



EE1320: Measurement Science

Lecture 5: Analog-to-Digital Convertors

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May 21, 2013

Course program 2013

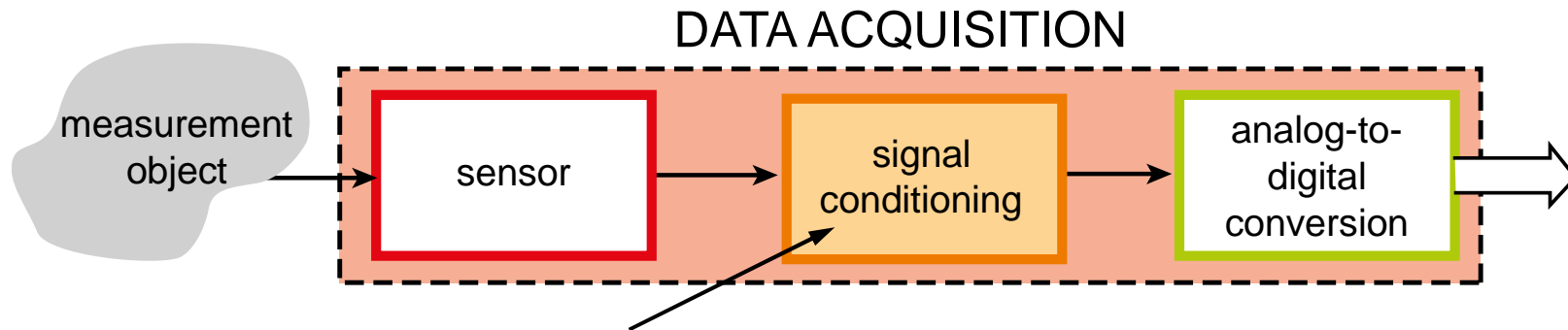
week	date	topic
4.1	Tu 23/4 Fr 26/4	#1 intro measurements and meas. systems #2 sensors
4.3	Tu 7/5	#3 sensor readout and signal conditioning
4.4	Tu 14/5 We 15/5	#4 instrumentation amplifiers intermediate test
4.5	Tu 21/5	#5 analog-to-digital converters
4.6	We 29/5	#6 measurement instruments I
4.7	Tu 4/6 We 5/6	#7 measurement instruments II intermediate test
4.8	Tu 11/6	tutorial
4.11	We 3/7	final exam

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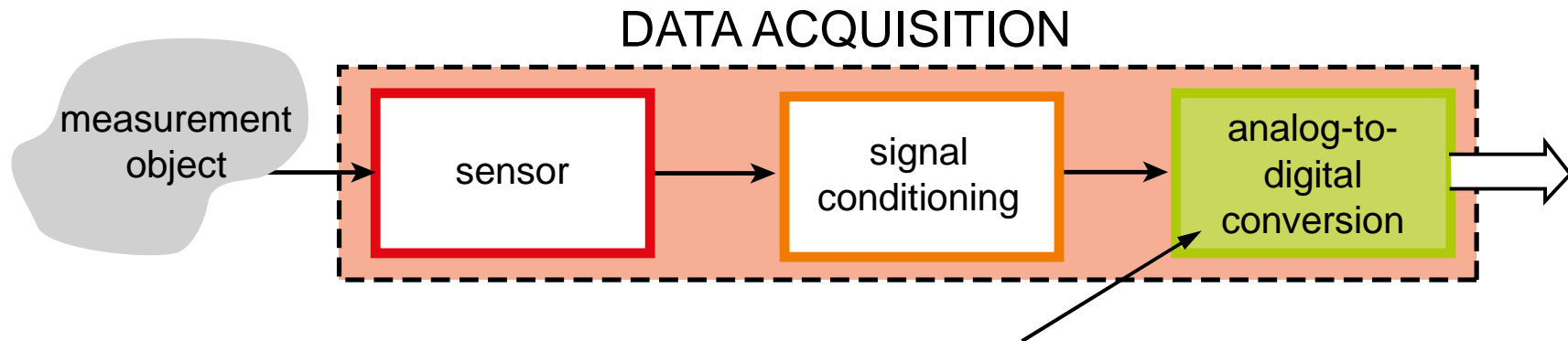
Previous lectures...

signal conditioning



- Signal conditioning needed to adjust output signal of the sensor to the input of the ADC
 - Opamp-based readout circuits, with non-idealities
 - Bridge circuits
 - Differential vs. common-mode signals
 - Difference and instrumentation amplifiers

Today: analog-digital convertors



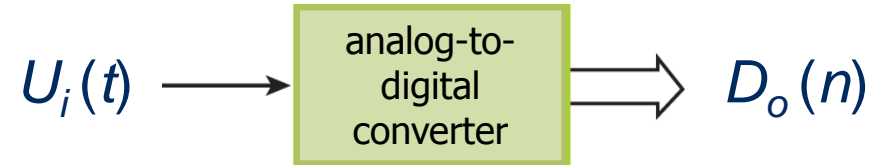
- Basic principles:
 - Sampling
 - Quantization
- Three important ADC types:
 - Flash ADCs
 - Dual-slope ADCs
 - Successive-approximation ADCs



Overview study material

- Regtien 2.1.1: classification of signals, analog vs. digital
- Regtien 2.2.3: sampling, aliasing
- Regtien 18: D/A en A/D conversion
- Regtien 15.2.2: Sample-and-hold circuits

ADC: sampling and quantization

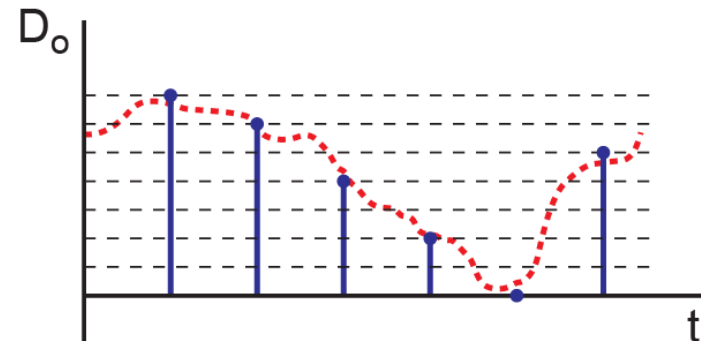
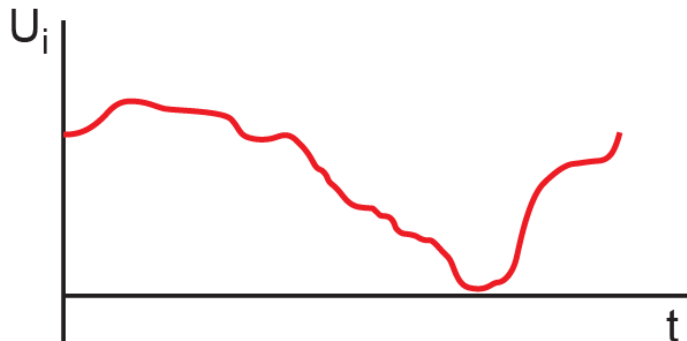


analog input signal

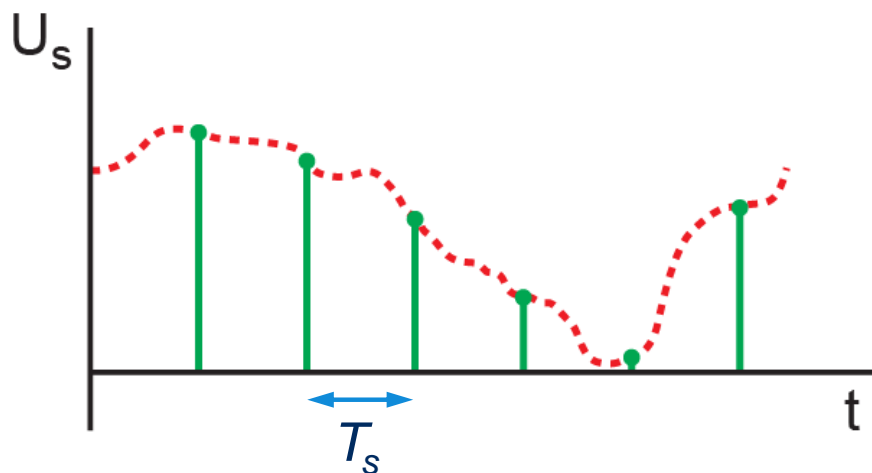
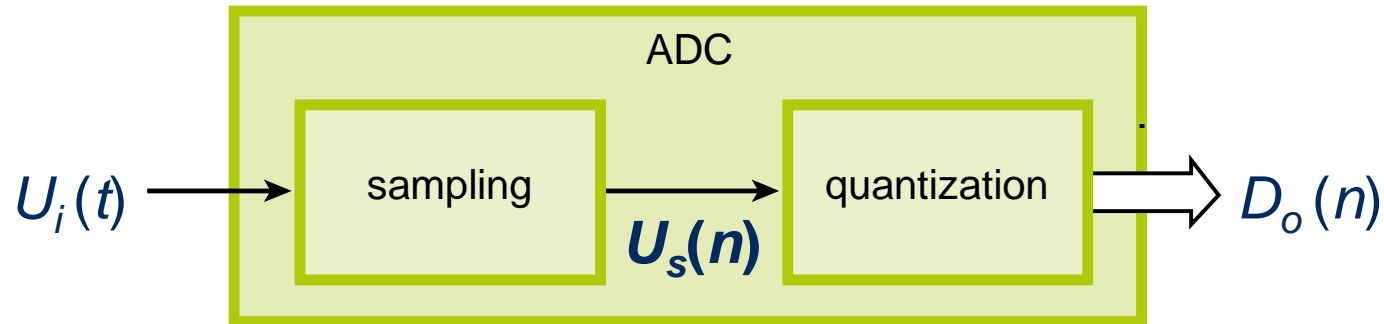
- time continuous
- amplitude continuous

digital output signal

- time discrete: sampled
- amplitude discrete: quantized



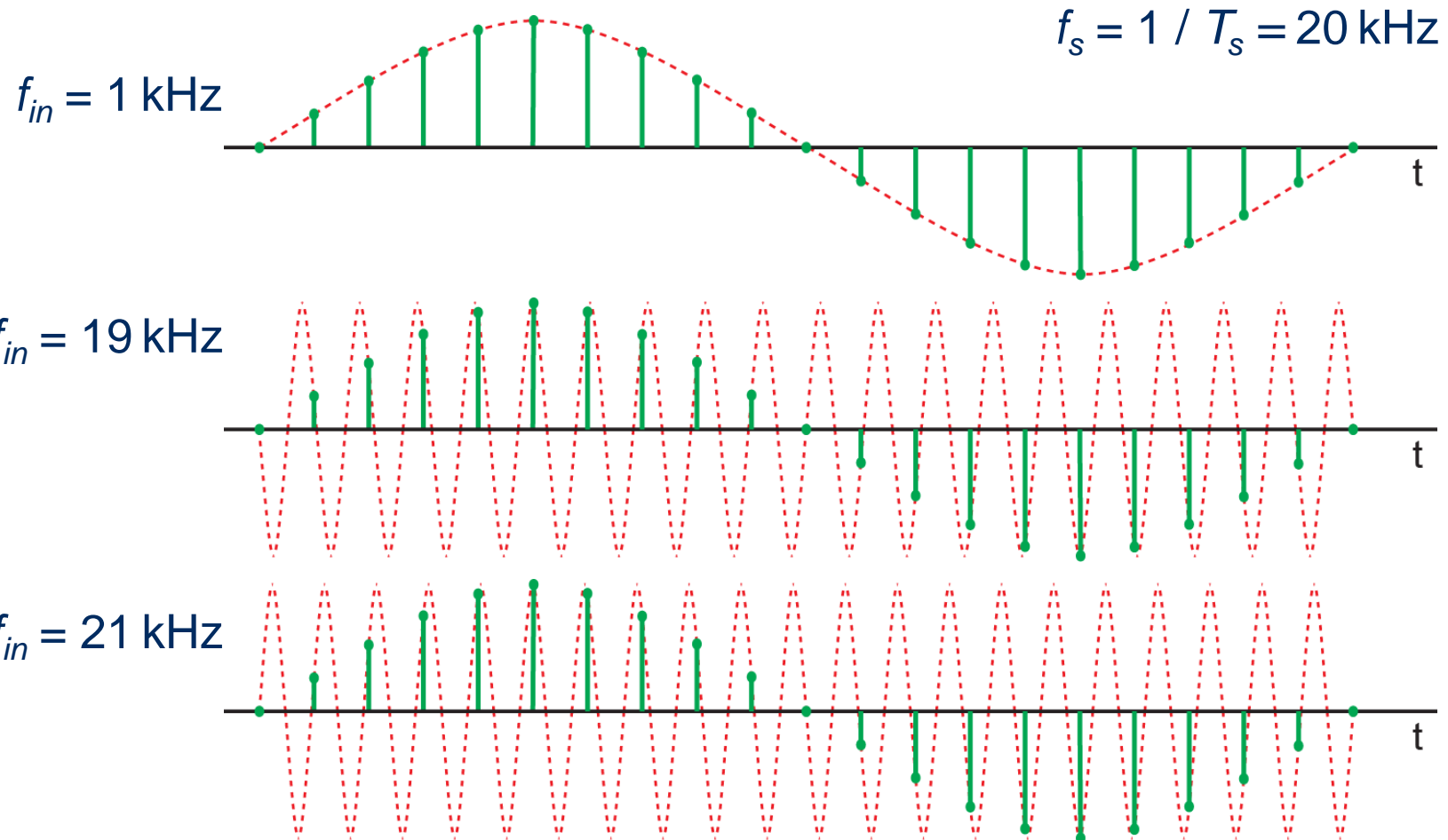
Sampling



sampled input signal

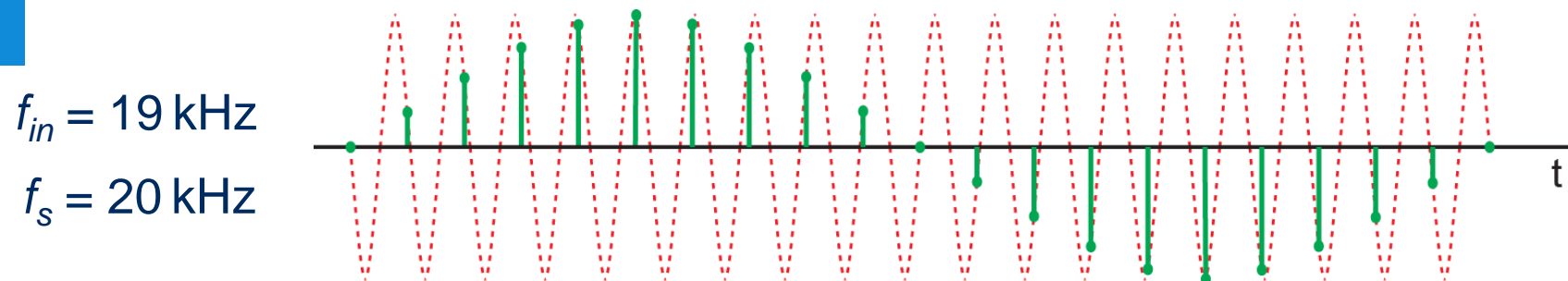
- amplitude information only at discrete points in time $t = n \cdot T_s$
- sampling frequency $f_s = 1 / T_s$ has to be sufficiently high to be able to track changes in U_i

Sampling



Various input signals yield the **exact same** sampled signal!

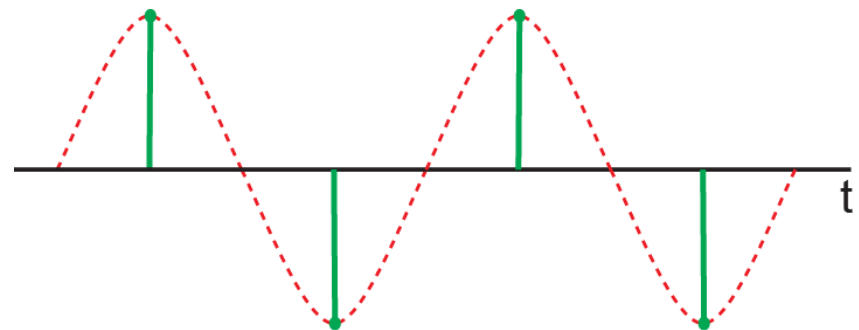
Aliasing



- 19 kHz input signal sampled with $f_s = 20 \text{ kHz}$ is indistinguishable from 1 kHz signal
⇒ by sampling, the 19 kHz 'folds back' to 1 kHz
- This folding back is called **aliasing**
- In order to prevent aliasing, the sampling has to be done at a sufficiently high frequency

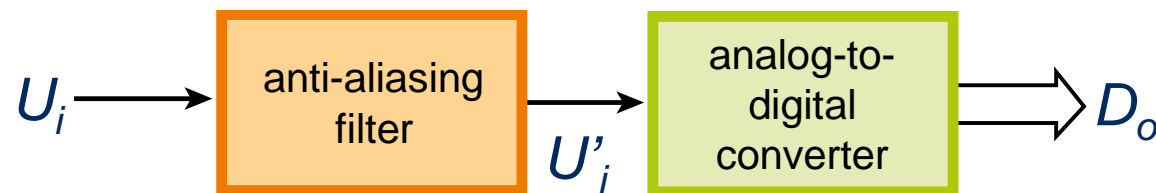
Shannon-Nyquist Theorem

- A signal that contains no components with a frequency higher than f_{max} can be fully reconstructed based on sampling at $f_s > 2 \cdot f_{max}$ (the Nyquist frequency)
- If $f_s \leq 2 \cdot f_{max}$ aliasing will occur
- So: at least 2 samples per period of the highest frequency component



Preventing aliasing

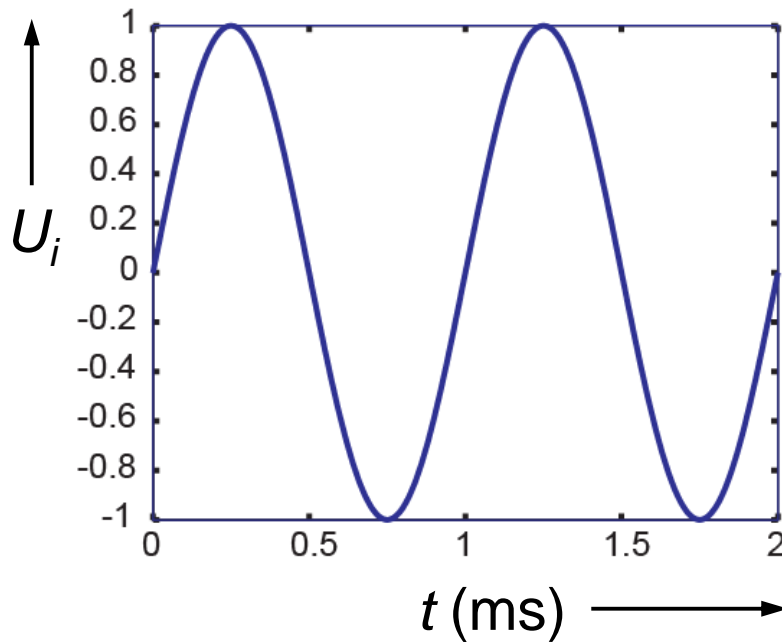
- Two ways:
 - Sample at least at the Nyquist frequency: $f_s > 2 \cdot f_{max}$
 - Limit the bandwidth of the input signal: $f_{max} < f_s / 2$
- **Anti-aliasing filter:** low-pass filter suppressing signal components above $f_s / 2$



Exercise: aliasing



- What is the minimum f_s at which aliasing is prevented?

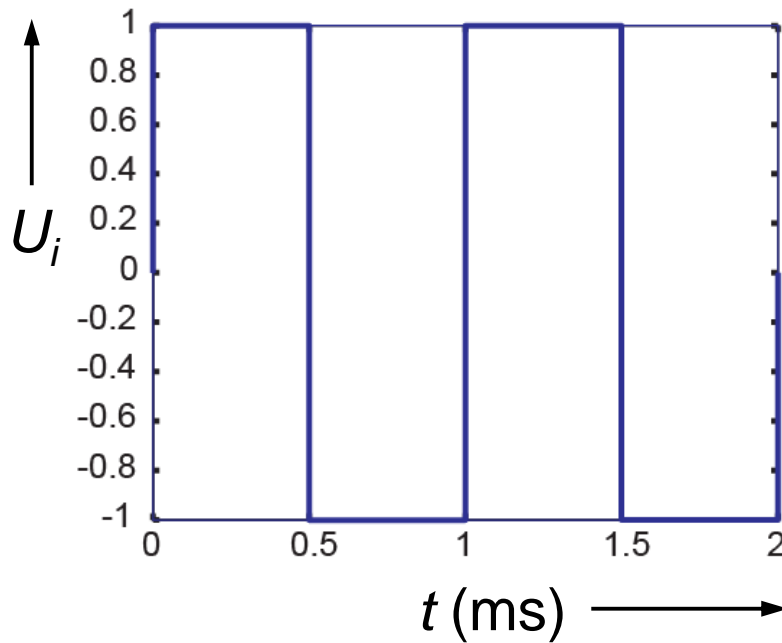


$$U_i(t) = \sin(2\pi \cdot f \cdot t), \quad f = 1 \text{ kHz}$$

Oefening: aliasing



- What is the minimum f_s at which aliasing is prevented?

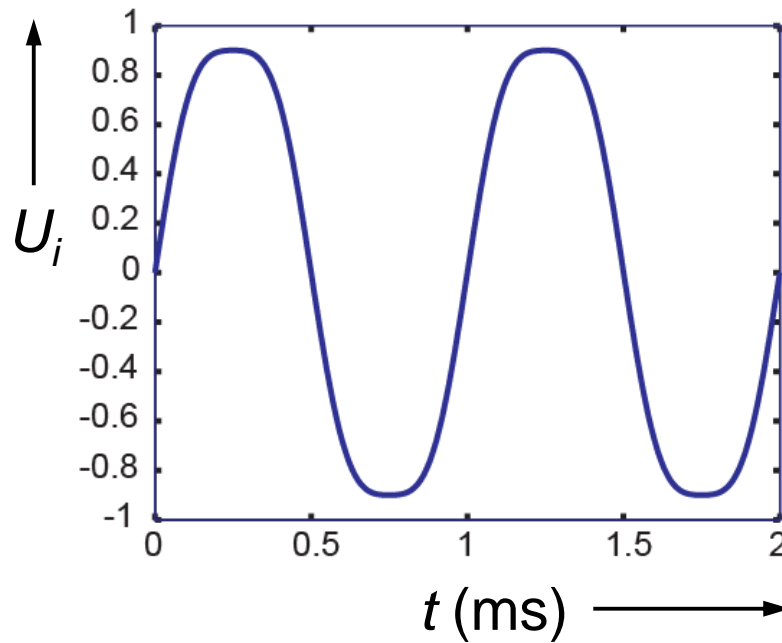


$$U_i(t) = \text{square wave } f = 1 \text{ kHz}$$

Exercise: aliasing



- What is the minimum f_s at which aliasing is prevented?

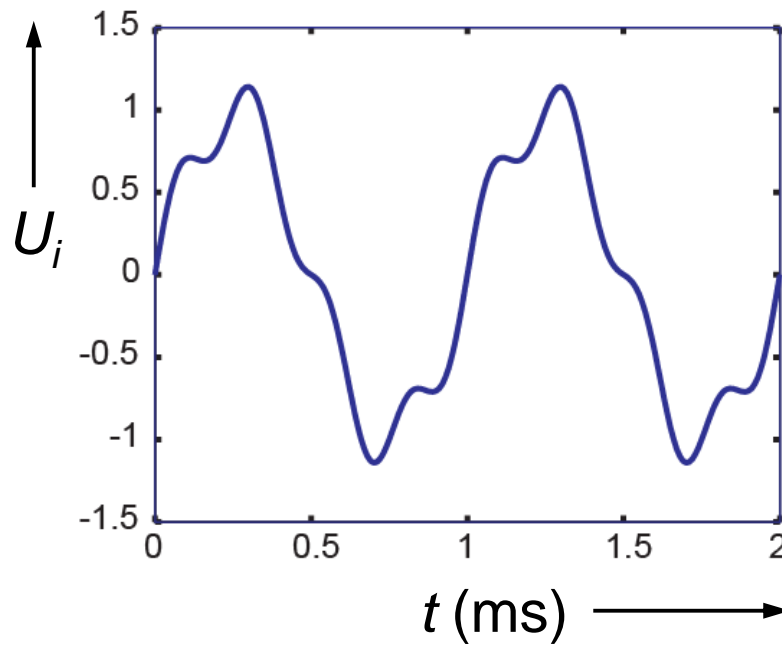


$$U_i(t) = \sin(2\pi \cdot f \cdot t) \\ + 0.1 \cdot \sin(2\pi \cdot 3f \cdot t), \\ f = 1 \text{ kHz}$$

Exercise: aliasing

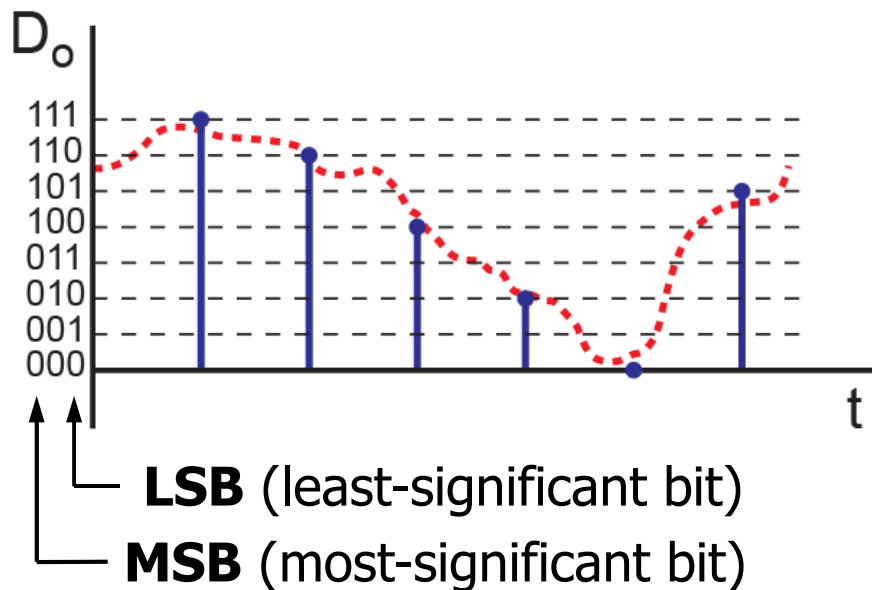
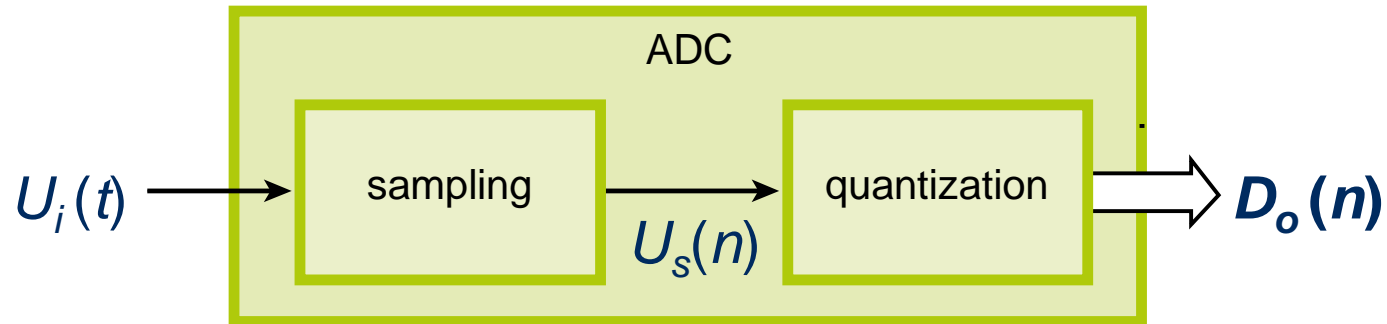


- What is the minimum f_s at which aliasing is prevented?



$$U_i(t) = \sin(2\pi \cdot f \cdot t) + 0.2 \cdot \sin(2\pi \cdot 4f \cdot t),$$
$$f = 1 \text{ kHz}$$

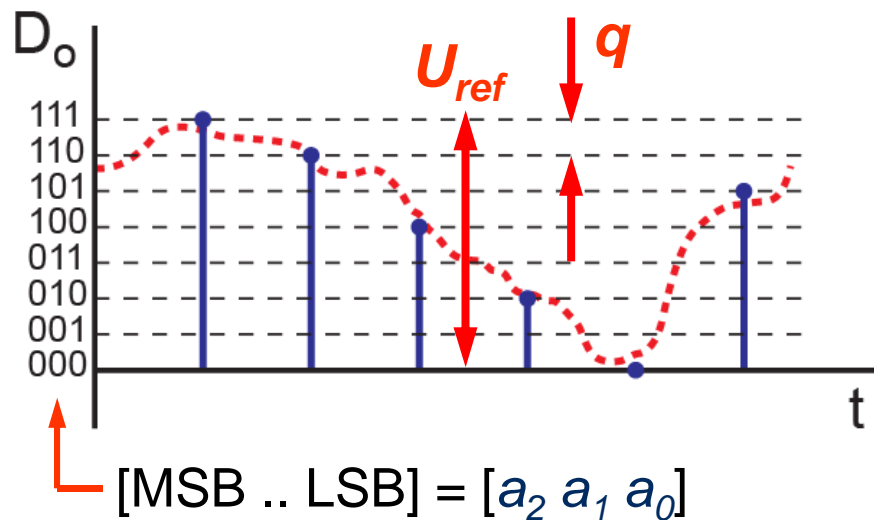
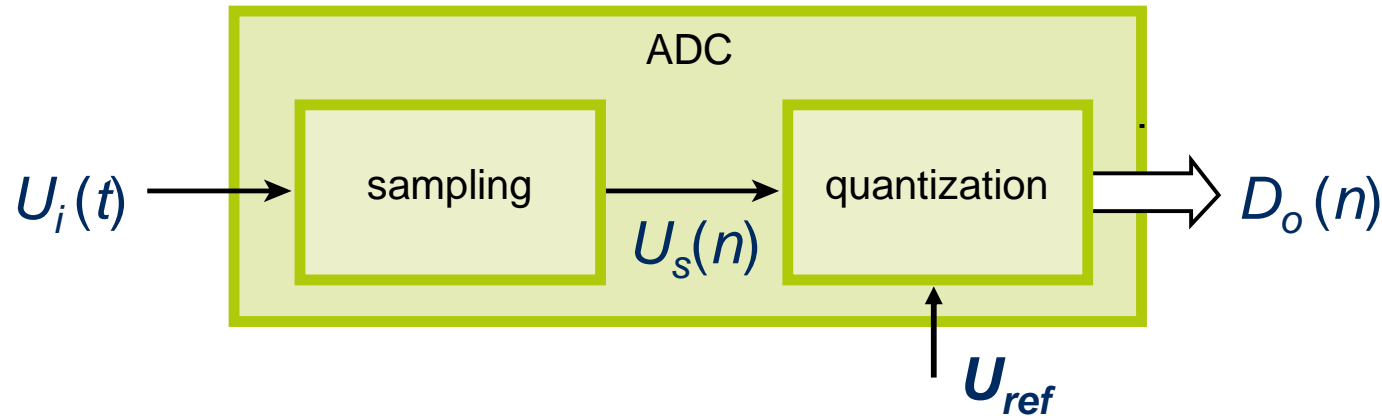
Quantization



quantized output signal

- sampled values are mapped onto a finite number of quantization levels
- the number of levels determines the **resolution**:
 n -bits ADC $\Leftrightarrow 2^n$ levels
- output D_o typically binary encoded using n bits

Quantization



- quantization levels defined w.r.t. **reference voltage** U_{ref}

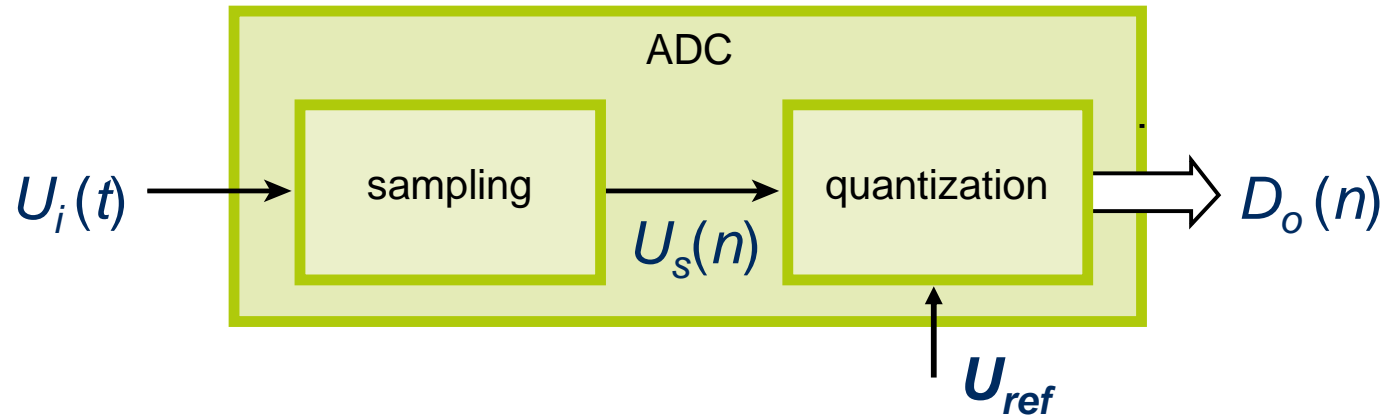
- quantization interval (LSB step):

$$q = \frac{U_{ref}}{2^n - 1} \approx \frac{U_{ref}}{2^n} \quad (n \gg 1)$$

- D_o yields U_i as fraction of U_{ref} :

$$U_i = a_{n-1} \frac{U_{ref}}{2} + a_{n-2} \frac{U_{ref}}{4} + \dots + a_0 \frac{U_{ref}}{2^n}$$

Quantization errors



- rounding error = **quantization error** ϵ_q

how big is the maximum ϵ_q of an 8-bits ADC with $U_{ref} = 1V$?



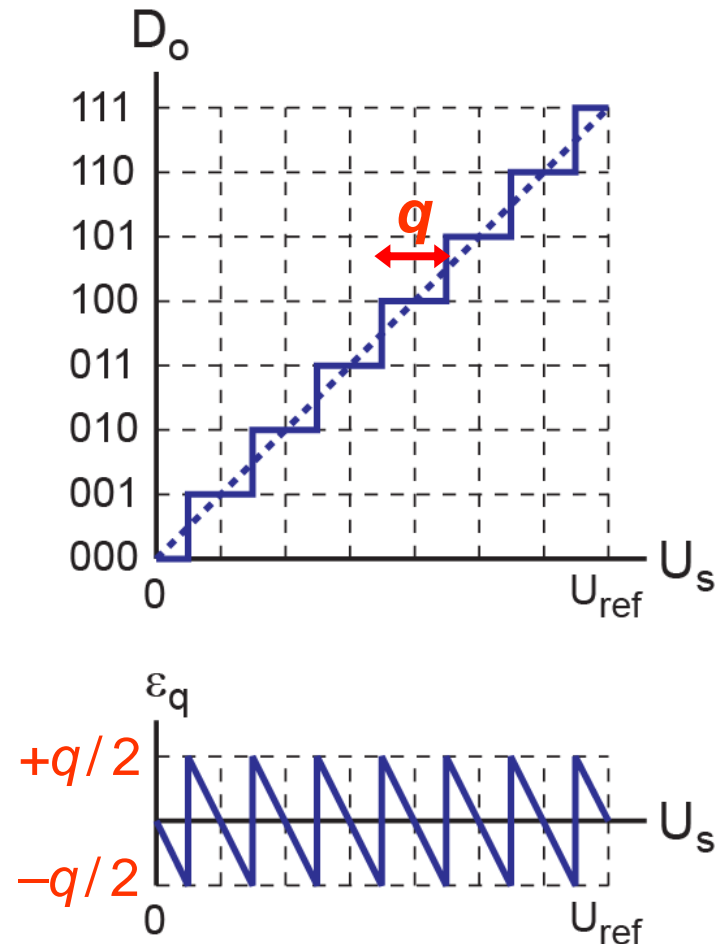
Quantization errors

- ideal transfer ADC:

- maximal quantization error ε_q

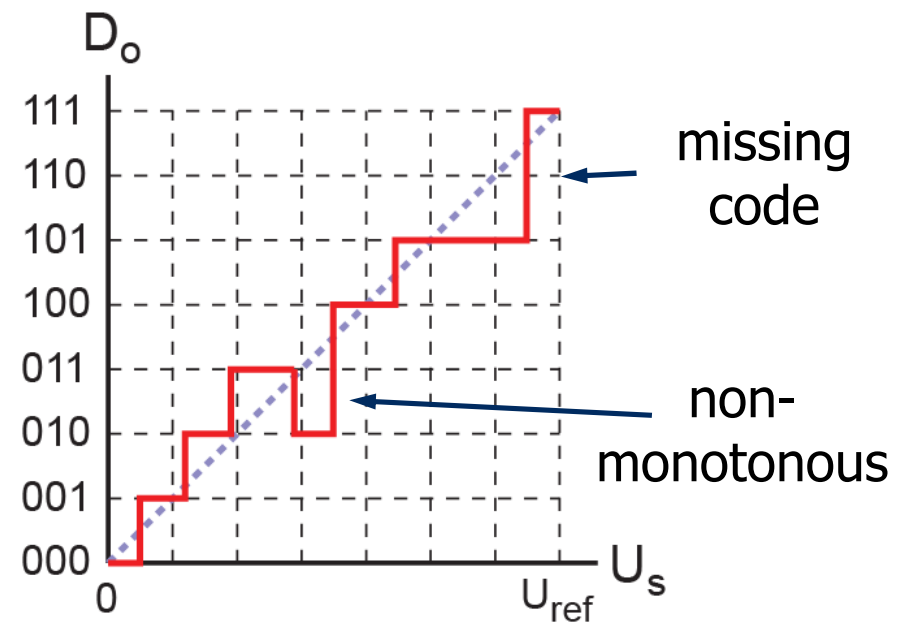
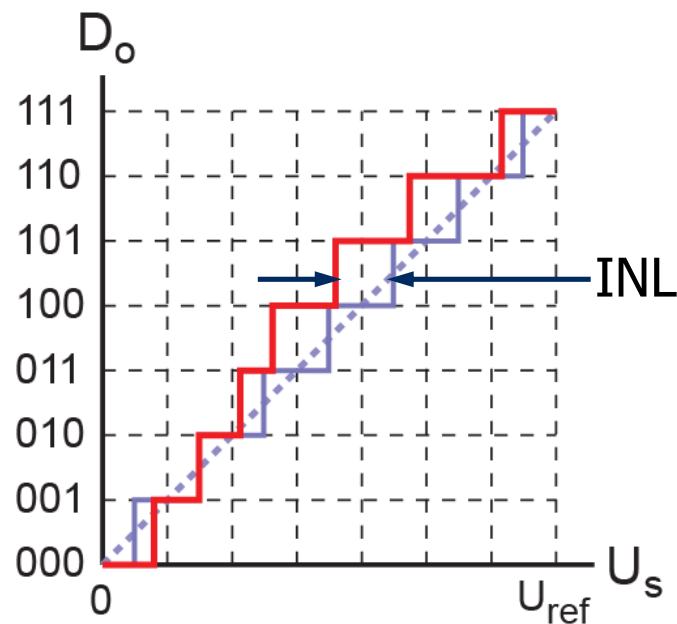
$$|\varepsilon_q| \leq \frac{q}{2} = \frac{U_{ref}}{2(2^n - 1)} \cong \frac{U_{ref}}{2^{n+1}} \quad (n \gg 1)$$

- corresponds to ± 0.5 LSB



Quantization errors

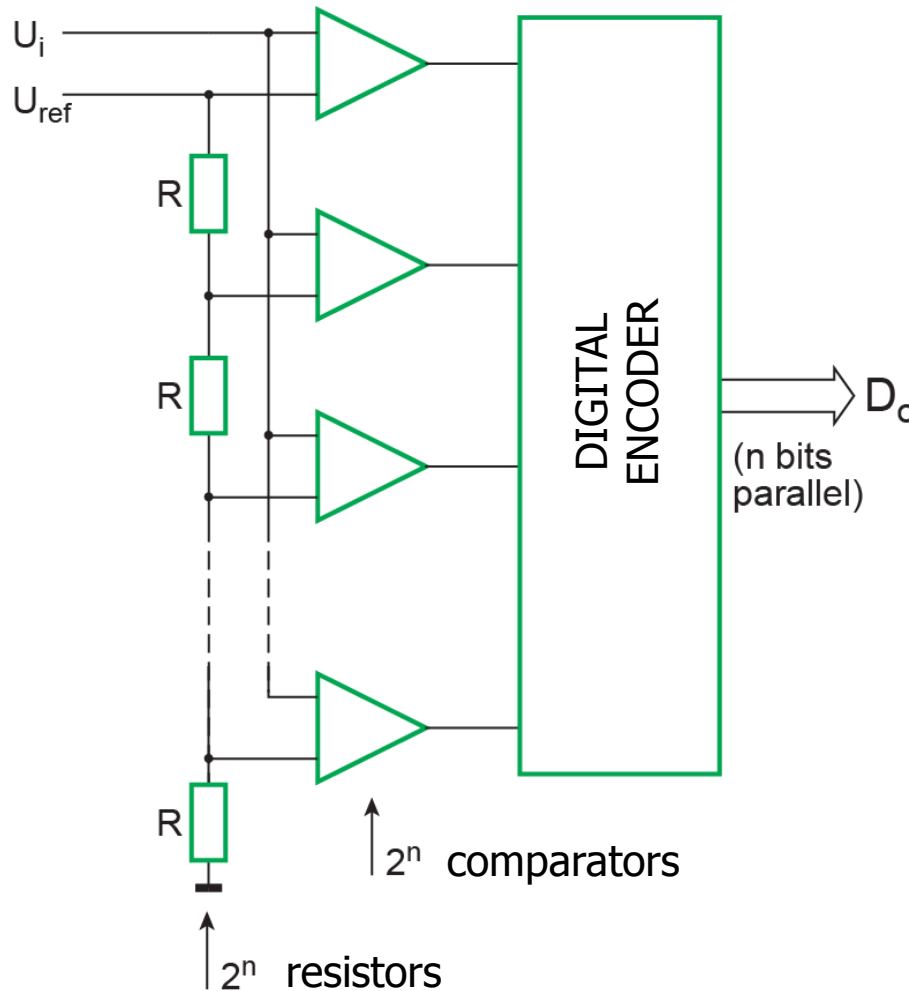
- In addition to (ideal) quantization errors, practical ADCs have more limitations:
 - offset and gain errors
 - non linearity: integral (INL), differential (DNL)
 - and sometimes: non-monotonous transfer (ambiguity) or missing codes



Types of analog-to-digital convertors

- **Direct** ADCs
 - conversion takes place in one step
 - example: flash ADC
- **Integrating** ADCs
 - conversion through an intermediate step: time period, frequency
 - example: dual-slope ADC
- **Compensating** ADCs
 - input signal is compensated (stepwise) by output signal of digital-to-analog convertor (DAC)
 - example: successive-approximation ADC (SAR ADC)

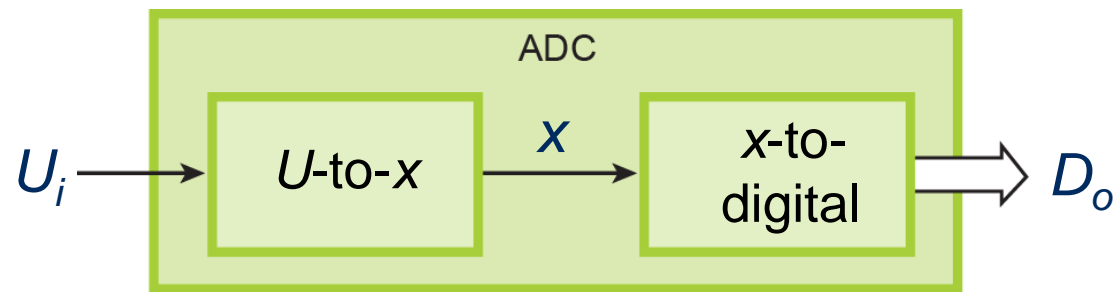
Flash ADC



- Resistive divider with 2^n resistors produces quantization levels
- Comparators compare U_i to quantization levels
- Encoder produces n -bit binary code
- Fast (>1 GHz possible), but many components!
- Can be found in digital oscilloscopes for example

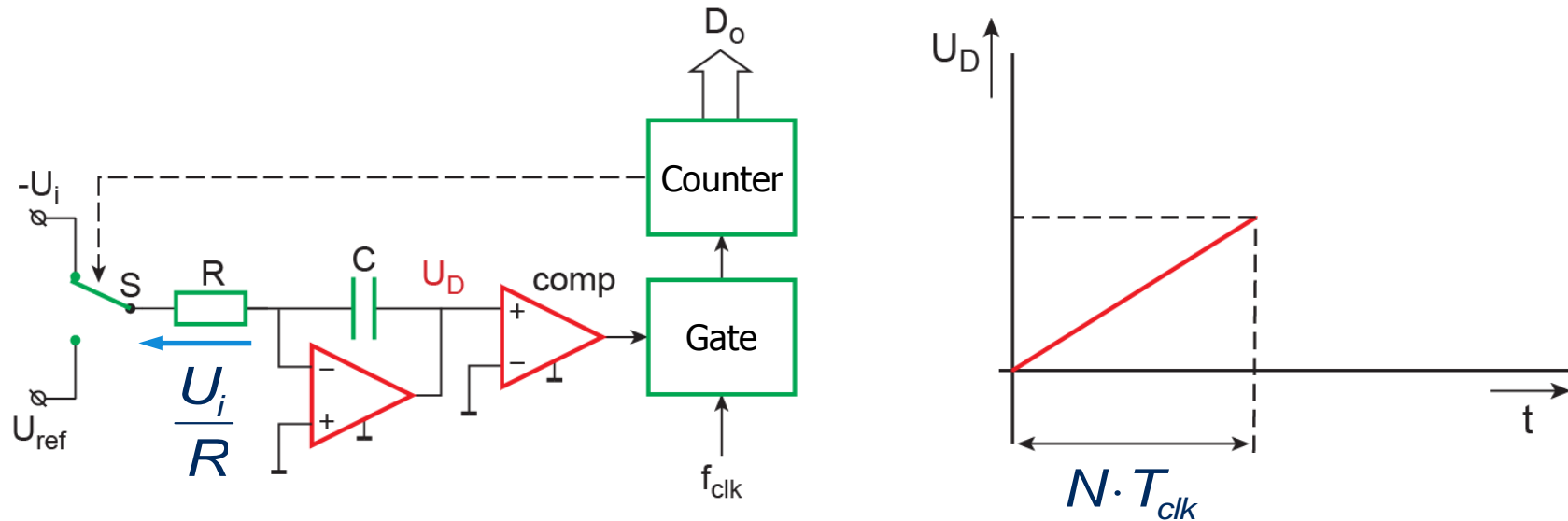
Indirect ADCs

- Use an intermediate step



- Intermediate signal x : time step, frequency, bitstream...
- Relatively slow, but a high resolution is possible
- Often used in multimeters

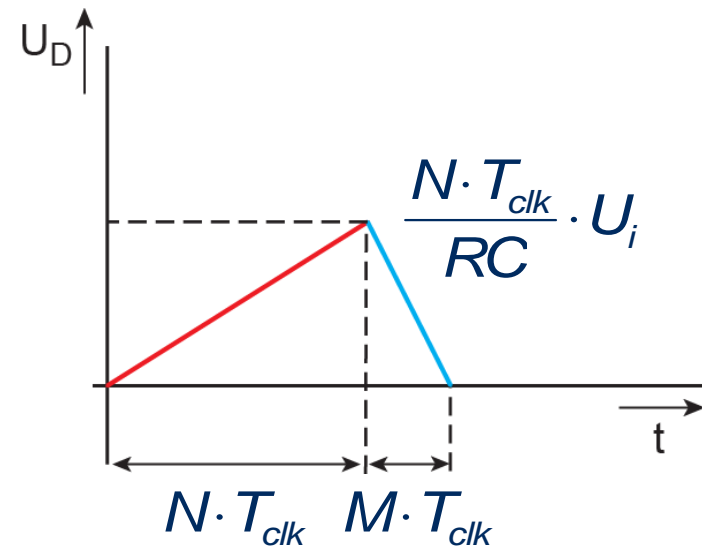
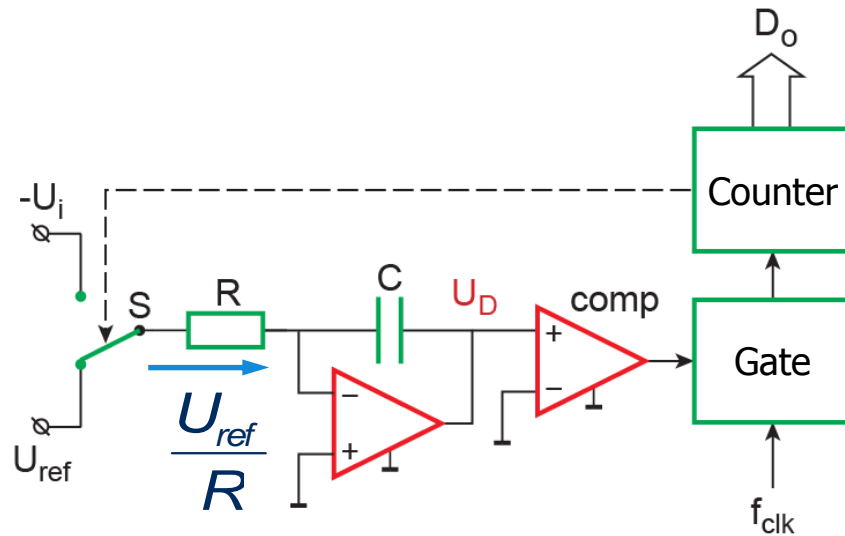
Dual-slope ADC



- Input signal is integrated over a fixed period $N \cdot T_{clk} = \frac{N}{f_{clk}}$

$$U_D = \frac{1}{RC} \int_0^{N T_{clk}} U_i(t) \cdot dt = \frac{N \cdot T_{clk}}{RC} \cdot U_i$$

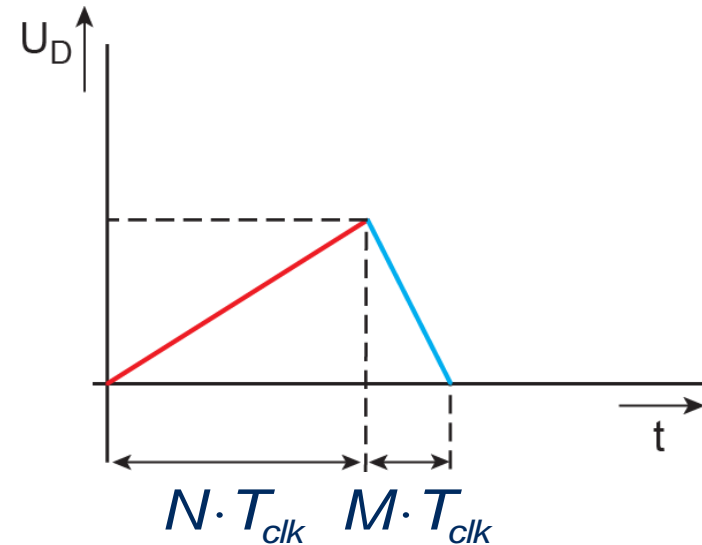
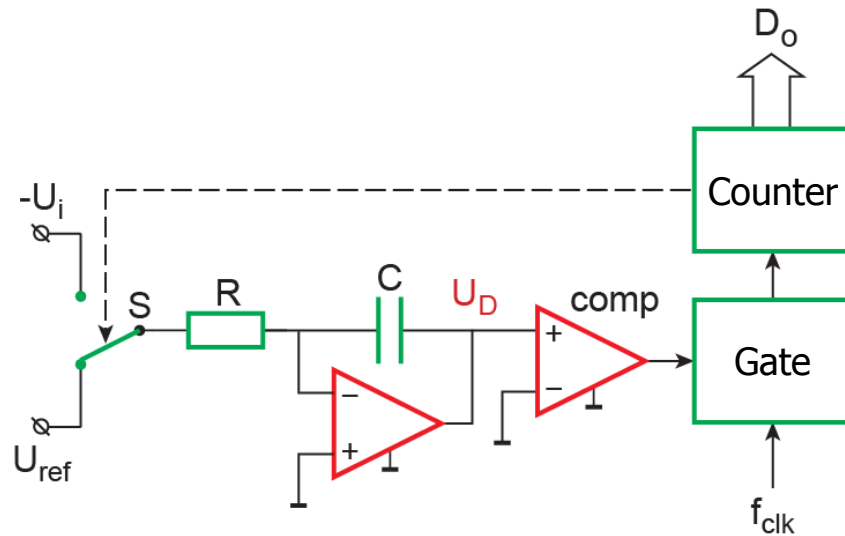
Dual-slope ADC



- Input signal is integrated over a fixed period $N \cdot T_{clk} = \frac{N}{f_{clk}}$
- Reference is integrated until U_D is back to 0

$$\frac{N \cdot T_{clk}}{RC} \cdot U_i = \frac{M \cdot T_{clk}}{RC} \cdot U_{ref} \Rightarrow M = \frac{U_i}{U_{ref}} N$$

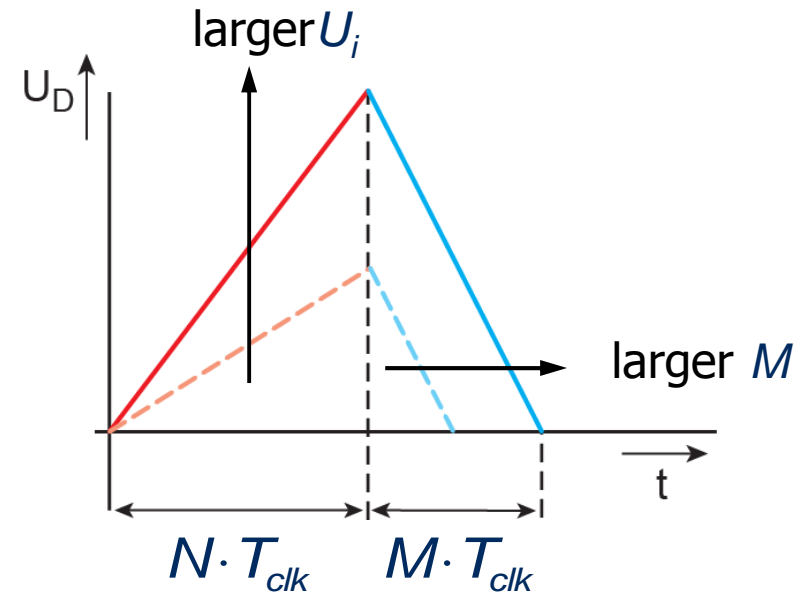
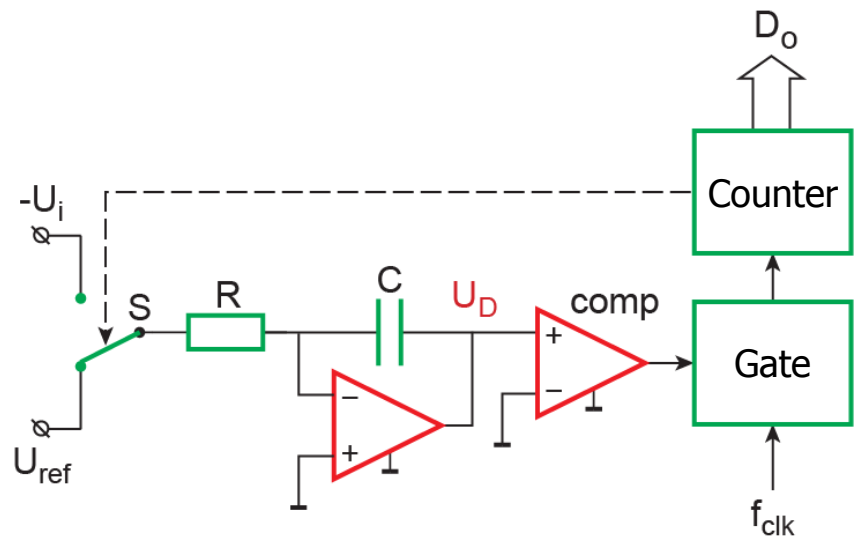
Dual-slope ADC



- Number of clock periods M is counted until U_D returns to 0 and is a direct measure for U_i / U_{ref} :

$$D_o = M = \frac{U_i}{U_{ref}} N$$

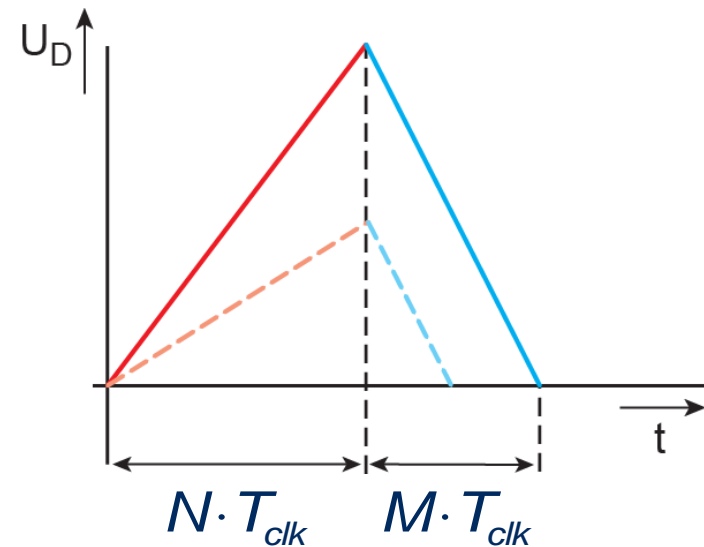
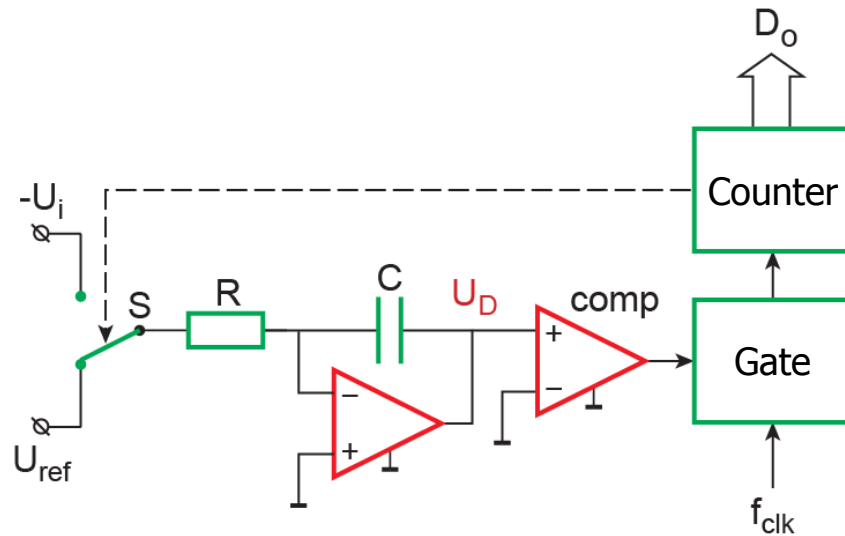
Dual-slope ADC



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Dual-slope ADC

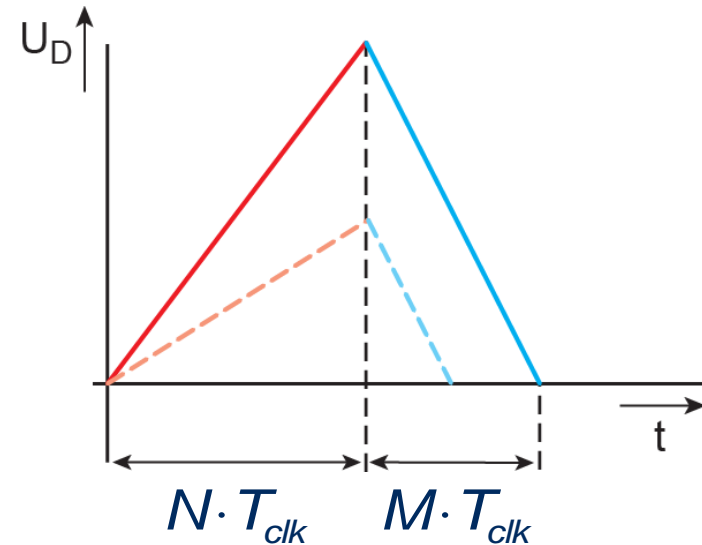
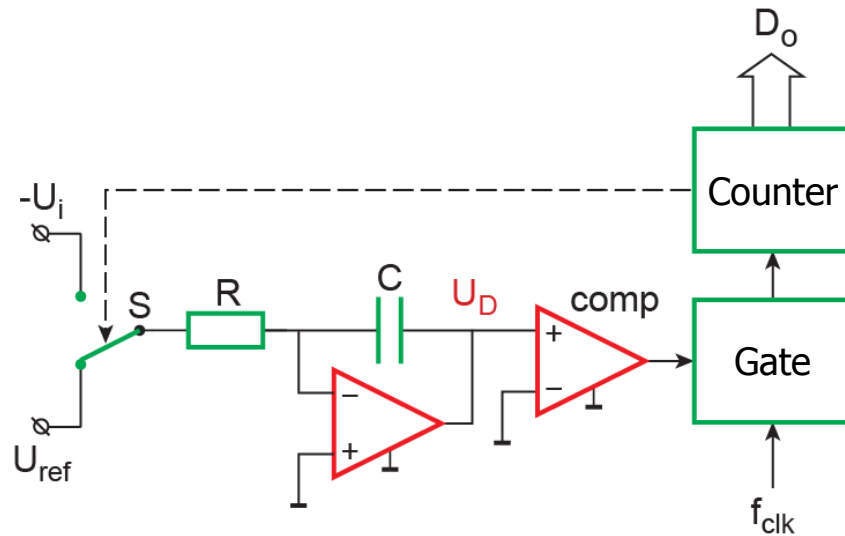


- Note:

- transfer independent of exact values of R , C
- U_i is integrated \Rightarrow noise / distortion are averaged out
- integration time $N \cdot T_{clk}$ is often a multiple of 20ms – why?

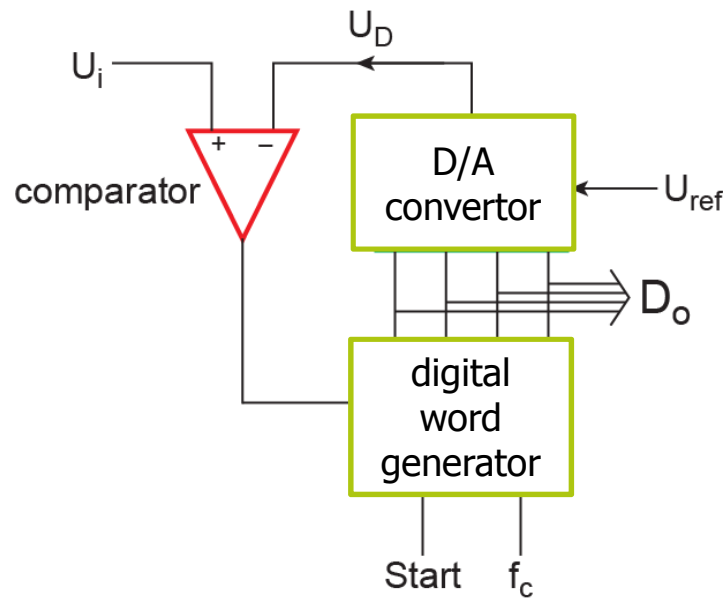


Exercise: dual-slope ADC



- Given: $U_{ref} = 1 \text{ V}$, $N = 16$
 - If the input $U_i = 0.25 \text{ V}$, what is the value of M ?
 - Which U_i result in a counter reading $M = 8$?
 - What is the resolution of this ADC?

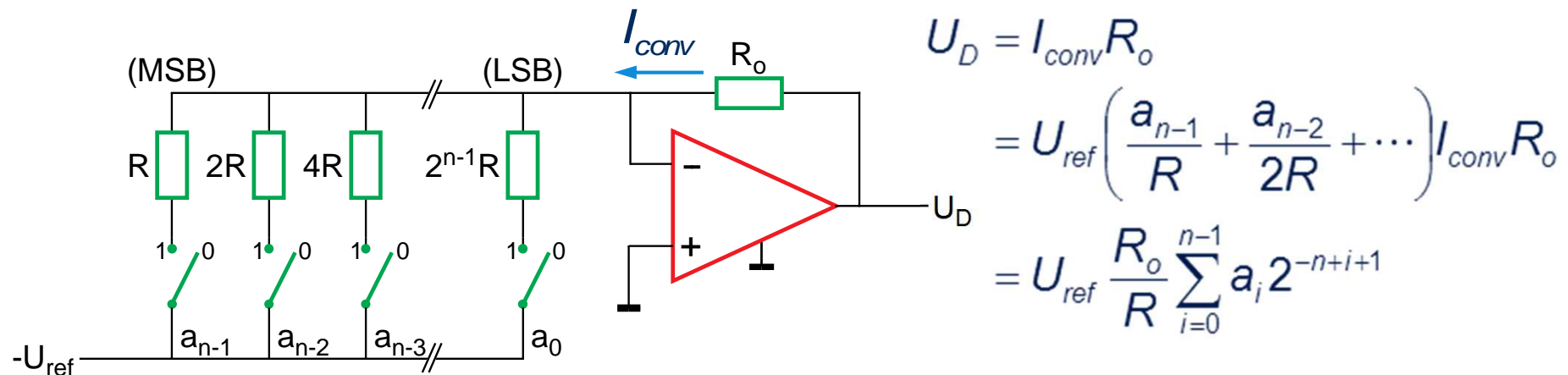
Compensating ADCs



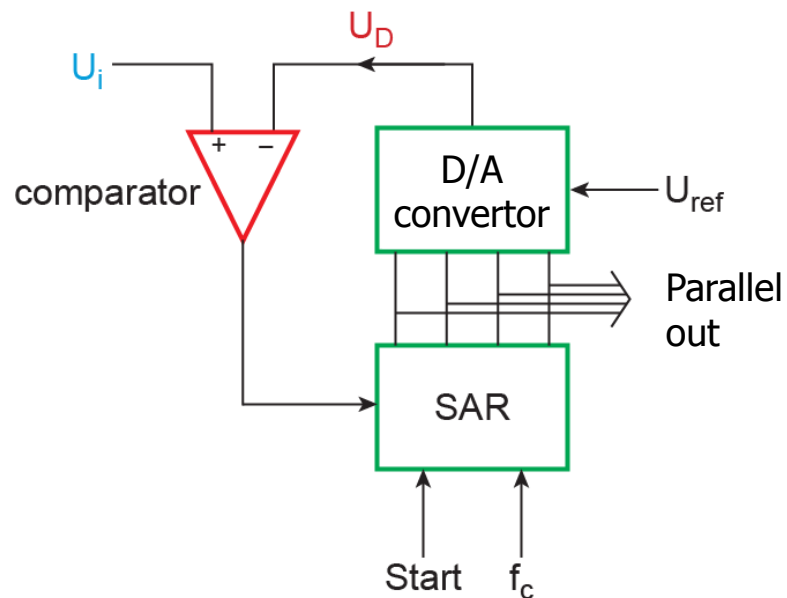
- Comparator compares U_i with output of a digital-to-analog convertor (DAC)
- Feedback: result is used to adjust input DAC (through an algorithm)
- Consequence: U_D tracks U_i
 $\Rightarrow D_o$ tracks U_i / U_{ref}
- Compensating ADCs are often found in data-acquisition systems

Digital-to-analog convertor

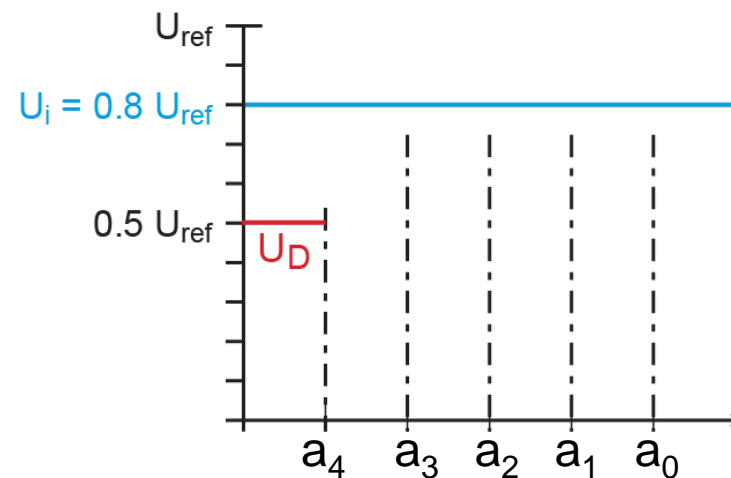
- Compensating ADCs need a DAC
 - determines resolution, linearity
- Example: DAC with binary-weighted resistors



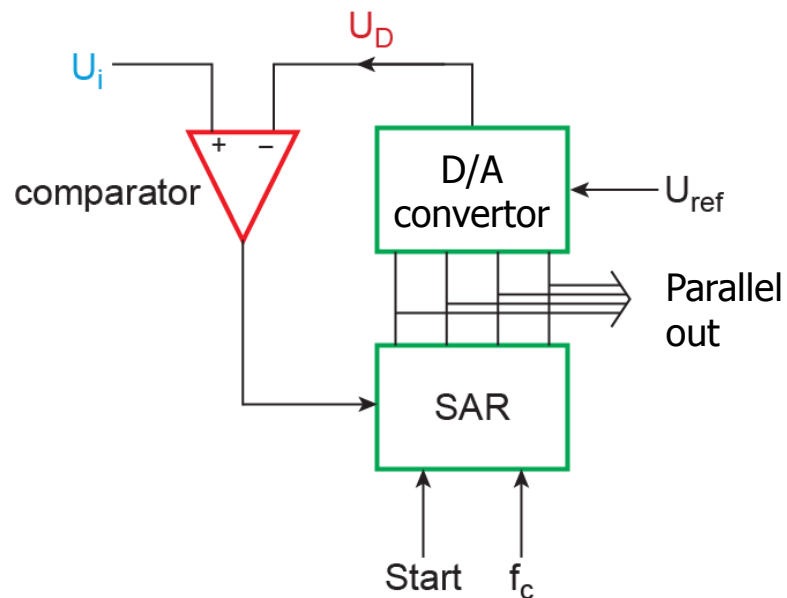
Successive-approximation ADC



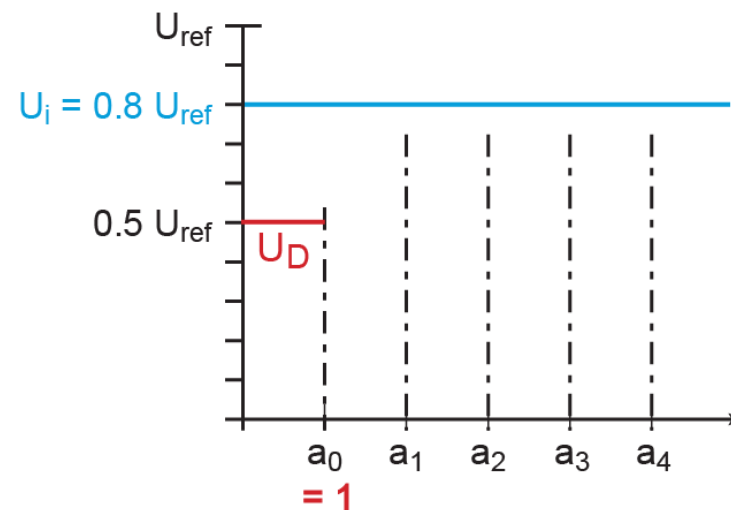
- U_D tracks U_i through a successive-approximation search algorithm



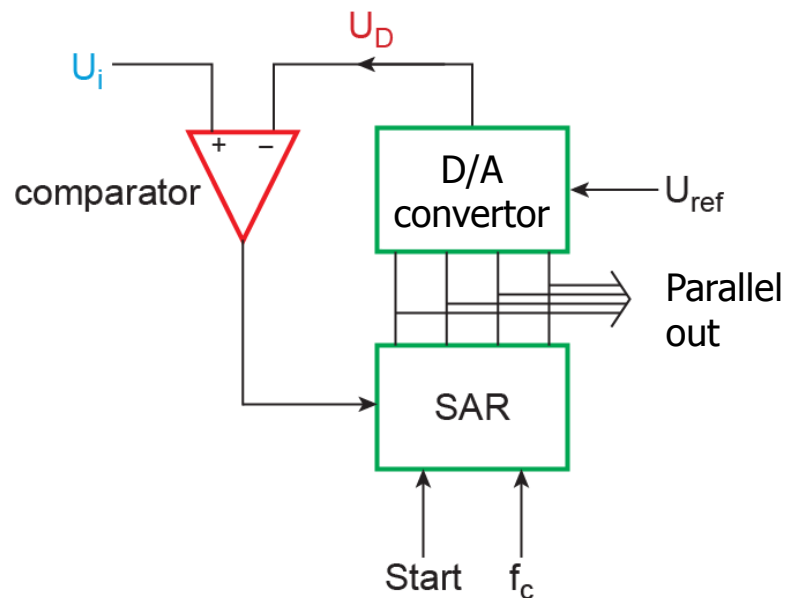
Successive-approximation ADC



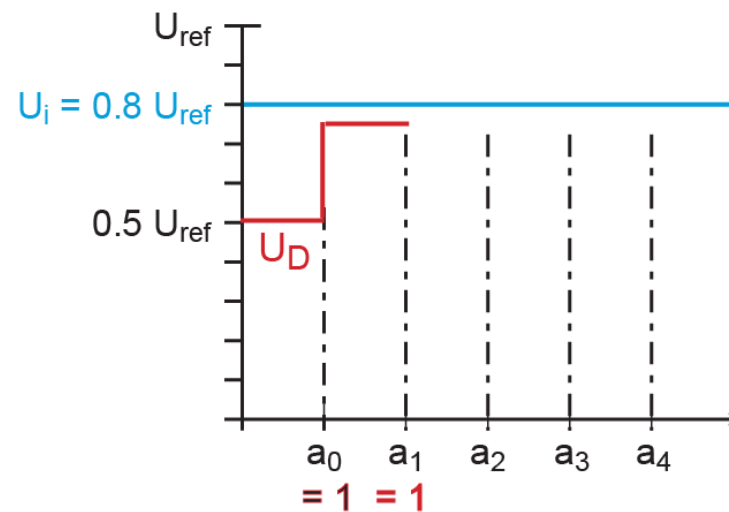
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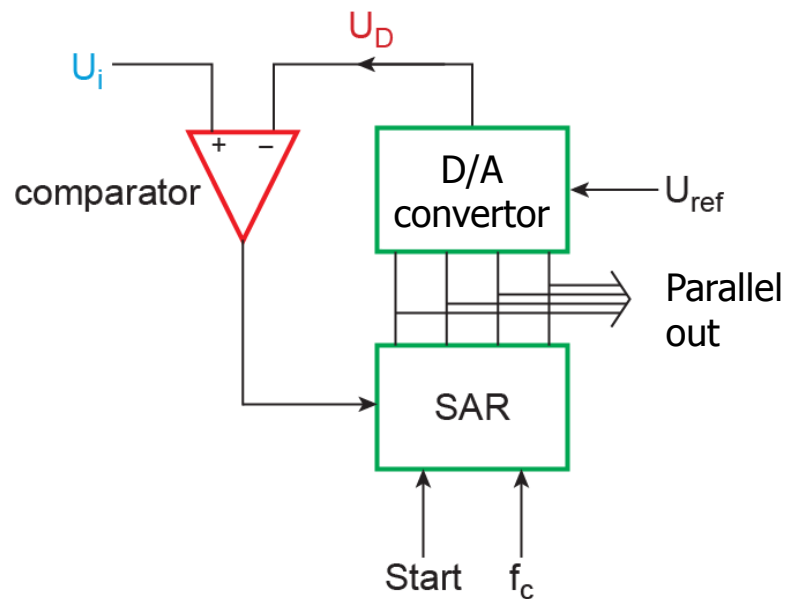
Successive-approximation ADC



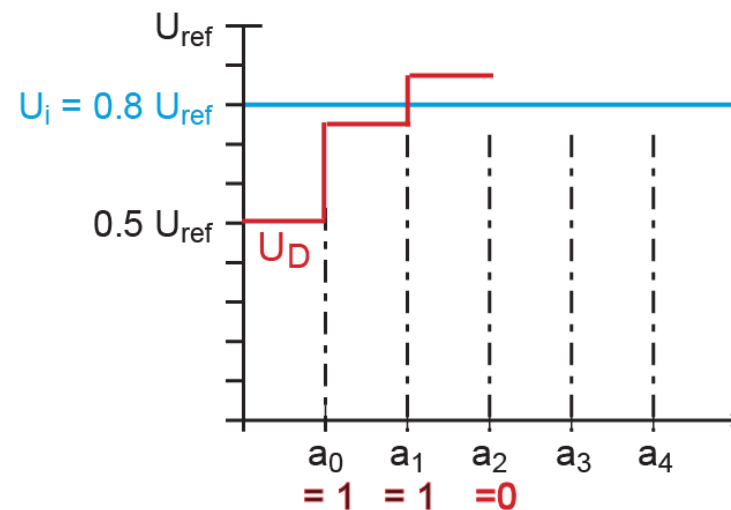
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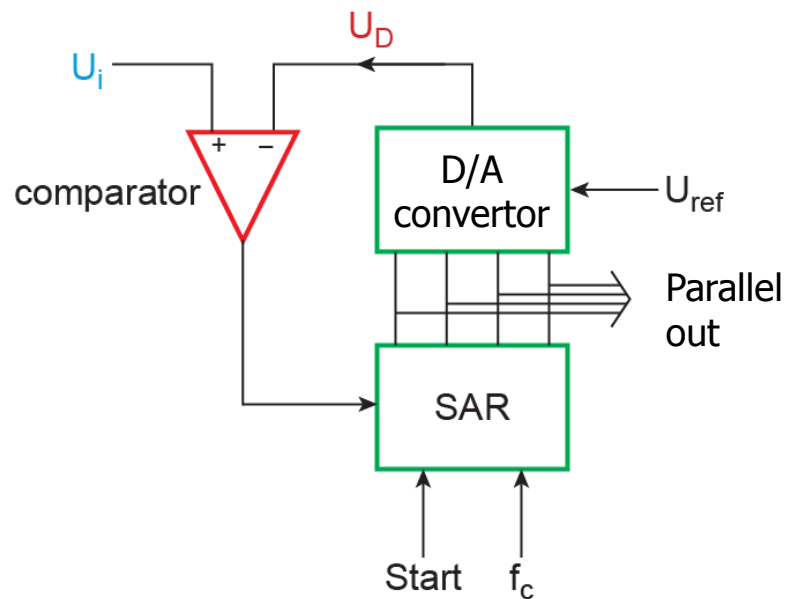
Successive-approximation ADC



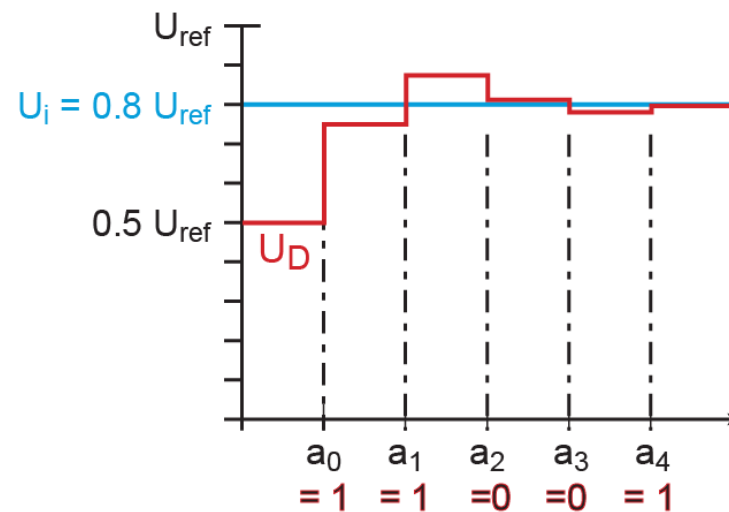
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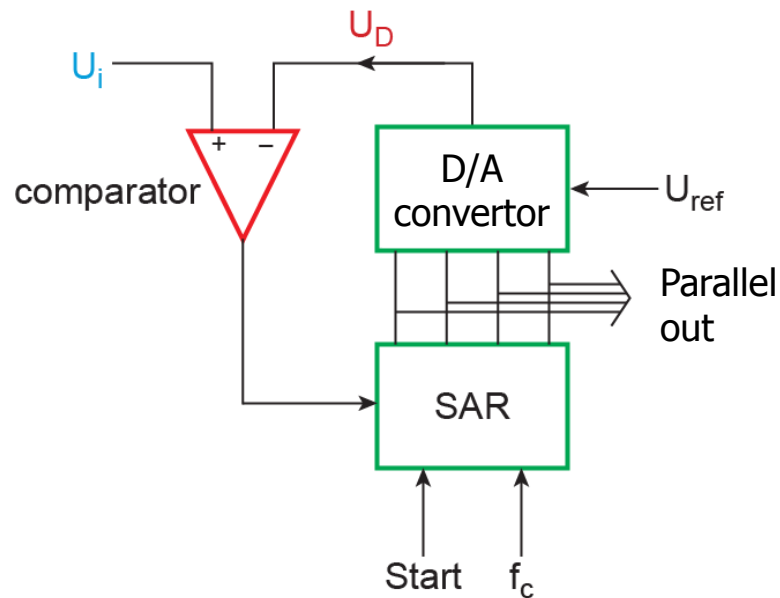
Successive-approximation ADC



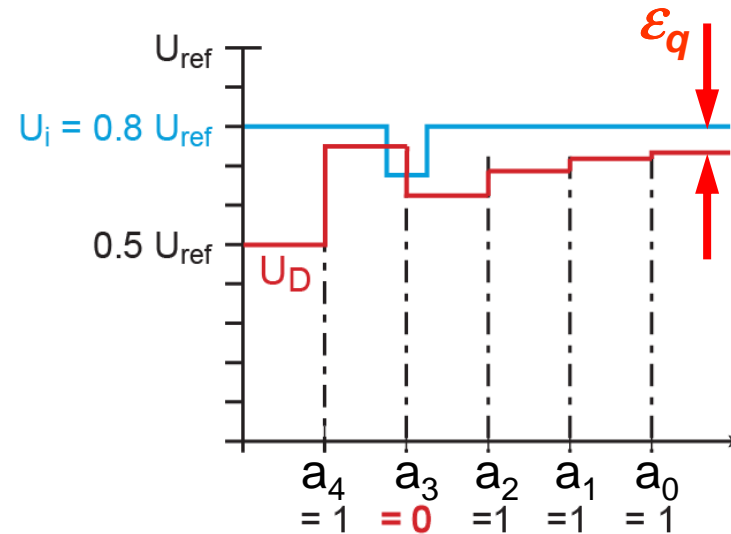
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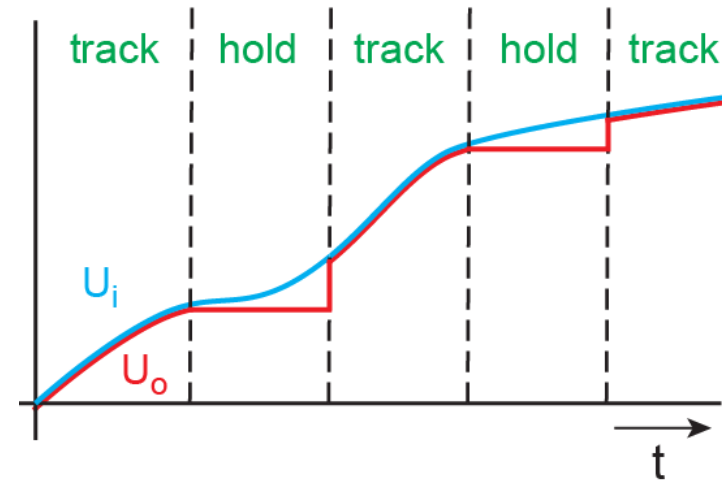
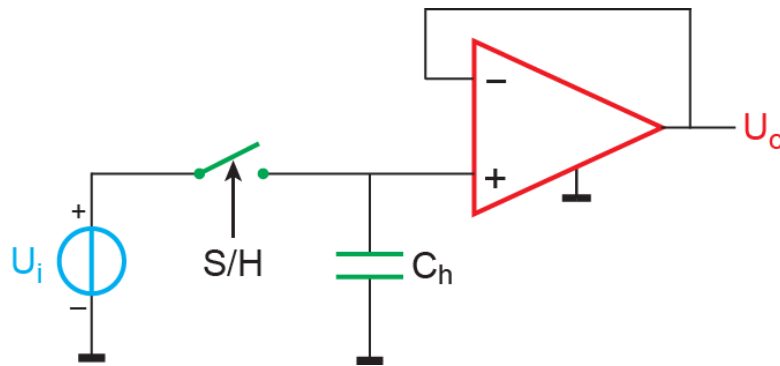
Importance of a stable input signal



- When U_i changes during the conversion, large errors can occur



Sample-and-hold circuit

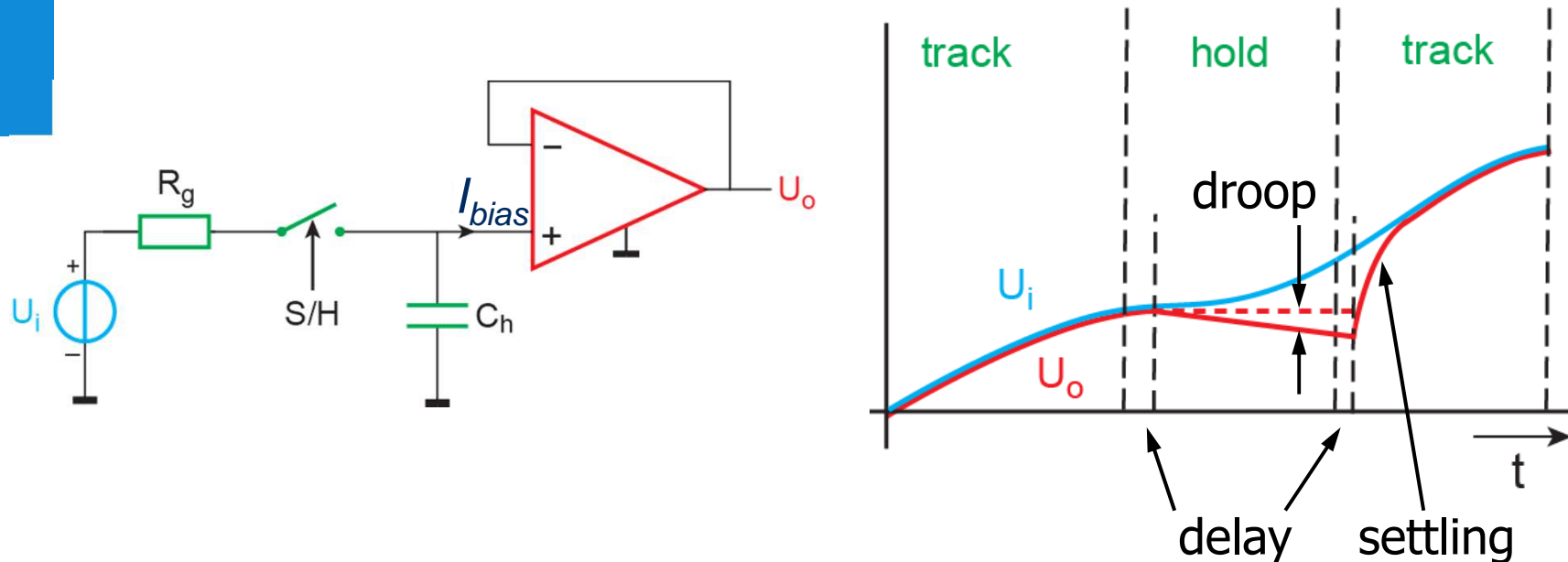


- track mode: output tracks input
- hold mode:
 - input voltage is stored in C_h
 - opamp manages buffering
- AD conversion during hold mode
⇒ variations in U_i do not disturb conversion

what are possible sources of error here??



Sample-and-hold sources of error



- **Delay:** at transitions between track and hold
- **Droop:** charge leaking from C_h due to bias current (I_{bias})
- **Settling:** limited tracking speed due to R_g and switch resistance R_{on} : $\tau = (R_g + R_{on}) \cdot C_h$

Summary

- ADCs convert a time- and amplitude-continuous input signal into a sampled and quantized output signal
- During sampling, the input signal is only passed at discrete time instances
 - Here, **aliasing** can occur
 - To prevent this, sampling has to be done at least at the **Nyquist** frequency: 2 x the highest frequency component
- Quantization maps the amplitude onto a digital code
 - Here, **quantization errors** occur, due to finite **resolution**

Summary

- Three frequently used ADC types:
- **Direct** ADCs:
 - single-step conversion
 - example: flash ADC in a digital oscilloscope
- **Integrating** ADCs:
 - conversion with an intermediate step (e.g. in the time domain)
 - example: dual-slope ADC in a digital multi-meter
- **Compensating** ADCs:
 - input signal is compensated by the output of a DAC
 - example: SAR ADC in a sensor interface

What's next?

- Study:
 - Regtien sections 2.1.1, 2.2.3, 18, 15.2.2
- Practice:
 - See the practice exercises on Blackboard!
- Questions, things unclear? Let me know!
M.A.P.Pertijs@tudelft.nl

Next time:
Measurement instruments