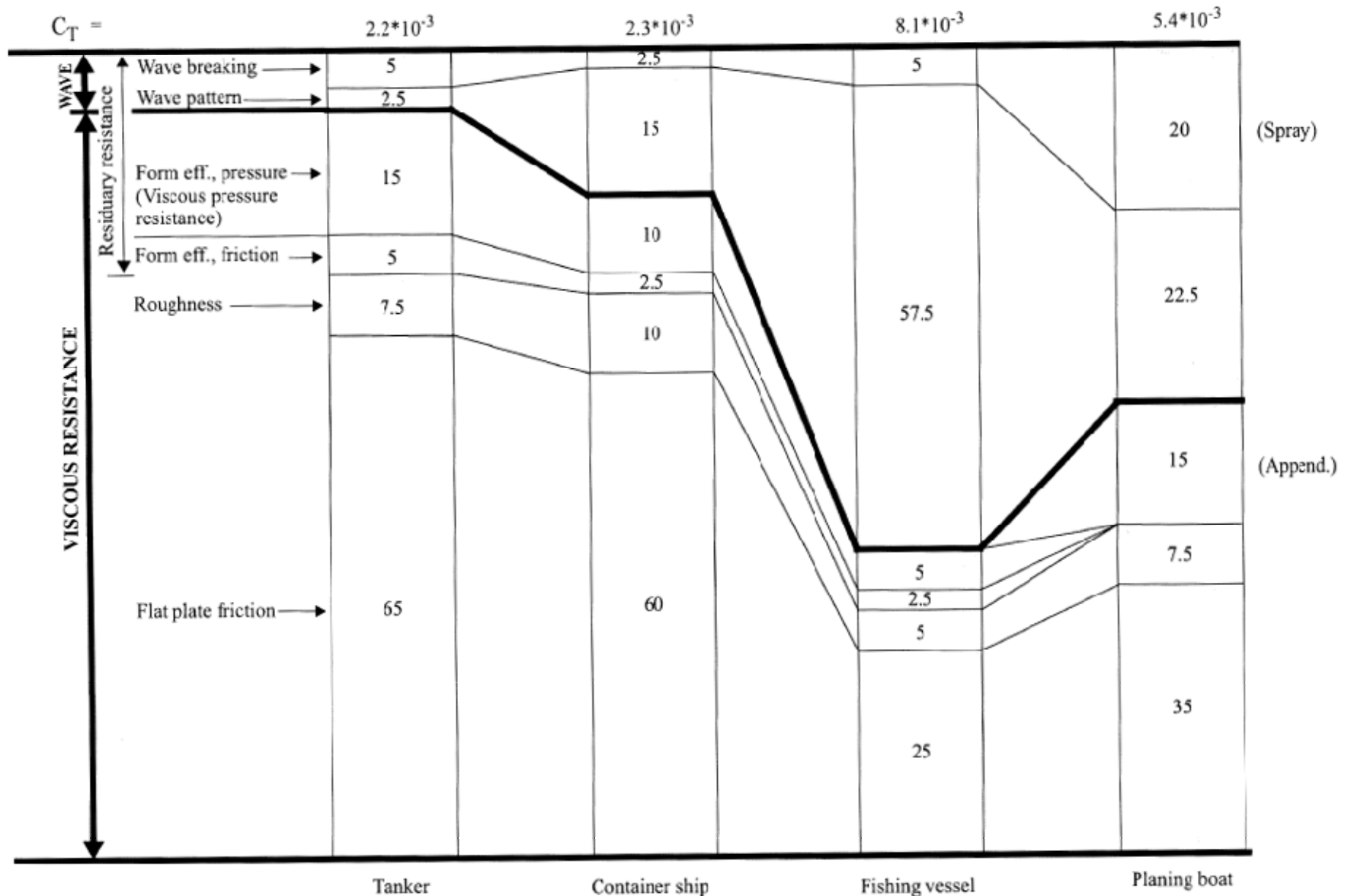
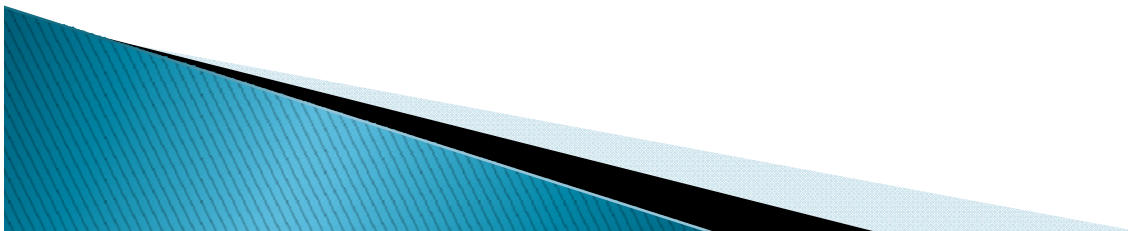


Figure 4.1 Resistance components for four vessels (%).

On flow phenomena



Potential and viscous flow

sheer stress τ [N/m²]:

$$\tau = \mu \frac{\partial u}{\partial y}$$

•velocity U (m/s)

•length scale L (m)

•viscosity μ (Pa s) (kg/ms)

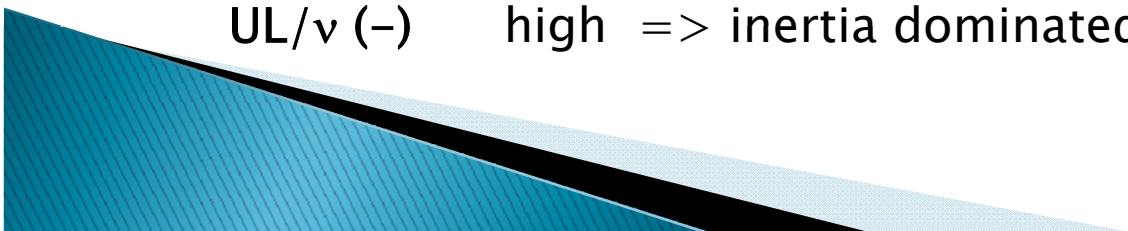
•density ρ (kg/m³)

•kinematic viscosity ν (m²/s)

$$\nu = \frac{\mu}{\rho} \quad \frac{[Pa \text{ sec}]}{[kg / m^3]}$$

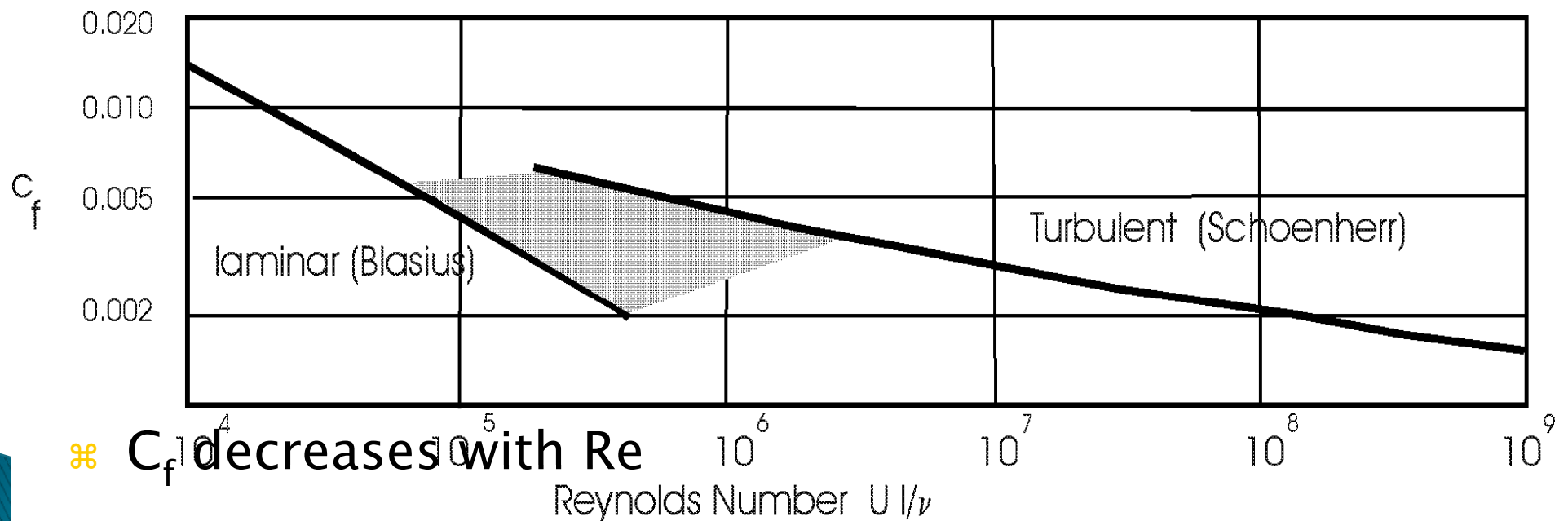
Reynolds: small \Rightarrow viscosity dominated \Rightarrow viscous flow

UL/ν (-) high \Rightarrow inertia dominated \Rightarrow potential flow

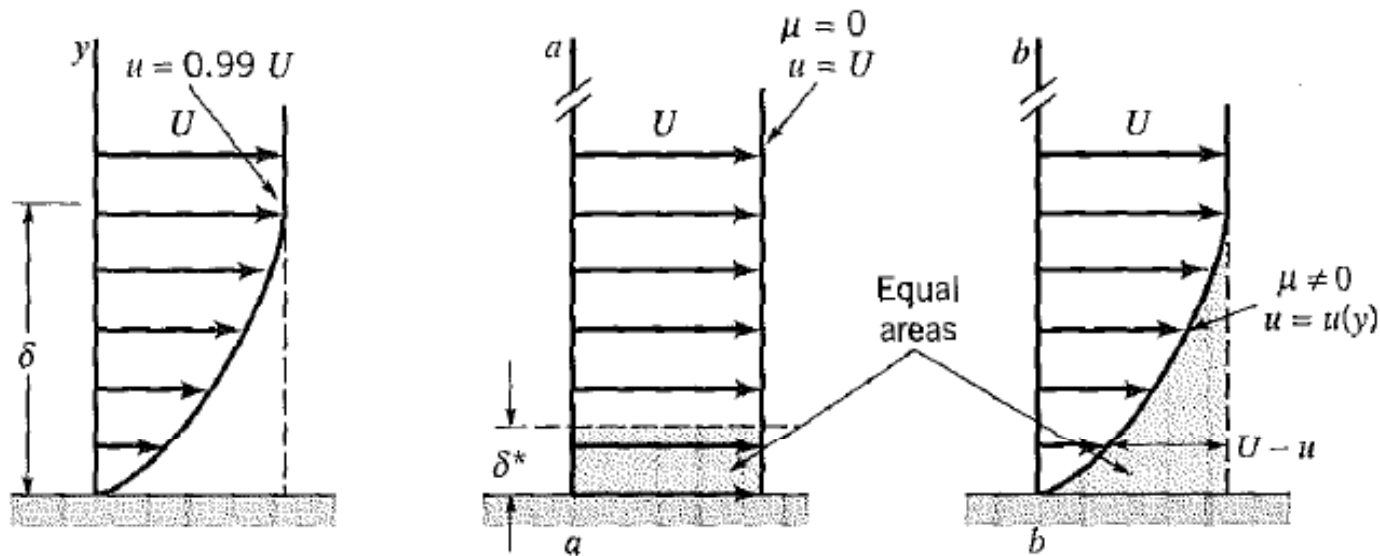


Non dimensional coefficients

⌘ $C_f(\text{Re}) = R_t / 0.5\rho U^2 S$ is not a constant



Boundary layer characterisation



⌘ BL thickness, δ_{99} is difficult to measure \Rightarrow integral measurements

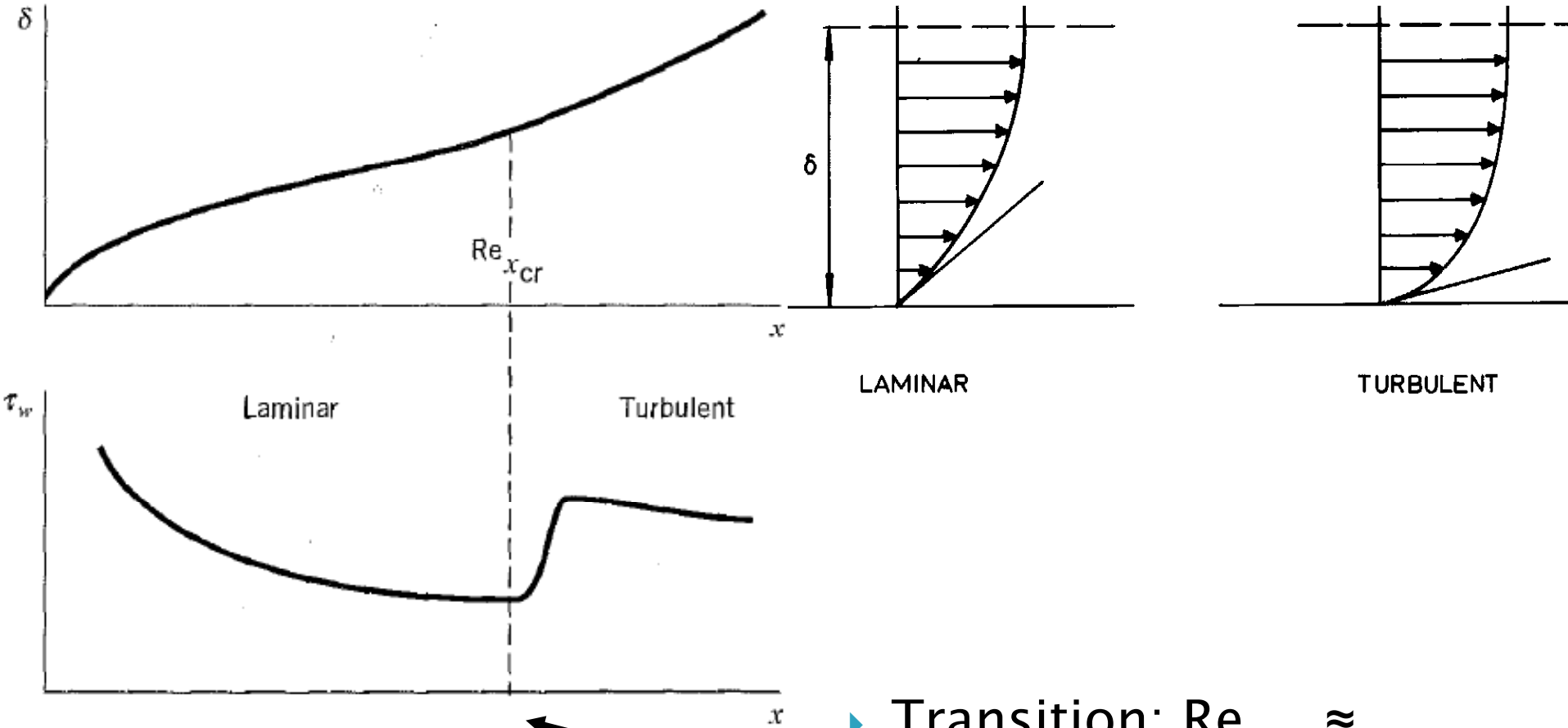
☒ displacement thickness

☒ momentum thickness

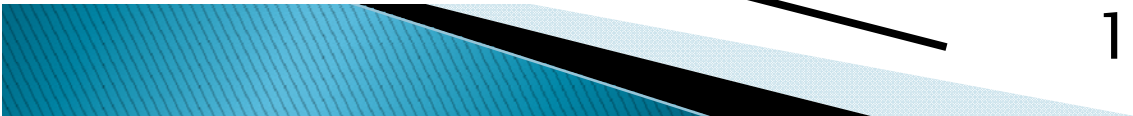
$$\delta^* = \int_0^{\infty} \left(1 - \frac{u}{U} \right) dy$$

$$\theta(x) \equiv \int_0^{\infty} \frac{U(y)}{U_0} \left(1 - \frac{U(y)}{U_0} \right) dy$$

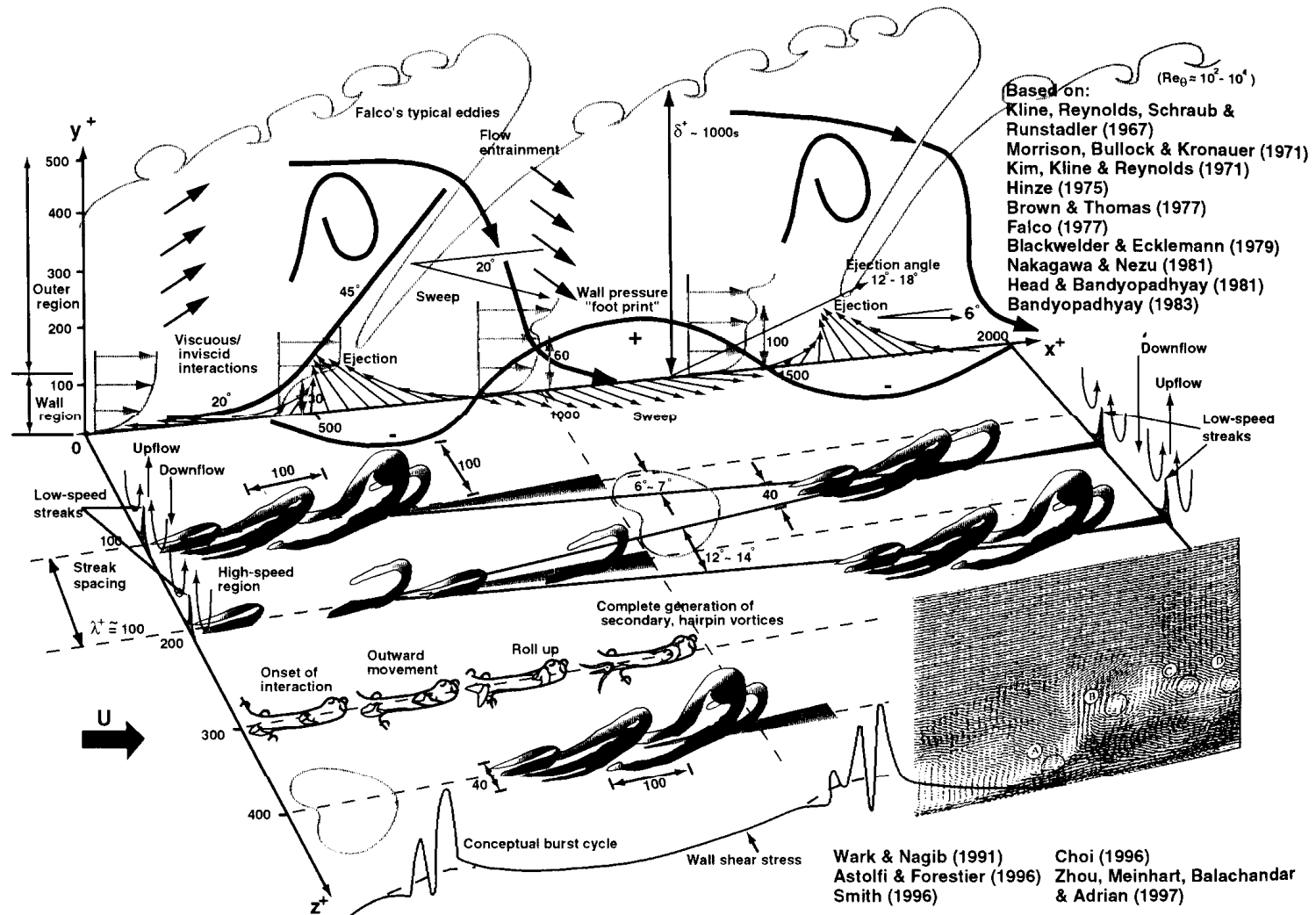
Boundary layer development



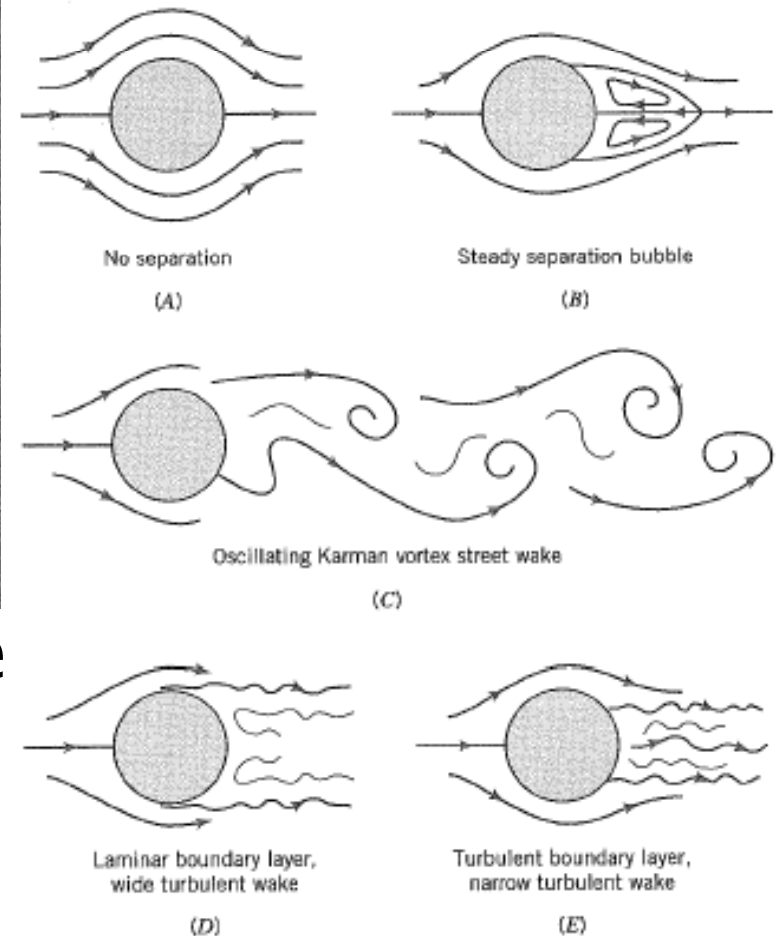
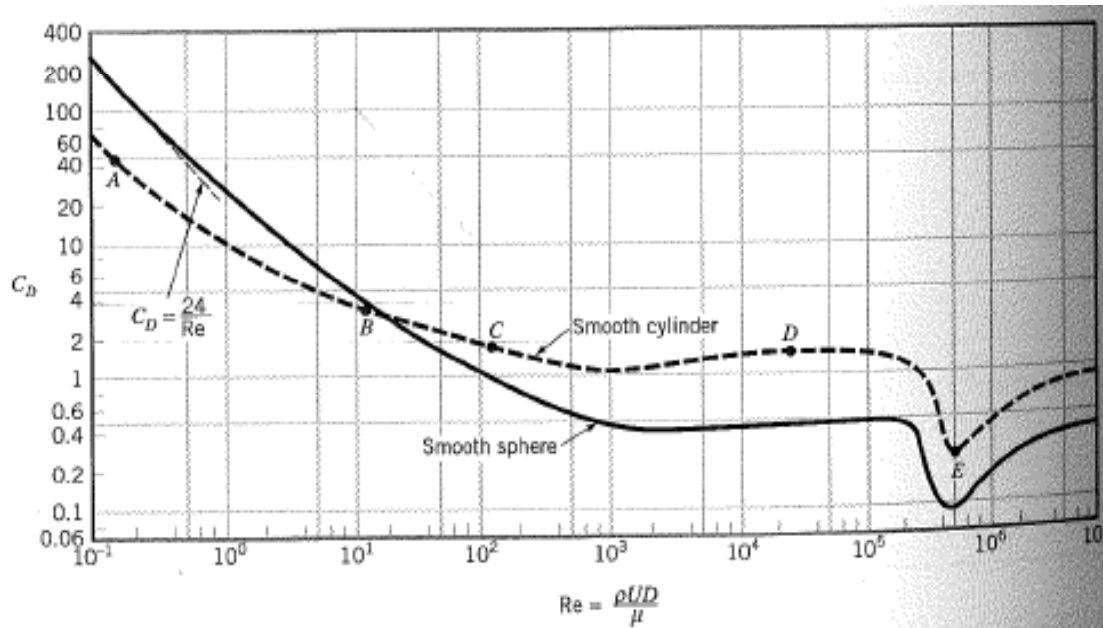
▶ Transition: $Re_{x,cr} \approx 10^5$



Development of boundary layer



Flow pattern around a cylinder



⌘ Exception where turbulence reduces the drag !!

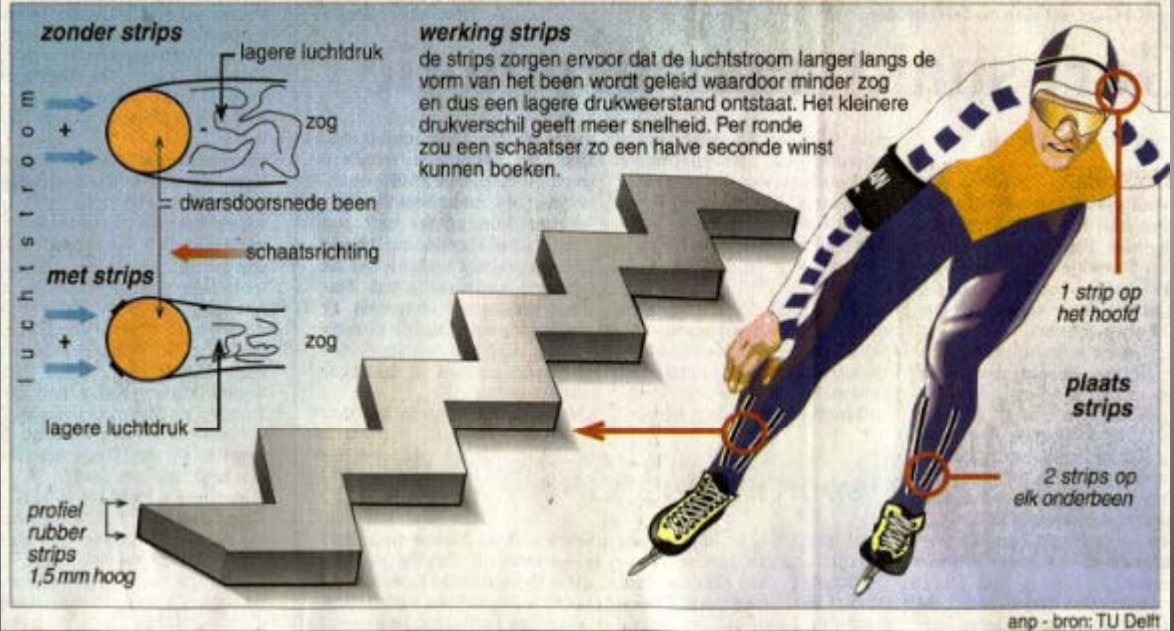
⌘ => golf ball

⌘ => suits for ice skaters

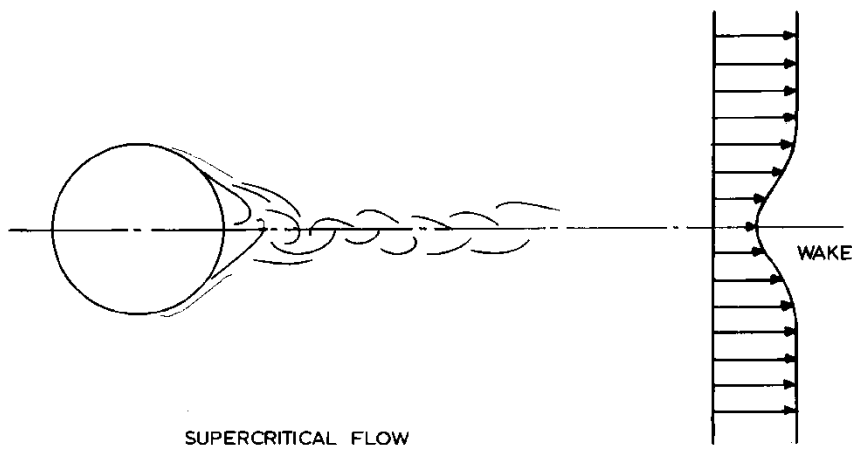
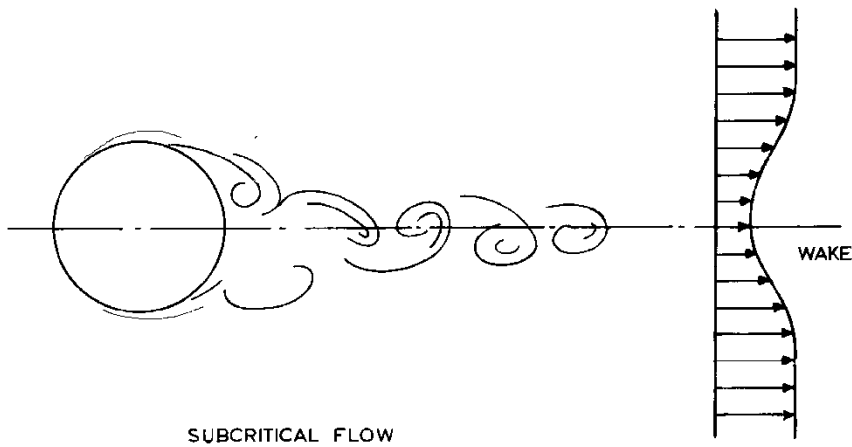
Examples



Strips op schaatspak verminderen drukweerstand en verhogen snelheid



Flow pattern around cylinder

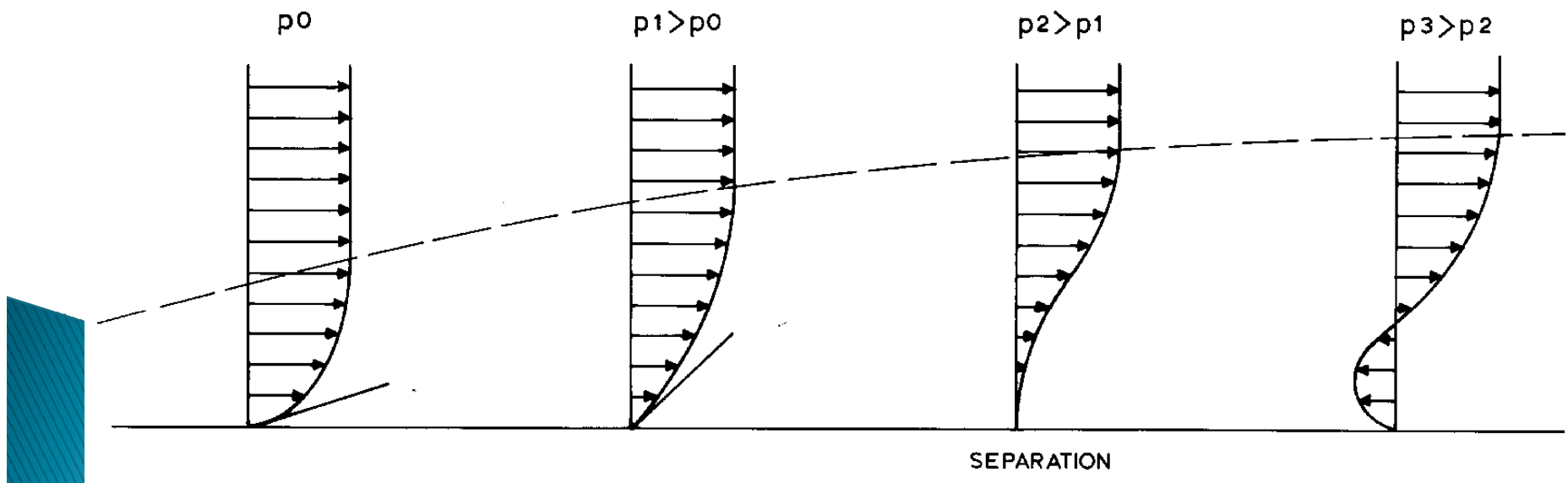


- ⌘ Reduction of the wake
 - ⏏ => lower momentum loss
 - ⏏ => lower resistance



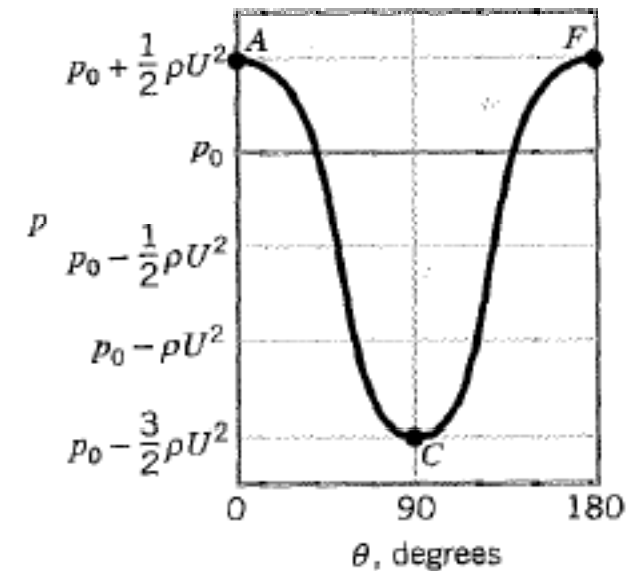
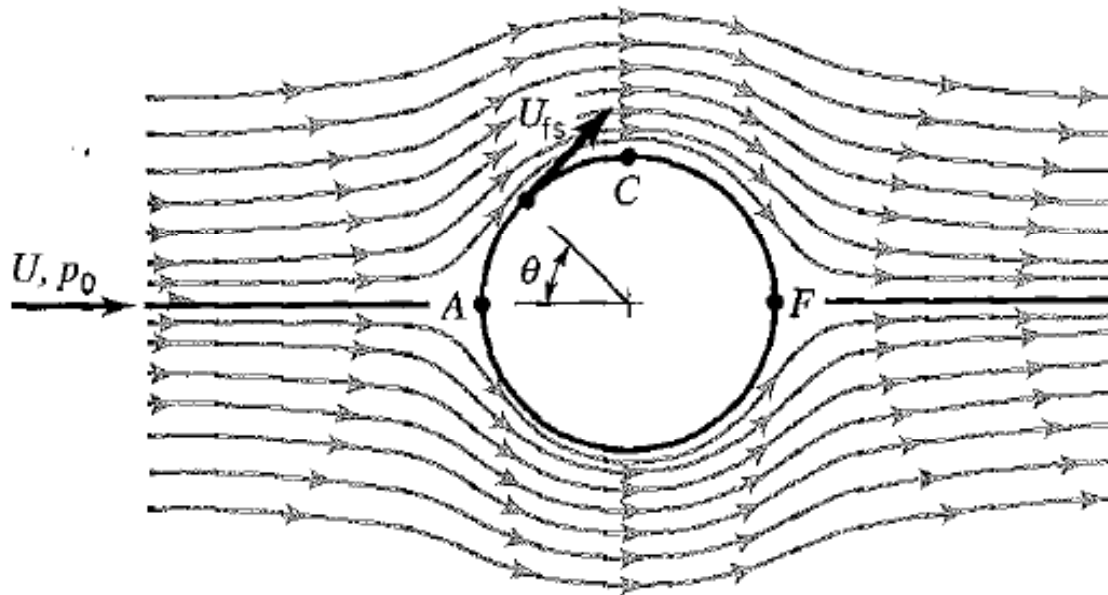
Velocity profiles in BL around separation

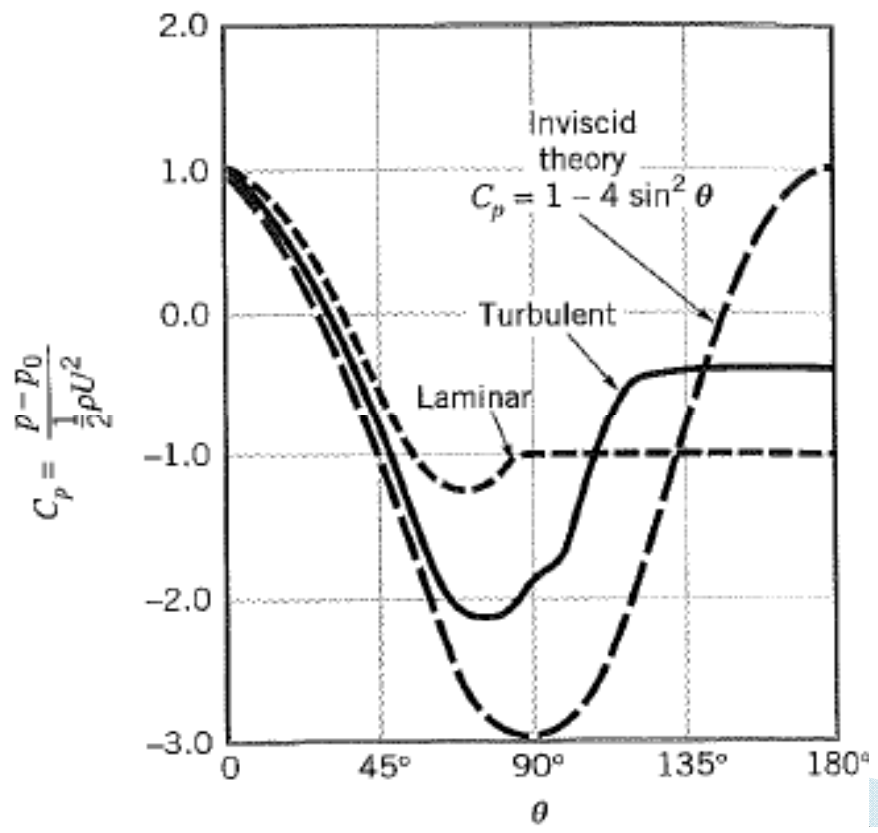
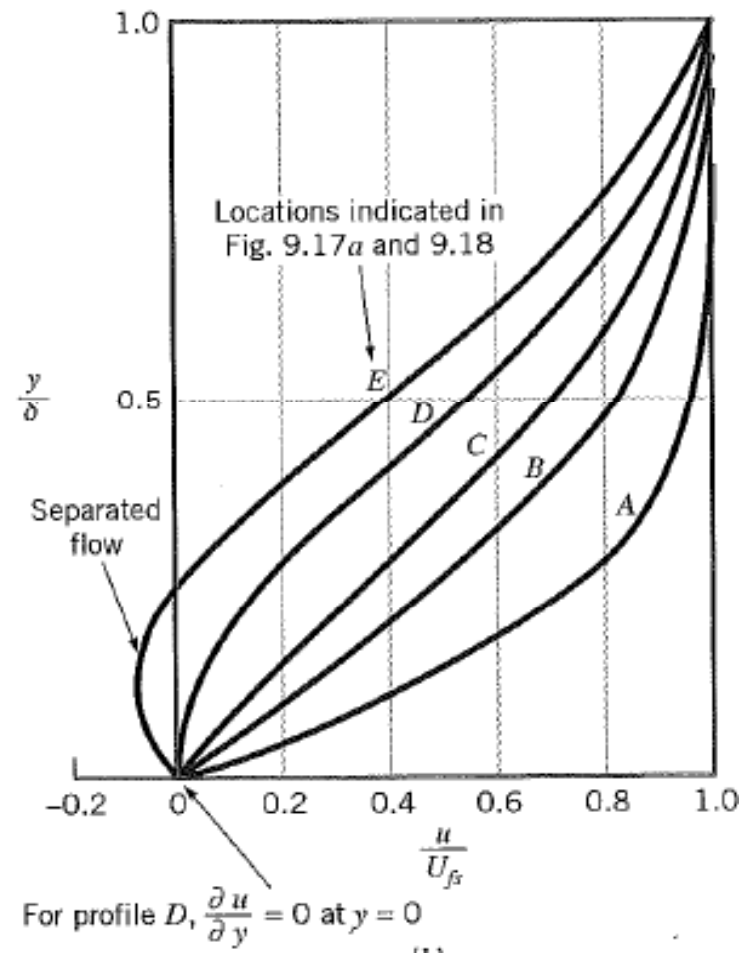
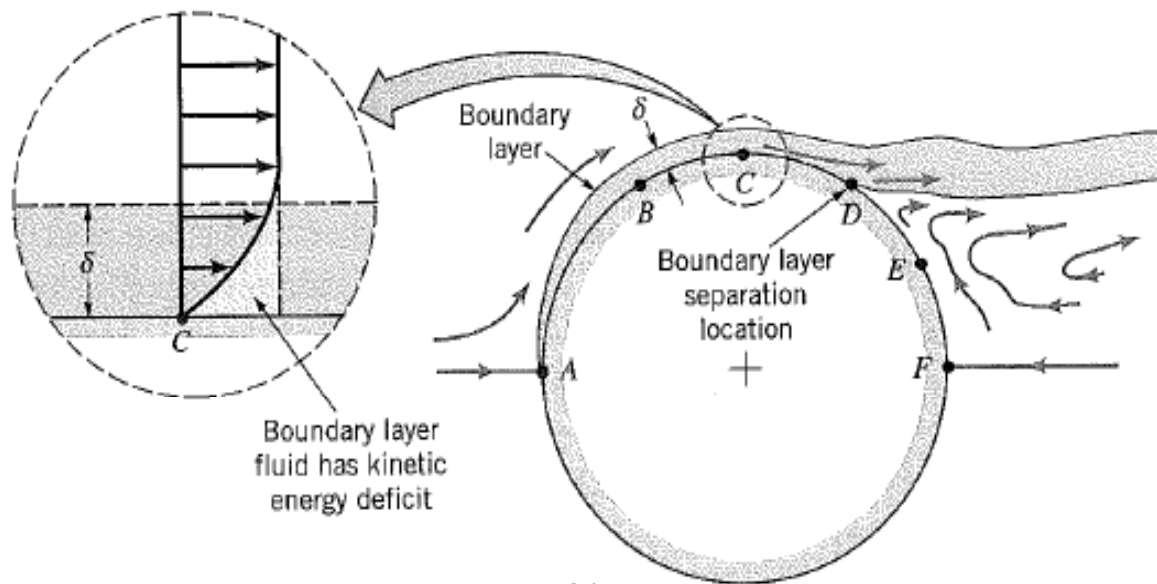
- ⌘ $dP/dx > 0$: favourable pressure gradient (bow)
 - ☒ Stabilises BL
- ⌘ $dP/dx < 0$; adverse pressure gradient (stern)
 - ☒ destabilises BL



Cylinder: Potential flow solution

- ⌘ Potential flow; no friction, no pressure gradient => No drag
- ⌘ High Re; limit $\mu \rightarrow 0$; no friction??
- ⌘ Experiments: always finite drag => **D'Alembert paradox**





Coupling form drag and friction drag

⌘ From flow over plate and cylinder:

☒ pressure \Rightarrow BL growth \Rightarrow friction

☒ friction \Rightarrow separation \Rightarrow pressure

⌘ Froude hypothesis:

☒ *For streamlined bodies (small dP/dx) without flow separation assume that pressure (form) drag and friction drag are independent*

⌘ \Rightarrow *Application on ship design:*

☒ *Form factor and flat plate resistance*



Study guidelines

- ▶ 1. Introduction – *read*
- ▶ 2. Governing equations
 - 2.1–2.3: *understand*, need not be reproduced
 - 2.4–2.5: BCs: Be able to *reproduce physical origin of bc's*
- ▶ 3. Similarity
 - *reproduce* similarity numbers if N–S eq. is given
 - *reproduce* consequences of similarity requirements
- ▶ 4. Decomposition of resistance
 - Reproduce
 - Understand appendix from BB “Notes on Resistance Breakdown” – ITTC/Paffett 1972



Laws of similarity

- ▶ Derivation of R_n , E_n , F_n , W_n from N-S eq. and bc's
- ▶ R_n - F_n dilemma

