

# Stelsystem- en Regeltechniek II

Lecture 8 – Frequency Domain Design

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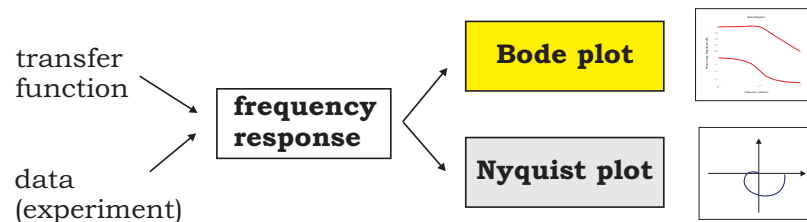
## Lecture Outline

Previous lecture: Bode plots, non-minimum-phase systems.

Today:

- Bode's gain-phase relation.
- Neutral stability.
- Gain and phase margin, performance specs.
- Controller design.

## Frequency Domain Methods



- Now we now how to sketch and plot Bode diagrams.
- The next step is analysis of system properties and design.

## Bode's Gain-Phase Relation

For any stable minimum-phase system, phase  $\angle G(j\omega)$  is uniquely related to magnitude  $|G(j\omega)|$ :

$$\angle G(j\omega_0) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{dM}{du} W(u) du$$

where  $M = \ln |G(j\omega)|$ ,  $u = \ln \omega/\omega_0$ ,  $W(u) = \text{ctanh}|u/2|$ .

For a constant slope, we can approximate the above by:

$$\angle G(j\omega_0) \simeq n \frac{\pi}{2}$$

where  $n$  is the slope ( 1 for 20 dB/dec, 2 for 40 dB/dec, etc).

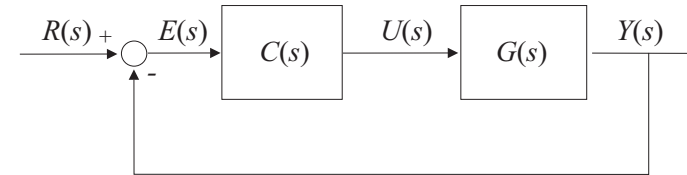
## Consequence of the Gain-Phase Relation

For open loop stable minimum-phase system, it is sometimes sufficient to look at the magnitude only.

This property can be used to derive a simple design rule for control.

But first, we must be able determine, from the Bode plot, whether the system is stable!

## Bode Plot: Closed-Loop Stability



$$L(s) = G(s)C(s)$$

Can we infer closed-loop stability from a Bode plot of the loop transfer function  $L(s)$ ?

## Proportional Controller: Loop Transfer

$$L(s) = \frac{Y(s)}{E(s)} = K G(s)$$

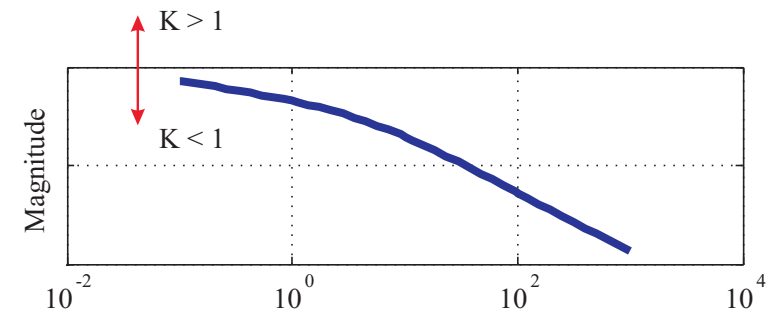
For the Bode plot, the following holds:

$$\angle G(j\omega) = \angle (KG(j\omega)) \quad (K \text{ is a real number})$$

$$|G(j\omega)| = |K| \cdot |G(j\omega)| \quad (\text{multiplication by a gain})$$

$$|G(j\omega)| \text{ dB} = |K| \text{ dB} + |G(j\omega)| \text{ dB}$$

## Proportional Controller: Loop Transfer



shift the magnitude response of  $G(j\omega)$  by  $20 \log(K)$   
phase does not change

## Example: DC Motor

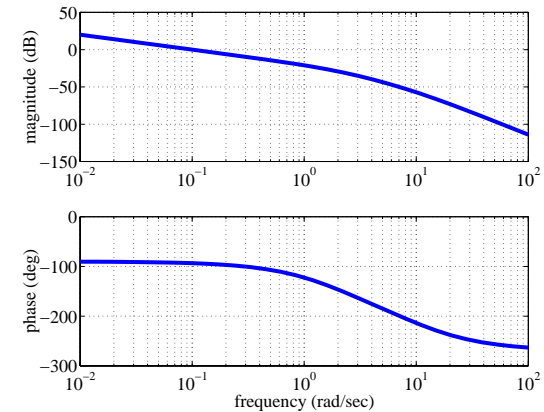
Transfer function:

$$G(s) = \frac{\theta(s)}{V(s)} = \frac{K_t}{s[(Ls + R)(Js + b) + K_t^2]}$$

inertia of the rotor	$J = 0.01 \text{ kg} \cdot \text{m}^2$
damping (friction)	$b = 0.1 \text{ Nms}$
back emf	$K_t = 0.01 \text{ Nm/A}$
resistance	$R = 1 \Omega$
inductance	$L = 0.5 \text{ H}$

## DC Motor: Open-Loop Bode Plot

$$G(s) = \frac{\theta(s)}{V(s)} = \frac{2}{s(s+10)(s+2)}$$



## Influence of Proportional Gain

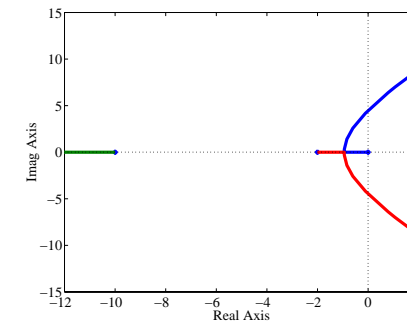
$$L(s) = KG(s) = \frac{K \cdot 2}{s(s+10)(s+2)}$$

Use Matlab: `sisotool('bode',G)`

OK, the magnitude moves up and down with the gain and the phase does not change ...

... but, is there anything on the Bode plot that would hint on the stability of the closed loop?

## Let's See Whether Root Locus Helps ...

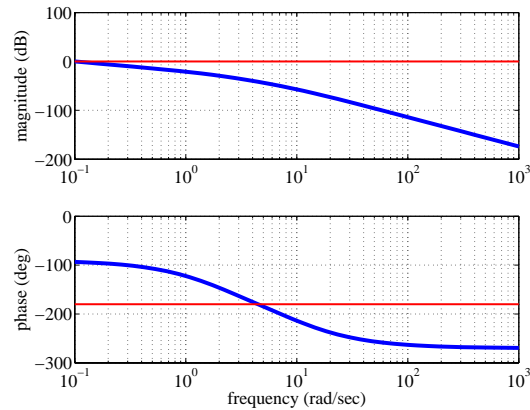


Basic properties of RL:  $\angle G(s) = -180^\circ$  and  $|KG(s)| = 1$

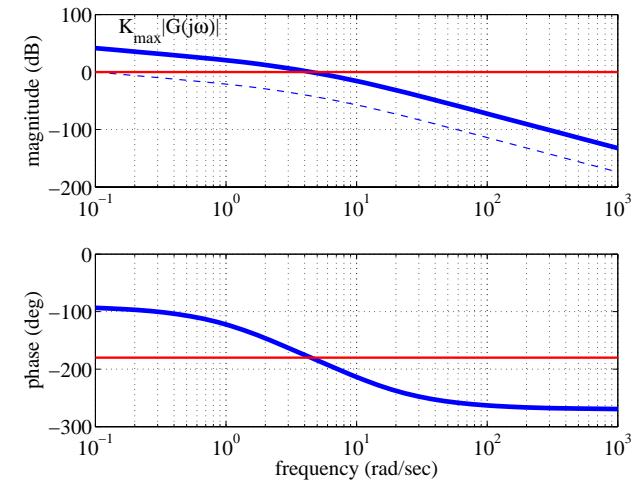
Neutral stability:  $|K_{\max}G(j\omega)| = 0 \text{ dB}$  and  $\angle G(j\omega) = -180^\circ$

## Back to the Bode Plot

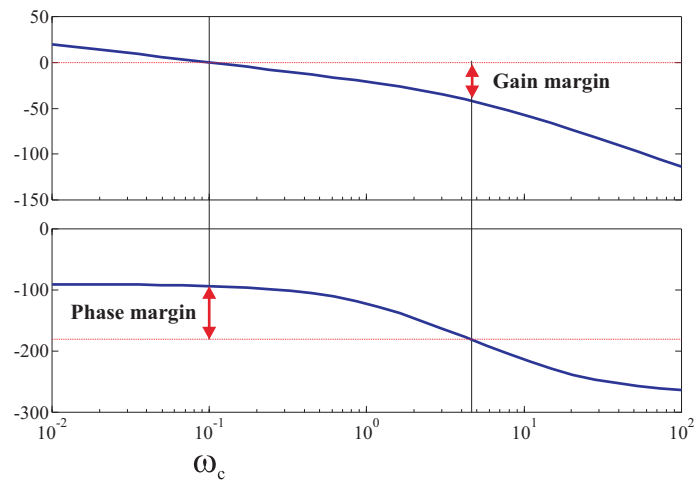
System is stable if:  $|KG(j\omega)| < 0$  dB at  $\angle G(j\omega) = -180^\circ$



## Point of Neutral Stability



## Crossover Frequency and Stability Margins



## Crossover Frequency and Stability Margins

- The crossover frequency  $\omega_c$  is the frequency for which the loop TF has gain 0 dB.
- The gain margin (GM) is the factor (or amount dB) by which the loop gain can be raised before instability occurs.
- The phase margin (PM) is the amount (in degrees) by which the phase exceeds  $180^\circ$  at  $\omega_c$ .

## Importance of Stability Margins

The margins tell us how far the closed-loop system is from the point of neutral stability. This indicates the robustness w.r.t. uncertainty in the plant model:

- Gain margin: by what factor the total process gain can increase.
- Phase margin: by how much the phase can decrease.

and performance:

- Phase margin: related to closed loop damping (overshoot).
- Crossover frequency: related to response speed (bandwidth).

## Robustness: Example

Suppose our model is:

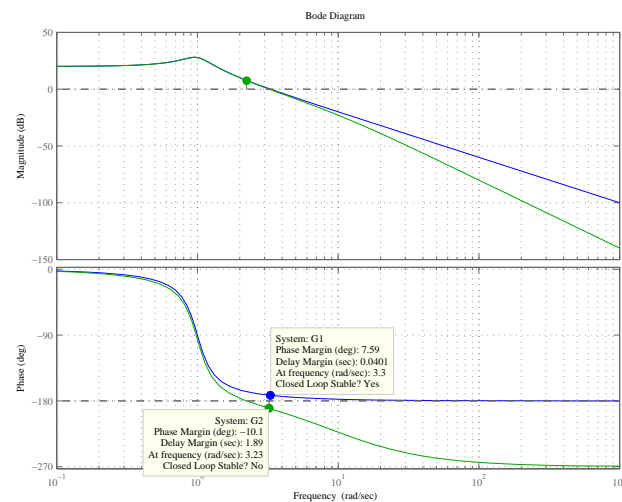
$$\hat{L}(s) = \frac{10}{s^2 + 0.4s + 1}$$

while the true plant is:

$$L(s) = \frac{10}{(s^2 + 0.4s + 1)(0.1s + 1)}$$

Relatively small mismatch in terms of step-response behavior, major difference in terms of closed-loop stability!

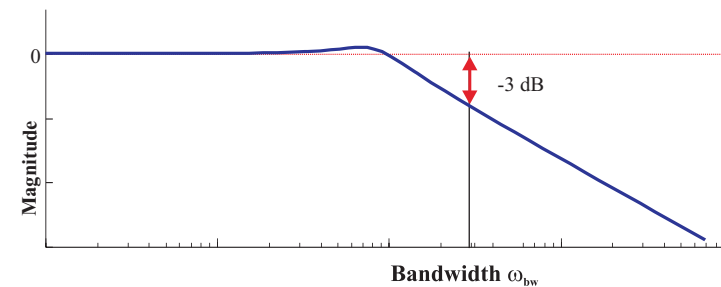
## Bode Plot of Model and True Plant



## Closed-Loop Bandwidth

Bandwidth = frequency up to which the input is “well reproduced” at the output of the closed-loop system.

Defined as frequency  $\omega_{bw}$  at which the magnitude has an attenuation of 0.707 (3dB) – corresponds to 0.5 power gain.



## Bandwidth and Crossover Frequency

Typically:

$$\omega_c \leq \omega_{bw} \leq 2\omega_c$$

The required speed of response (e.g., the settling time or rise time) can be expressed in terms of  $\omega_c$ . Recall:

$$t_r = 1.8/\omega_n$$

(for second-order dominant response).

## Phase Margin and Overshoot

The larger PM, the larger damping (less overshoot):

$$\zeta \approx \frac{\text{PM}}{100}$$

this holds up to  $\text{PM} = 60^\circ$

See the Franklin et al. for a graphical relationship between the overshoot and PM (page 357).

## Recall Specs for Second-Order Systems

$$t_r = \frac{1.8}{\omega_n}$$

$$t_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}}$$

$$t_s = \frac{4.6}{\zeta \omega_n} \quad \text{for } \pm 1\%$$

$$M_p = e^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}}$$

## More Complex Plants

- System unstable for small  $K$  and stable for large  $K$ , e.g.,:

$$L(s) = \frac{K(s+2)}{s^2-1}$$

- Conditionally stable systems (unstable for small and large  $K$ , stable for some intermediate values), e.g.,:

$$L(s) = \frac{K(s+2)}{(s+10)^2(s+1)(s-1)}$$

In the sequel, we consider systems with no poles in RHP.

## The Basic Idea

- Adjust the proportional gain to get the required crossover frequency and/or steady-state tracking error.
- If needed, use the derivative action to add phase in the neighborhood of  $\omega_c$  in order to increase the phase margin.
- If needed, use the integral action to increase the gain at low frequencies in order to guarantee the required steady-state tracking error.

## Bode Plots: Homework Assignments

- Read Sections 6.1 through 6.6, except for the Nyquist criterion.
- Work out examples in these sections and verify the results by using Matlab.
- Reproduce the derivation of the frequency response as given on the overhead sheets.
- Work out a selection of problems 6.3 through 6.9 and verify your results by using Matlab.