Time domain models Course: Wb2301

Lecture 6 Erwin de Vlugt March 16 2010

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Contents

- Distortion from Sample and hold circuits
- The Z-transformation
- Discrete time-domain identification
- Model structures and parameterization
- Open and closed loop identification using discrete models



Signal Reconstruction



Zero order hold (ZOH) Sample time $\Delta t = 1s$

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ZOH FRF



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Signal Distortion



- Signal distortion due to sampling and hold circuit
- Reduce distortion by increasing sampling frequency
- No signal transfer at the Nyquist frequency ($\omega_h = \frac{1}{2}\omega_s$ and sample frequency (ω_s)

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Z-transformation

$$X(z) = \mathcal{Z}\{x[n]\} = \sum_{n=-\infty}^{\infty} x(n)z^{-n}$$

where n is an integer and z is, in general, a complex number:

$$z = Ae^{j\phi}$$
$$= A(\cos\phi + j\sin\phi)$$

where A is the magnitude, and ϕ is the angle of z



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Z-transformation

Example:

$$[x(1) \ x(2) \ x(3) \ \dots \ x(N)] = [1 \ 2 \ 3 \ 0 \ 0 \ \dots \ 0]$$
$$X(z) = 1z^0 + 2z^{-1} + 3z^{-2}$$

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Continuous to discrete poles-zeros





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Z-Laplace Mappings

Inverse mapping

$$s = \frac{1}{\Delta t} \ln(z)$$

Using the bilinear (Tustin) approximation (1st order Taylor coeff.):

$$s = \frac{2}{\Delta t} \frac{z-1}{z+1} = \frac{2}{\Delta t} \frac{1-z^{-1}}{1+z^{-1}}$$
$$z = \frac{2+s\Delta t}{s-s\Delta t}$$

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Example

$$H(s) = \frac{1}{s+1} \qquad H(z)_{tustin} = \frac{\Delta t}{2+\Delta t} \frac{z+1}{z-\frac{2-\Delta t}{2+\Delta t}}$$



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Time domain identification

- 1. Digital acquisition: signals are represented by discrete numbers (sampling)
- 2. Systems are described by polynomials in the z-domain
 - Deterministic and stochastic parts can be separated (noise models)
 - Appropriate for nonlinear identification
 - Disadvantage: a priori knowledge required



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Time domain identification

• Purpose

Capture system properties by a limited number of parameters (n < N) These n parameters (indirectly!) represent system dynamics, i.e. physical properties

• Approach

Discriminate input related response from noise in output



Auto-regressive (AR) filter



Describes many physical processes due to feedback structure

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Moving Average (MA) filter



Finite time integration structure

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General Model



$$y(k) = G(z^{-1})u(k) + H(z^{-1})e(k)$$

- white noise e(k)
- goal: estimate $G(z^{-1})$ from y(k), u(k)

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System Identification

- Experimental system data
- Choice of model structure
- Optimization criterion
- Validation

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Finding the best model

System:

$$y(k) = G_0(z^{-1})u(k) + H_0(z^{-1})e(k)$$

Assume a model (G, H, ϵ) can be found such that:

$$y(k) = G(z^{-1})u(k) + H(z^{-1})\epsilon(k)$$

Then the model error is:

$$\epsilon(k) = H^{-1}(z^{-1}) \left[y(k) - G(z^{-1})u(k) \right]$$

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Obtaining the model



System: $G_0(z^{-1}), H_0(z^{-1})$ Model: $G(z^{-1}), H(z^{-1})$

$$\epsilon(k) = H^{-1}(z^{-1}) \left[y(k) - G(z^{-1})u(k) \right]$$

Optimal fit : If $G(z^{-1}) \approx G_0(z^{-1})$ and $H(z^{-1}) \approx H_0(z^{-1})$ then $\epsilon(k) \approx e(k)$

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Least squares (LS) Criterion

$$V(\theta)_N = \min \sum_{k=1}^N \epsilon(k, \theta)^2$$

- V cost function
- θ model parameter vector
- ϵ model error
- N number of data points

For the optimal solution: $\epsilon \rightarrow e$



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Finite Impulse Response (FIR) structure



$$y(k) = B(z^{-1})u(k) + e(k)$$

 $e(k) = y(k) - B(z^{-1})u(k)$

An FIR model is linear in its parameters.

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Output Error (OE) structure



$$y(k) = \frac{B(z^{-1})}{F(z^{-1})}u(k) + e(k)$$
$$e(k) = y(k) - \frac{B(z^{-1})}{F(z^{-1})}u(k)$$

An OE model is <u>nonlinear</u> in its parameters.

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ARX structure



$$y(k) = \frac{B(z^{-1})}{A(z^{-1})}u(k) + \frac{1}{A(z^{-1})}e(k)$$
$$e(k) = A(z^{-1})y(k) - B(z^{-1})u(k)$$

An ARX model is linear in its parameters.

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ARMAX structure



$$y(k) = \frac{B(z^{-1})}{A(z^{-1})}u(k) + \frac{C(z^{-1})}{A(z^{-1})}e(k)$$
$$e(k) = \frac{A(z^{-1})}{C(z^{-1})}y(k) - \frac{B(z^{-1})}{C(z^{-1})}u(k)$$

An ARMAX model is nonlinear in its parameters.

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Box-Jenkins (BJ) structure



$$y(k) = \frac{B(z^{-1})}{F(z^{-1})}u(k) + \frac{C(z^{-1})}{D(z^{-1})}e(k)$$
$$e(k) = \frac{D(z^{-1})}{C(z^{-1})}y(k) - \frac{D(z^{-1})B(z^{-1})}{C(z^{-1})F(z^{-1})}u(k)$$

An BJ model is <u>nonlinear</u> in its parameters.

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Optimizing the criterion (ARX)

$$\epsilon(k) = A(z^{-1})y(k) - B(z^{-1})u(k)$$

with n_a, n_b are the model orders according to:

$$na: \quad A(z^{-1}) = 1 + a_1 z^{-1} + \ldots + a_{na} z^{-na}$$
$$nb: \quad B(z^{-1}) = b_1 + b_2 z^{-1} \ldots + b_{nb} z^{-nb+1}$$

Structured regression format:

$$\epsilon(k) = y(k) + [A(z^{-1}) - 1]y(k) - B(z^{-1})u(k)$$

= $y(k) - \phi(z^{-1})\theta$

where

$$\theta = [b_1 \ b_2 \dots b_n \ a_1 \ a_2 \dots a_n]^T$$
$$\phi = [U \ -Y]$$

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Optimizing the criterion (ARX)

$$V(\theta)_N = \min \sum_{k=1}^N \epsilon(k, \theta)^T \epsilon(k, \theta) = \epsilon(k)^T \epsilon(k)$$
$$\frac{\delta V(\theta)}{\delta \theta} = [y(k) - \phi \theta]^T \phi = 0$$

$$\theta = y(k)^T \phi [\phi^T \phi]^{-1}$$

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Choice of model structure

Use system knowledge

- Existence of feedback loops
- Noise sources

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Closed loop system



Goal: estimate
$$\frac{y(k)}{u(k)}$$

Take:

$$H_1(z^{-1}) = \frac{N_1}{D_1}$$

 $H_2(z^{-1}) = \frac{N_2}{D_2}$

$$y = \frac{H_1 H_2}{1 + H_1 H_2} u + \frac{1}{1 + H_1 H_2} e$$

= $\frac{N_1 N_2}{D_1 D_2 + N_1 N_2} u + \frac{D_1 D_2}{D_1 D_2 + N_1 N_2} e$
= $\frac{B}{A} u + \frac{C}{A} e$

This system has an ARMAX structure.

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Analysis

Frequency response:

$$z^{-n} = e^{-ns\Delta t}$$
 with $s = j2\pi f$ $(f = [0...\frac{f_s}{2}])$

Impulse response:

$$u(k) = m$$
 with $m = 1$ for $k = 0$
 $m = 0$ for $k > 0$

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Example



2DOF arm admittance: spectral (grey) ARX (black)

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Closed loop algorithms

Goal: estimate H_2



- 1. Two stage method
- 2. Coprime factorization method



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Two stage

System transferfunctions:

$$u(k) = \frac{H_1}{1 + H_1 H_2} r(k) + \frac{H_1}{1 + H_1 H_2} e(k)$$

$$y(k) = \frac{H_1 H_2}{1 + H_1 H_2} r(k) + \frac{1}{1 + H_1 H_2} e(k)$$

Two stage:

- 1. Open loop from r(k) to u(k)
- 2. Simulate a 'noise free' input $u^*(k)$
- 3. Open loop estimate from $u^*(k)$ to y(k) gives the estimated system H_2

Drawback: only for stable (sub)systems because of the simulation step March 16 2010 32



Coprime factorization

System transferfunctions:

$$u(k) = \frac{H_1}{1 + H_1 H_2} r(k) + \frac{H_1}{1 + H_1 H_2} e(k)$$

$$y(k) = \frac{H_1 H_2}{1 + H_1 H_2} r(k) + \frac{1}{1 + H_1 H_2} e(k)$$

Coprime factorization:

- 1. Open loop from r(k) to u(k) gives $\frac{H_1}{1+H_1H_2}$
- 2. Open loop from r(k) to y(k) gives $\frac{H_1H_2}{1+H_1H_2}$
- 3. then, $\frac{y(k)}{r(k)}\frac{r(k)}{u(k)}$ gives H_2

Drawback: high order because poles and zeros do not cancel out

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Summary

- Time domain models use only a few parameters (w.r.t. FRFs)
- Model structure required and must be selected a priori
- Optimum order must be selected
- Parameterization by minimizing an error criterion
- Direct simulation/validation



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