

Fluid mechanics (wb1225)

Lecture 11: Flow past immersed bodies

Tacoma Narrows Bridge



[1]



Noren krijgen optie op nieuw snel schaatspak

De Poolse schaatser Pavek Zygmunt demonstreerde dinsdag in een windtunnel in Delft een nieuw schaatspak. Omdat de Nederlanders in Salt Lake City verplicht in kleding van Nike uitkomen, krijgt Noorwegen de optie op het in Delft ontwikkelde nieuwe schaatspak, waarvan een rendement van ongeveer vijf procent wordt verwacht. Het Deltapak 'Flash' is de doorstart van de strips die vier jaar geleden in Nagano mede bijdroegen aan de Nederlandse successen.

FOTO ANP

[2]

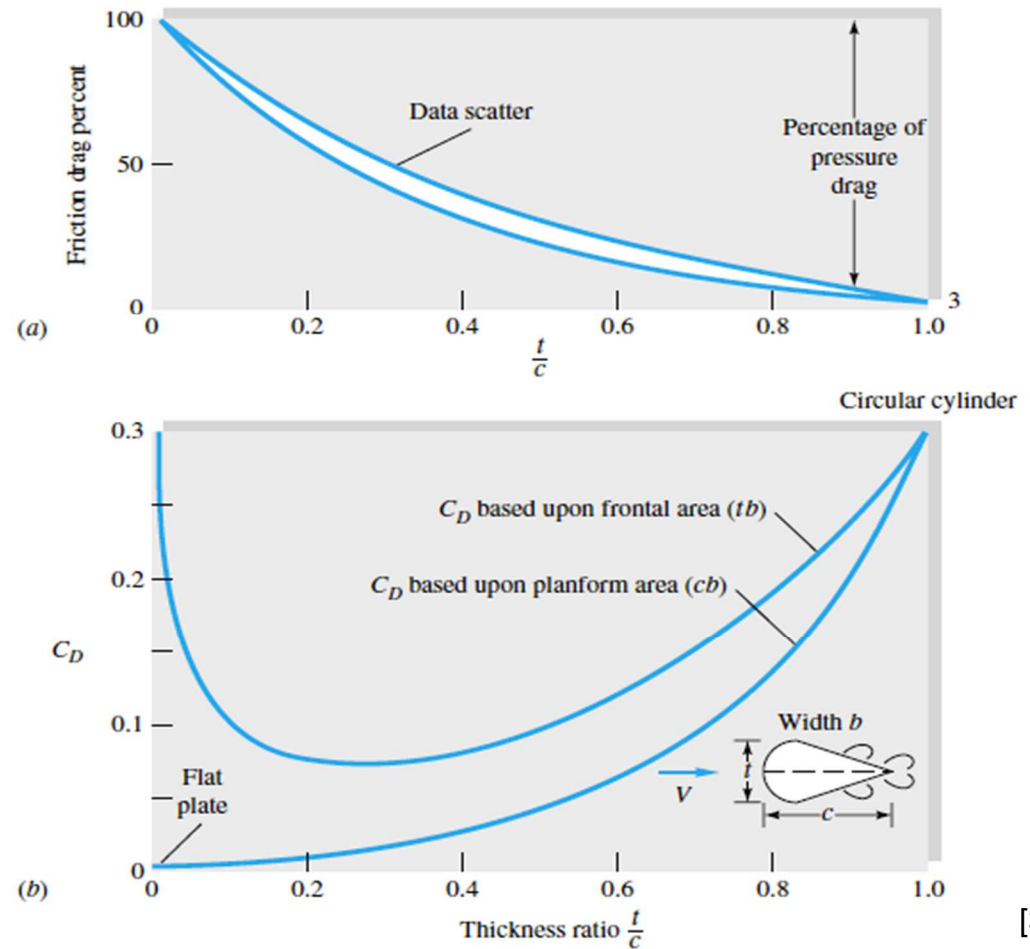
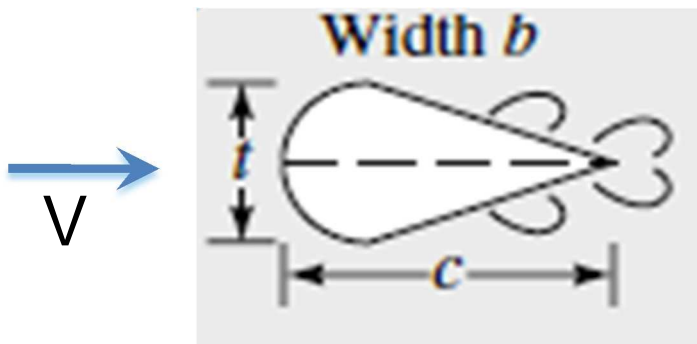
Drag on immersed body

$$C_D = \frac{\text{drag}}{\frac{1}{2} \rho V^2 A}$$

$$C_D = C_{D,\text{pressure}} + C_{D,\text{friction}}$$

$$A = \begin{cases} \text{frontal area} \\ \text{planform area} \end{cases}$$

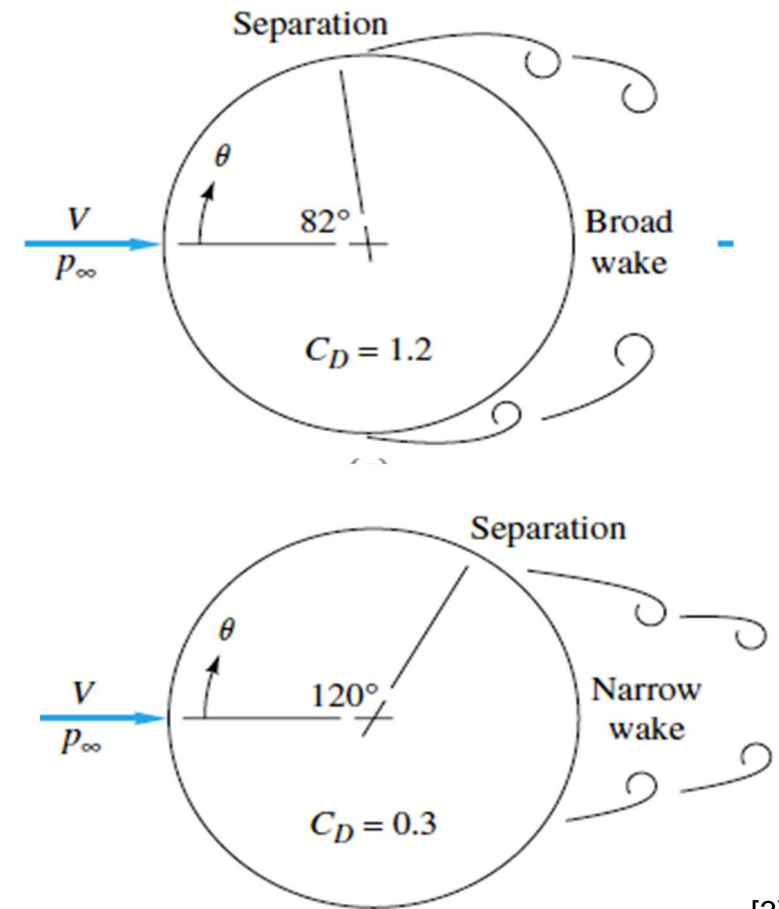
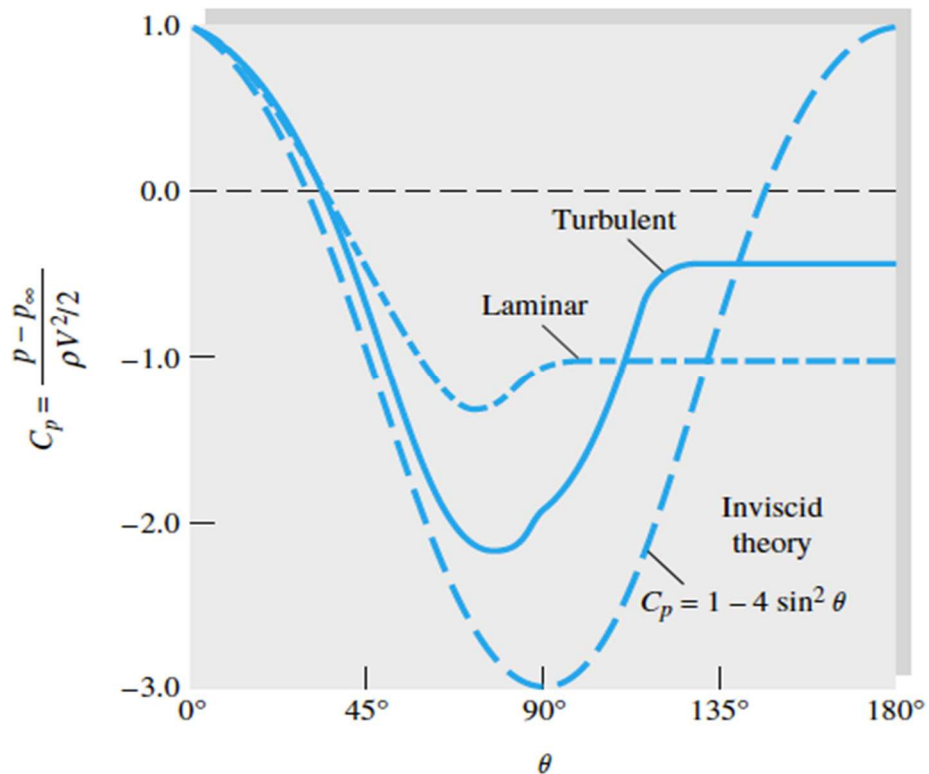
Streamlined cylinder



[3]

Pressure distribution

$$C_P = \frac{p - p_\infty}{\frac{1}{2} \rho V^2} = 1 - 4 \sin^2 \theta$$

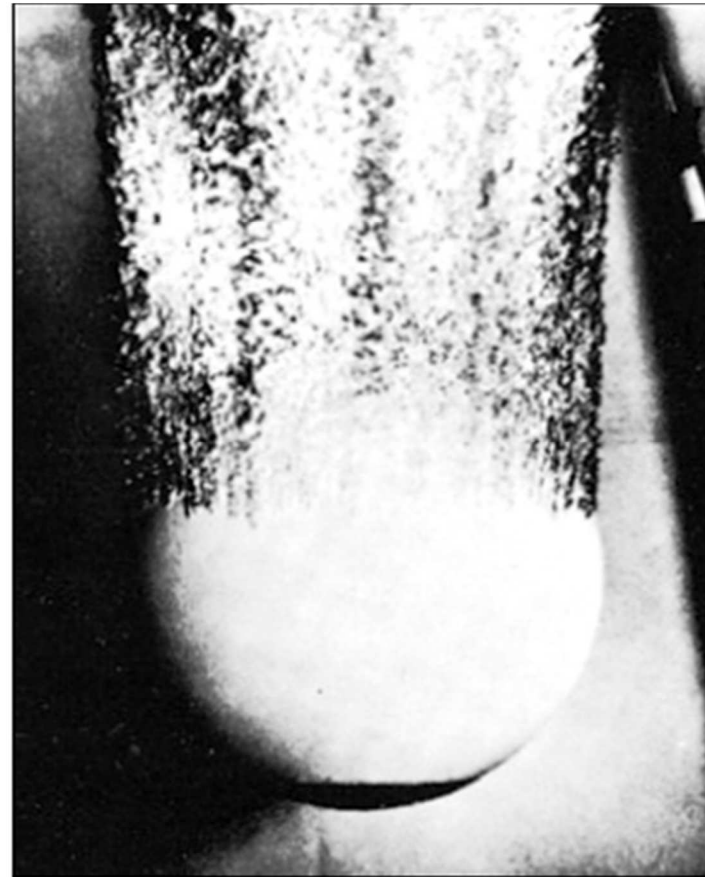


[3]

Laminar vs turbulent flow



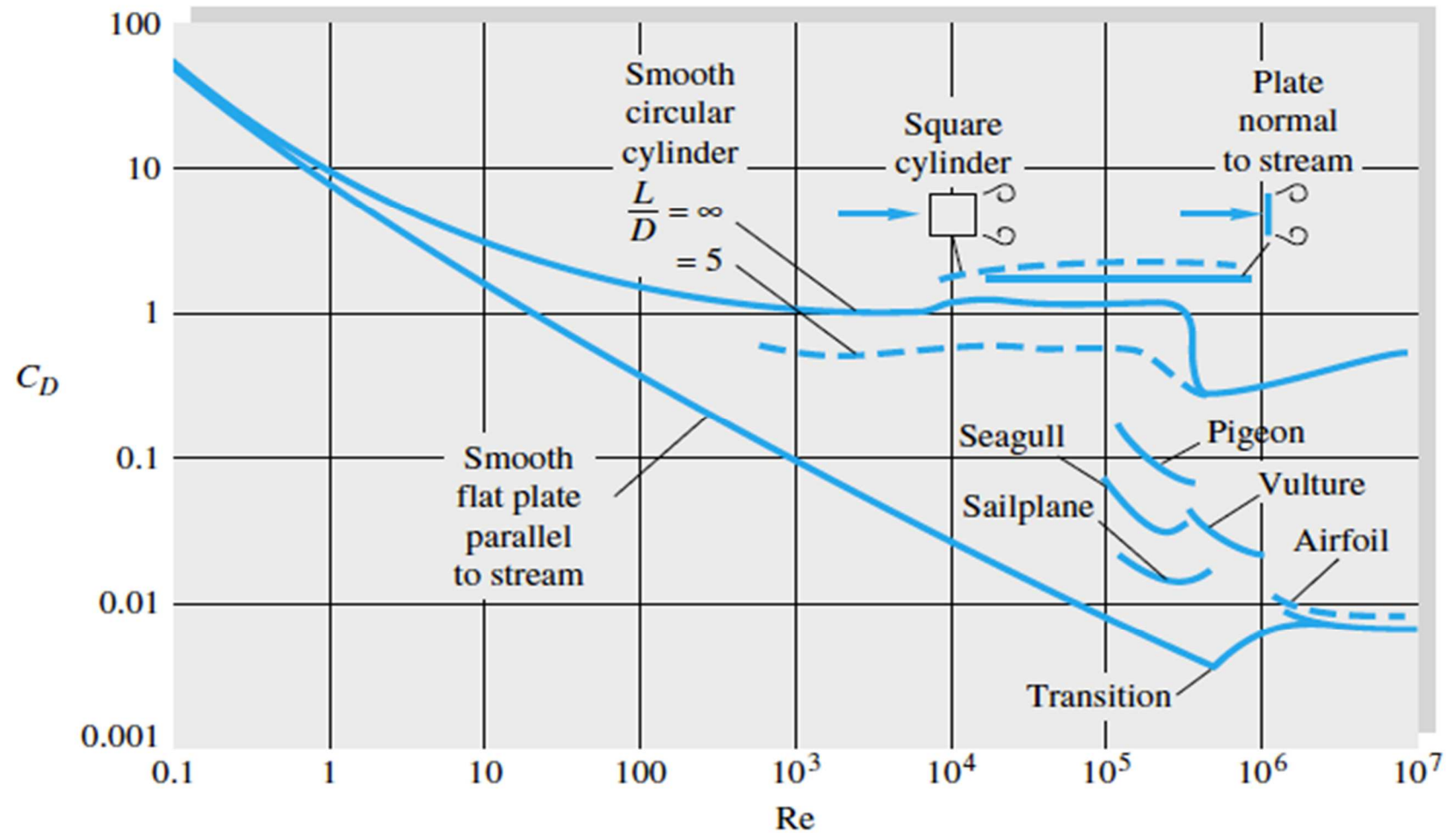
laminar



turbulent

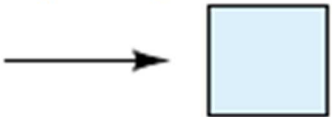
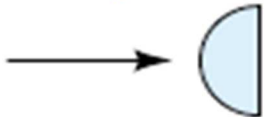
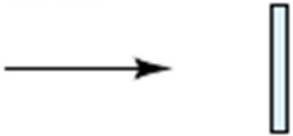
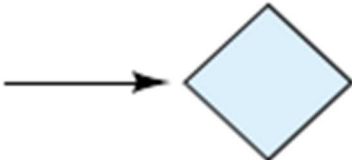
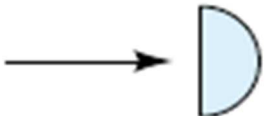
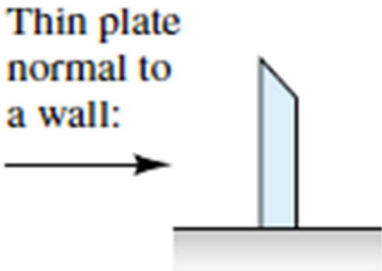
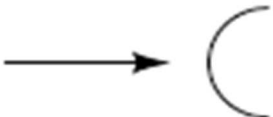
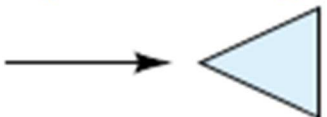
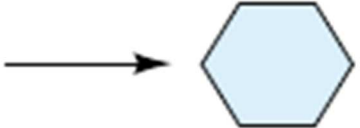
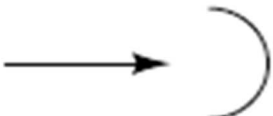

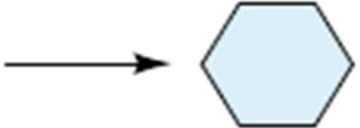
[3]

Arbitrary objects



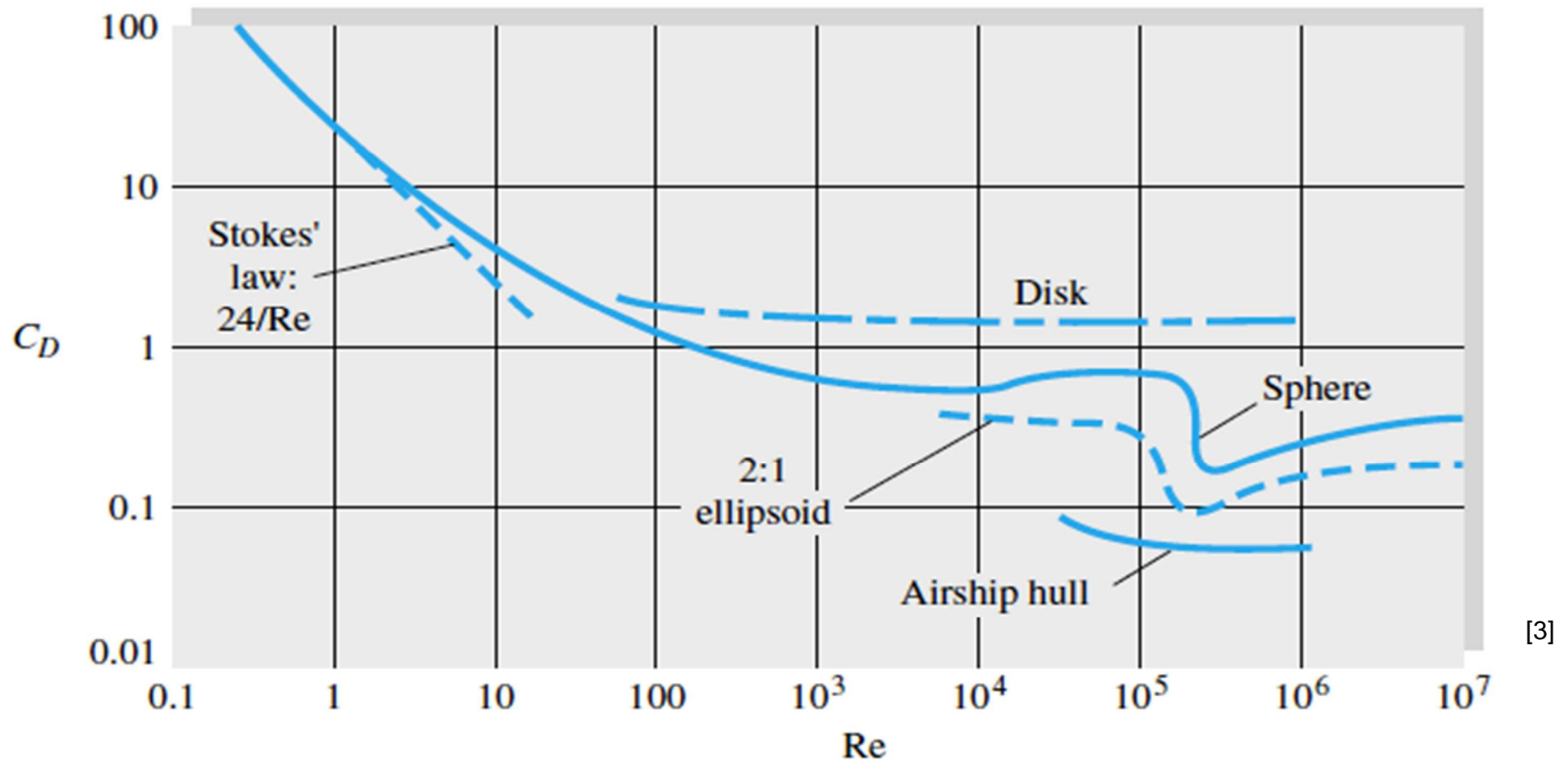
[3]

Two-dimensional objects

Shape	C_D based on frontal area	Shape	C_D based on frontal area	Shape	C_D based on frontal area
Square cylinder: 	2.1	Half-cylinder: 	1.2	Plate: 	2.0
	1.6		1.7	Thin plate normal to a wall: 	1.4
Half tube: 	1.2	Equilateral triangle: 	1.6	Hexagon: 	1.0
	2.3		2.0		0.7


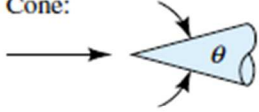
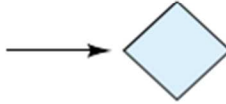
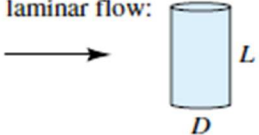
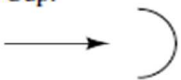
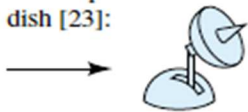
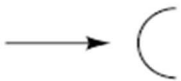
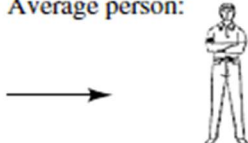
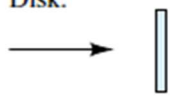
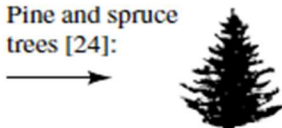
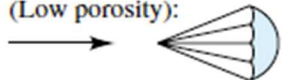
[3]

Three-dimensional objects

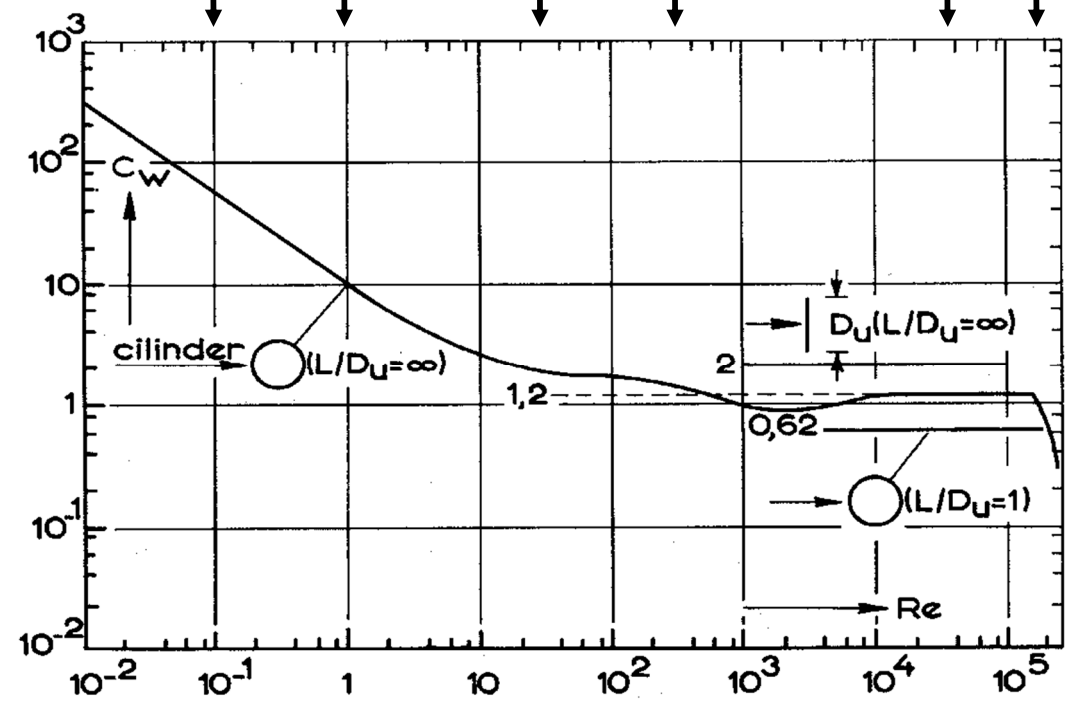
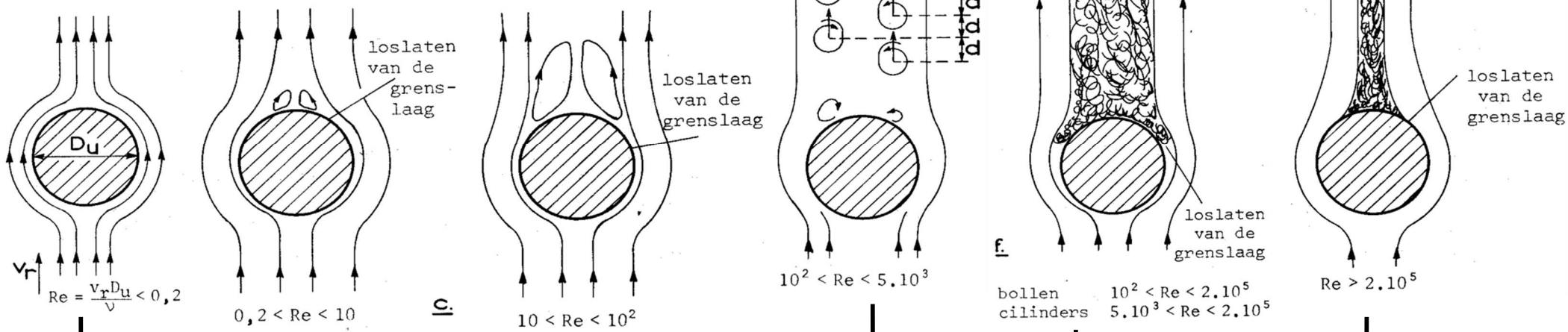


Three-dimensional objects

Table 7.3 Drag of Three-Dimensional Bodies at $Re \geq 10^4$

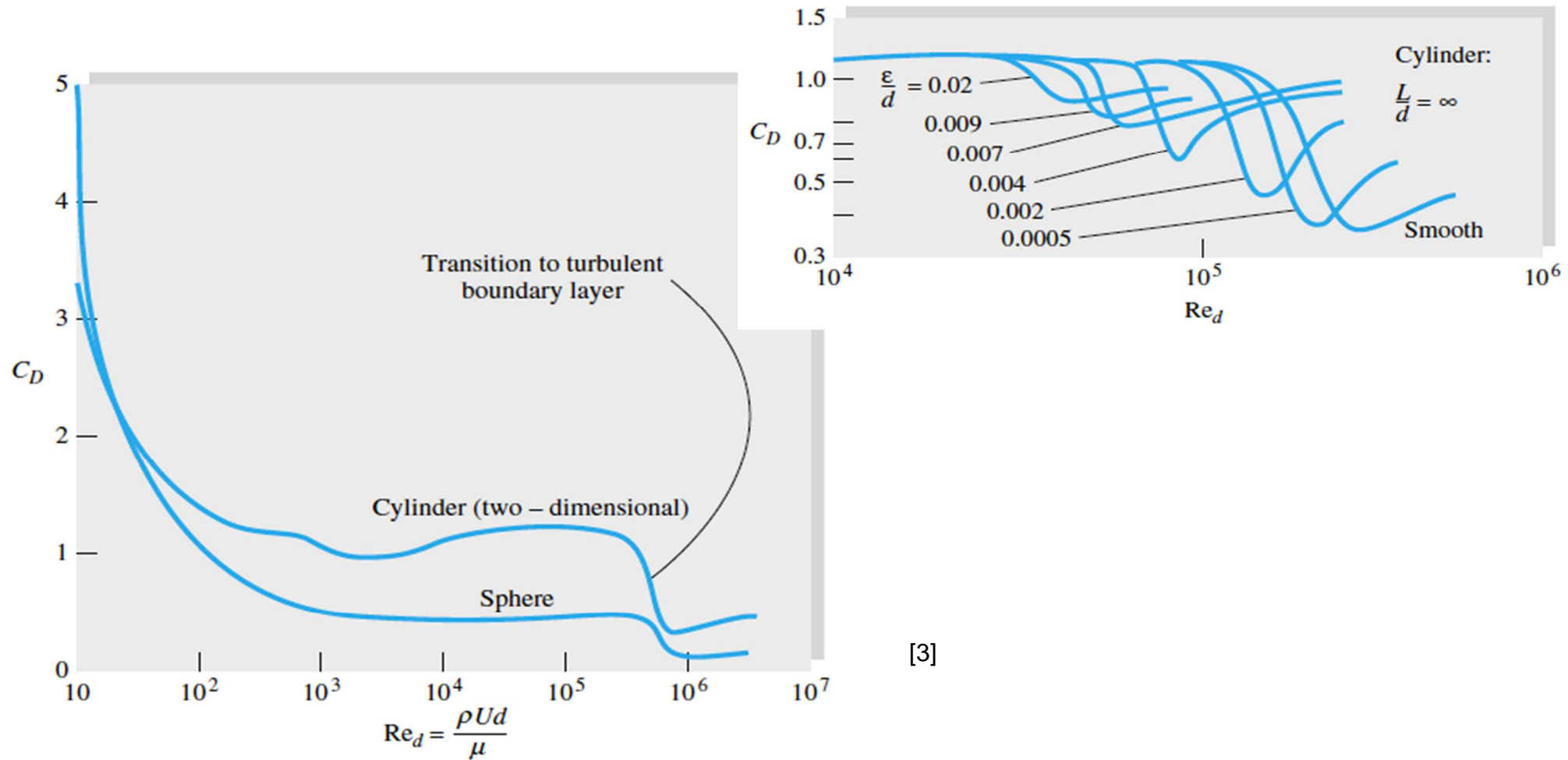
Body	C_D based on frontal area	Body	C_D based on frontal area																					
Cube: 	1.07	Cone: 	<table border="1"> <tr> <td>θ:</td> <td>10°</td> <td>20°</td> <td>30°</td> <td>40°</td> <td>60°</td> <td>75°</td> <td>90°</td> </tr> <tr> <td>C_D:</td> <td>0.30</td> <td>0.40</td> <td>0.55</td> <td>0.65</td> <td>0.80</td> <td>1.05</td> <td>1.15</td> </tr> </table>	θ :	10°	20°	30°	40°	60°	75°	90°	C_D :	0.30	0.40	0.55	0.65	0.80	1.05	1.15					
θ :	10°	20°	30°	40°	60°	75°	90°																	
C_D :	0.30	0.40	0.55	0.65	0.80	1.05	1.15																	
	0.81	Short cylinder, laminar flow: 	<table border="1"> <tr> <td>L/D:</td> <td>1</td> <td>2</td> <td>3</td> <td>5</td> <td>10</td> <td>20</td> <td>40</td> <td>∞</td> </tr> <tr> <td>C_D:</td> <td>0.64</td> <td>0.68</td> <td>0.72</td> <td>0.74</td> <td>0.82</td> <td>0.91</td> <td>0.98</td> <td>1.20</td> </tr> </table>	L/D :	1	2	3	5	10	20	40	∞	C_D :	0.64	0.68	0.72	0.74	0.82	0.91	0.98	1.20			
L/D :	1	2	3	5	10	20	40	∞																
C_D :	0.64	0.68	0.72	0.74	0.82	0.91	0.98	1.20																
Cup: 	1.4	Porous parabolic dish [23]: 	<table border="1"> <tr> <td>Porosity:</td> <td>0</td> <td>0.1</td> <td>0.2</td> <td>0.3</td> <td>0.4</td> <td>0.5</td> </tr> <tr> <td>$\leftarrow C_D$:</td> <td>1.42</td> <td>1.33</td> <td>1.20</td> <td>1.05</td> <td>0.95</td> <td>0.82</td> </tr> <tr> <td>$\rightarrow C_D$:</td> <td>0.95</td> <td>0.92</td> <td>0.90</td> <td>0.86</td> <td>0.83</td> <td>0.80</td> </tr> </table>	Porosity:	0	0.1	0.2	0.3	0.4	0.5	$\leftarrow C_D$:	1.42	1.33	1.20	1.05	0.95	0.82	$\rightarrow C_D$:	0.95	0.92	0.90	0.86	0.83	0.80
Porosity:	0	0.1	0.2	0.3	0.4	0.5																		
$\leftarrow C_D$:	1.42	1.33	1.20	1.05	0.95	0.82																		
$\rightarrow C_D$:	0.95	0.92	0.90	0.86	0.83	0.80																		
	0.4	Average person: 	$\rightarrow C_D A = 9 \text{ ft}^2$ $\uparrow C_D A = 1.2 \text{ ft}^2$																					
Disk: 	1.17	Pine and spruce trees [24]: 	<table border="1"> <tr> <td>U, m/s:</td> <td>10</td> <td>20</td> <td>30</td> <td>40</td> </tr> <tr> <td>C_D:</td> <td>1.2 ± 0.2</td> <td>1.0 ± 0.2</td> <td>0.7 ± 0.2</td> <td>0.5 ± 0.2</td> </tr> </table>	U , m/s:	10	20	30	40	C_D :	1.2 ± 0.2	1.0 ± 0.2	0.7 ± 0.2	0.5 ± 0.2											
U , m/s:	10	20	30	40																				
C_D :	1.2 ± 0.2	1.0 ± 0.2	0.7 ± 0.2	0.5 ± 0.2																				
Parachute (Low porosity): 	1.2																							

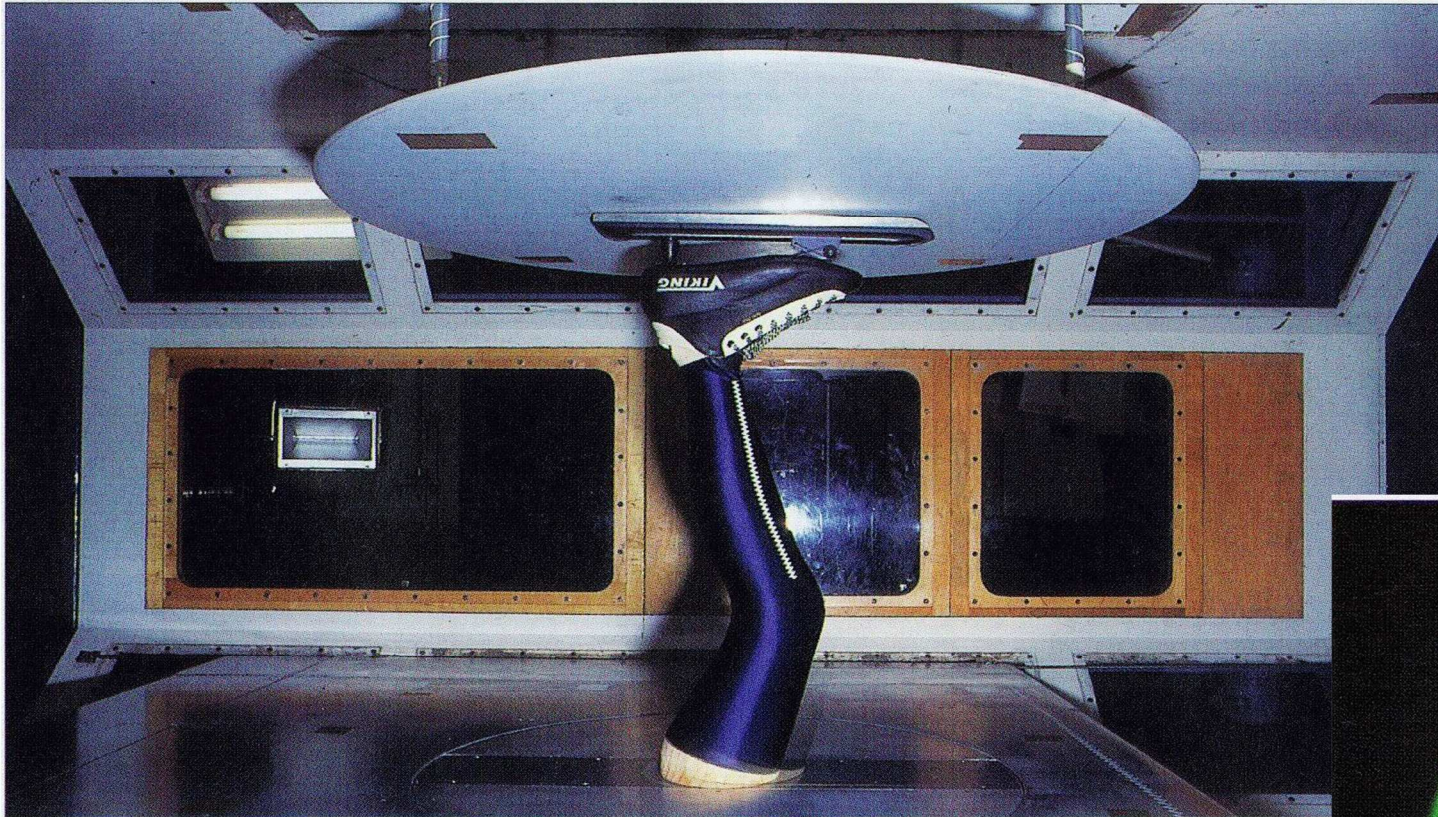
[3]



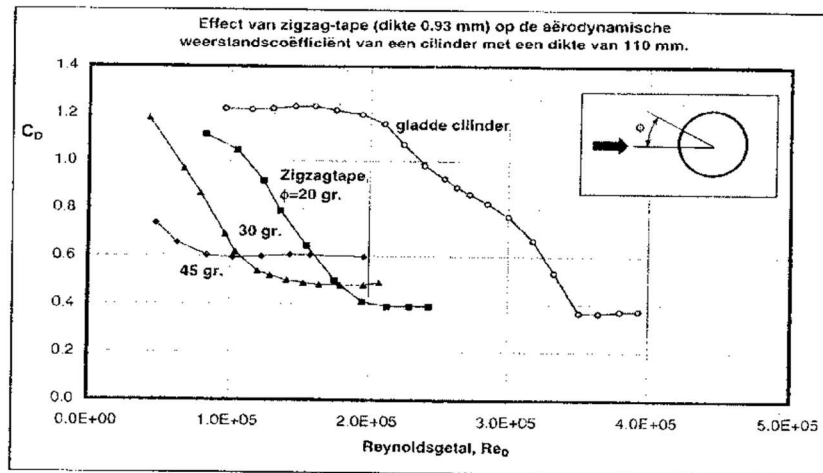
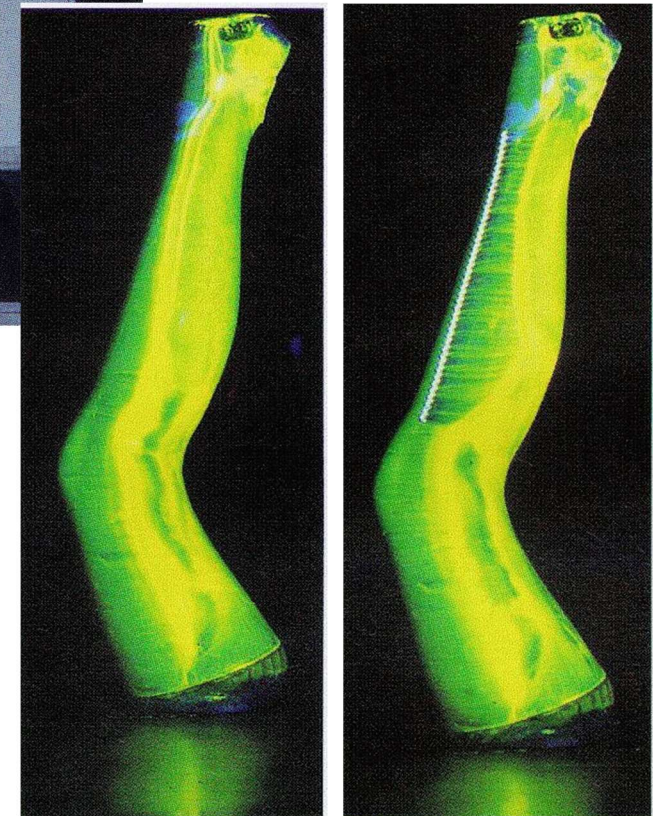
[3]

Drag reduction

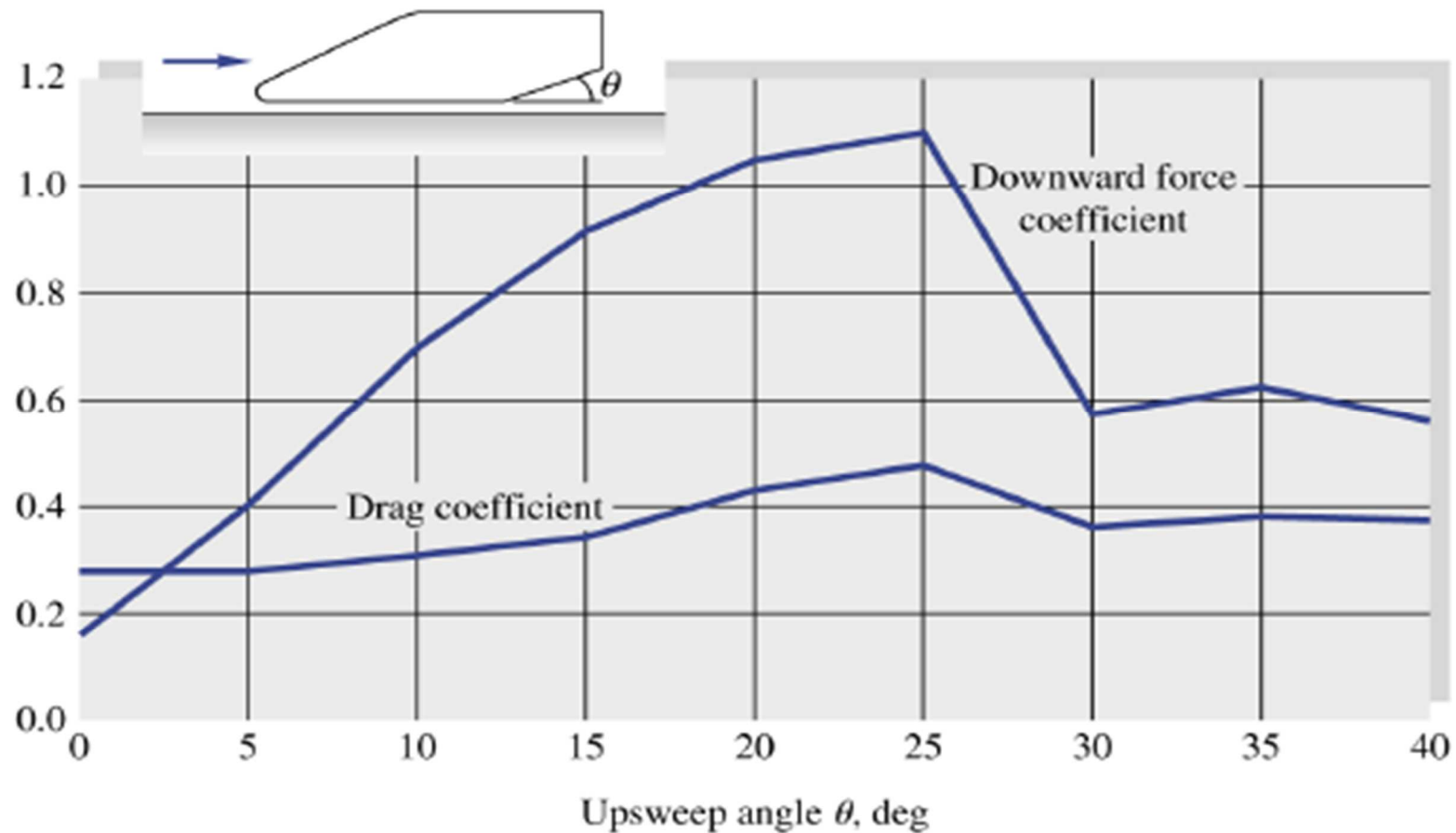




[4]

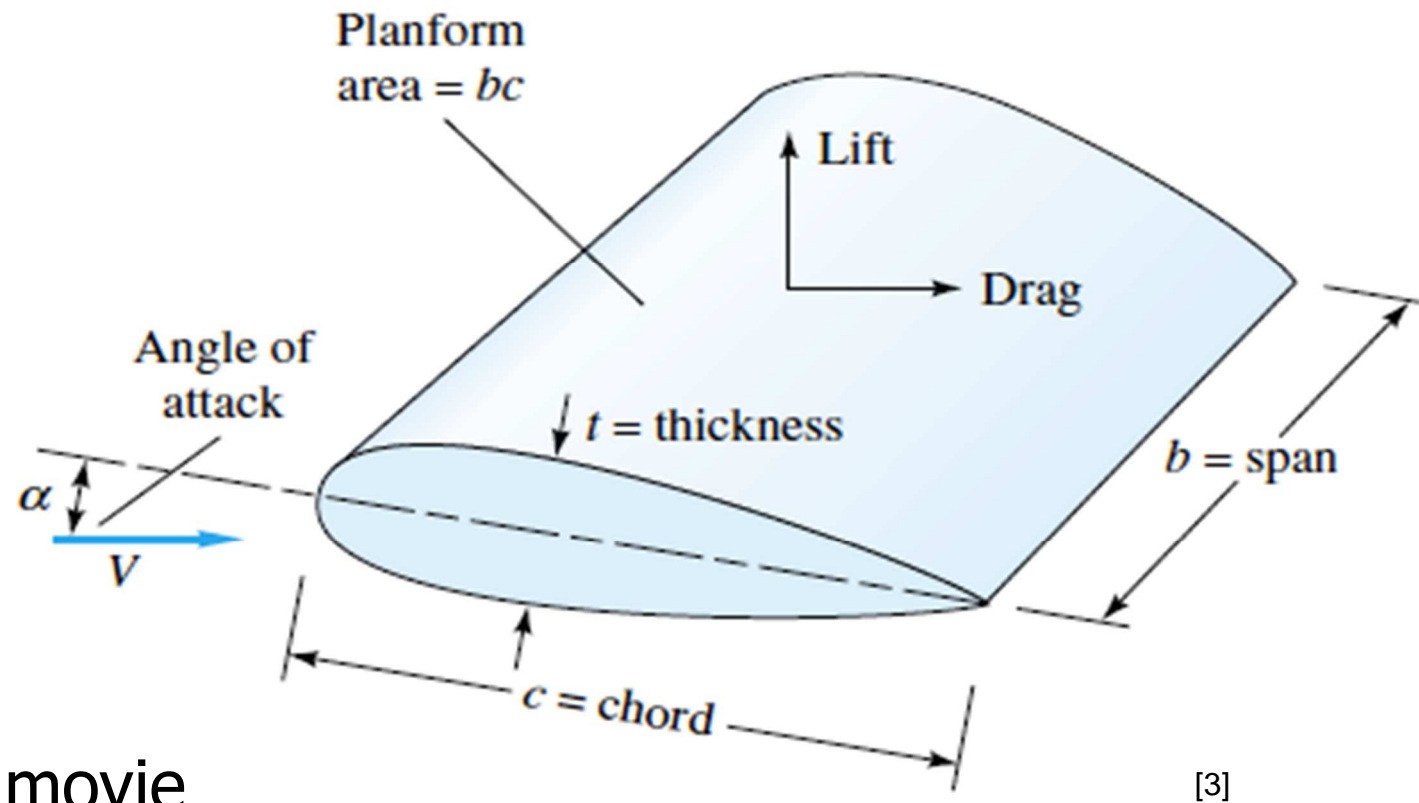


Race car aerodynamics



[3]

Airfoils



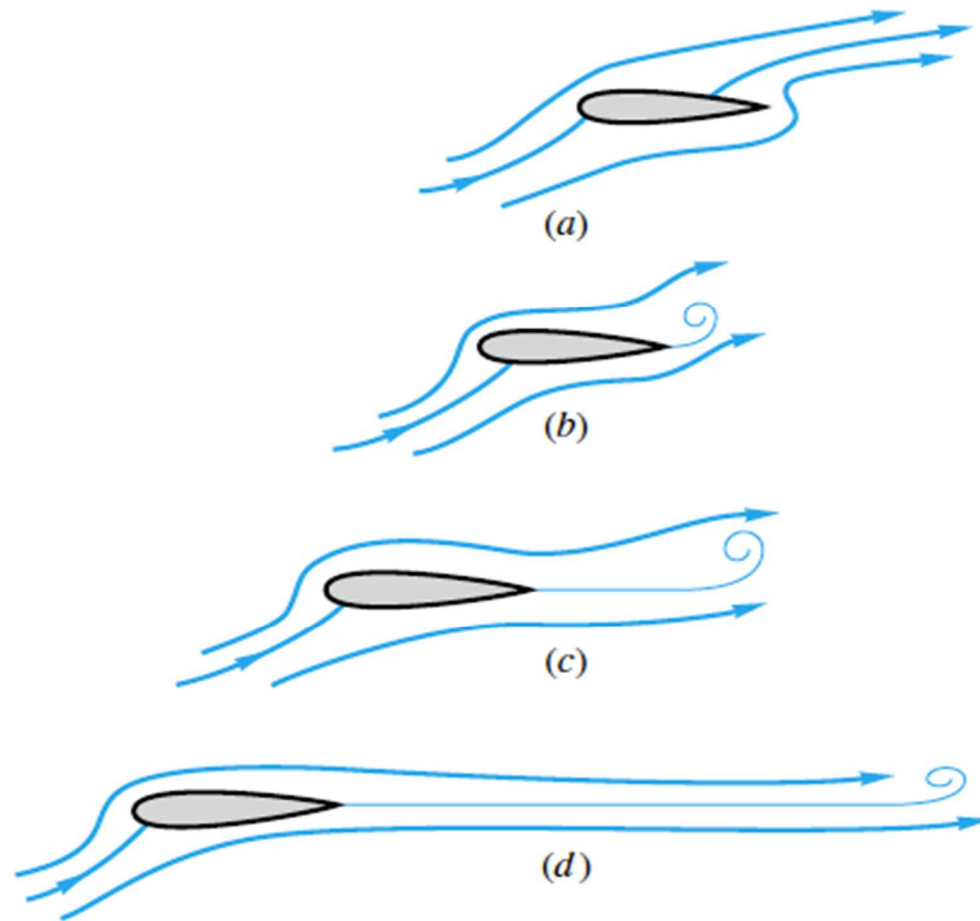
$$C_L = \frac{L}{\frac{1}{2} \rho V^2 A_p}$$

$$C_D = \frac{D}{\frac{1}{2} \rho V^2 A_p}$$

movie

[3]

Development of lift



[3]

movie

Lift vs. drag

lift force: $L = \pi \rho c V^2 \sin \theta_0 = 2\pi \sin \theta_0 \cdot c \cdot \frac{1}{2} \rho V^2$ (Joukowski condition)

lift coefficient: $C_L = 2\pi \sin \theta_0$

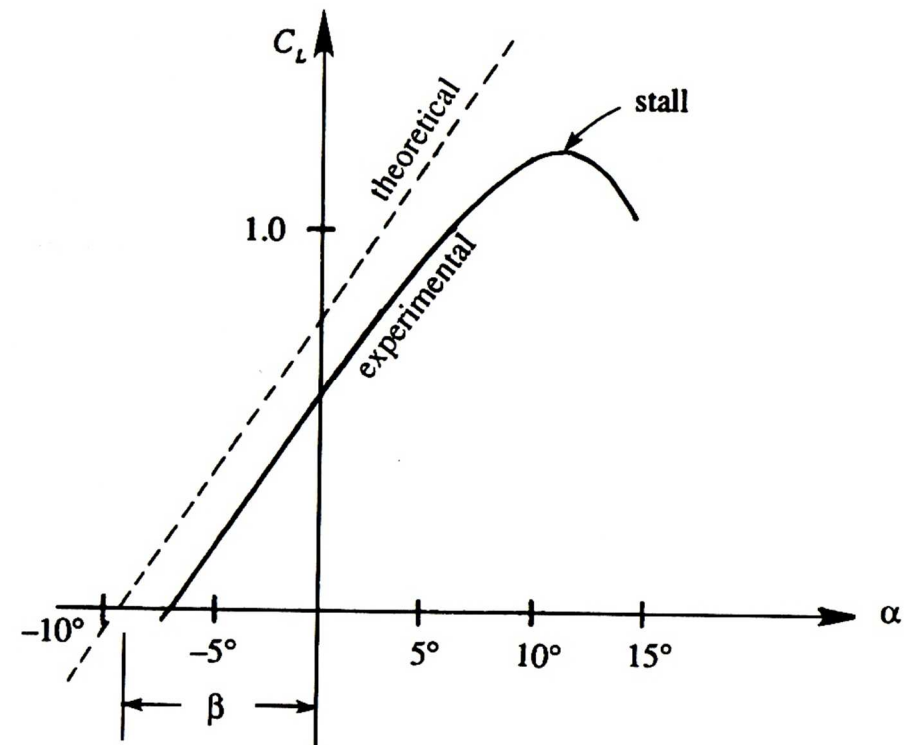
practice: drag: $C_D = f(\alpha)$

slender sections

$$C_L = 2\pi \sin \alpha \rightarrow dC_L / d\alpha = 2\pi \cos \alpha$$

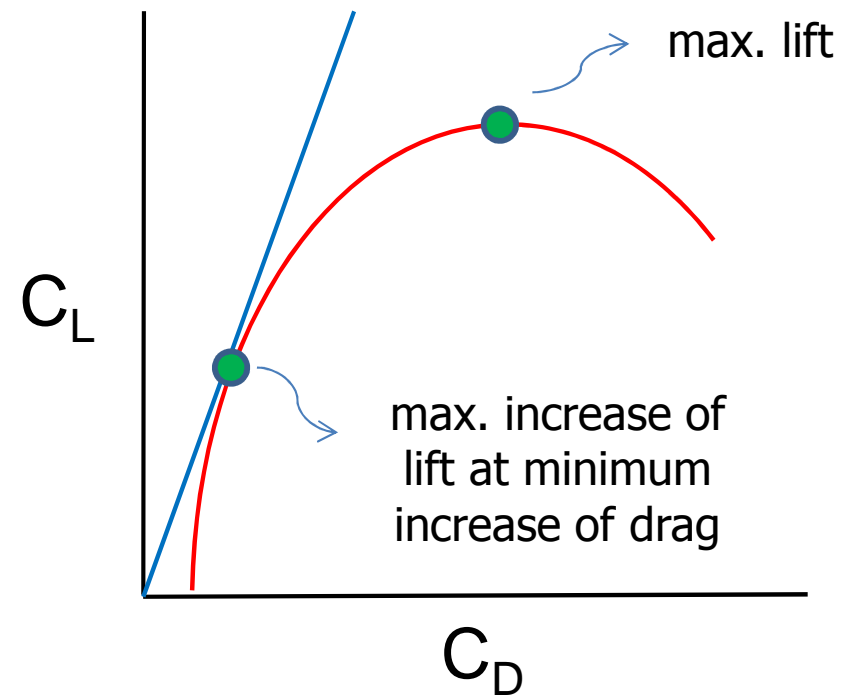
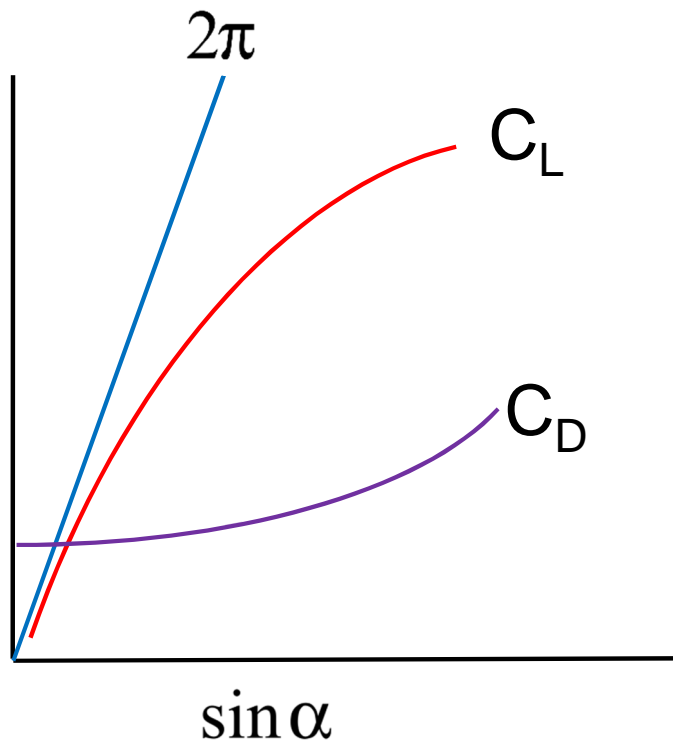
$$C_D = C_{D,0} + B\alpha^2 \rightarrow dC_D / d\alpha = 2B\alpha$$

symmetric airfoil



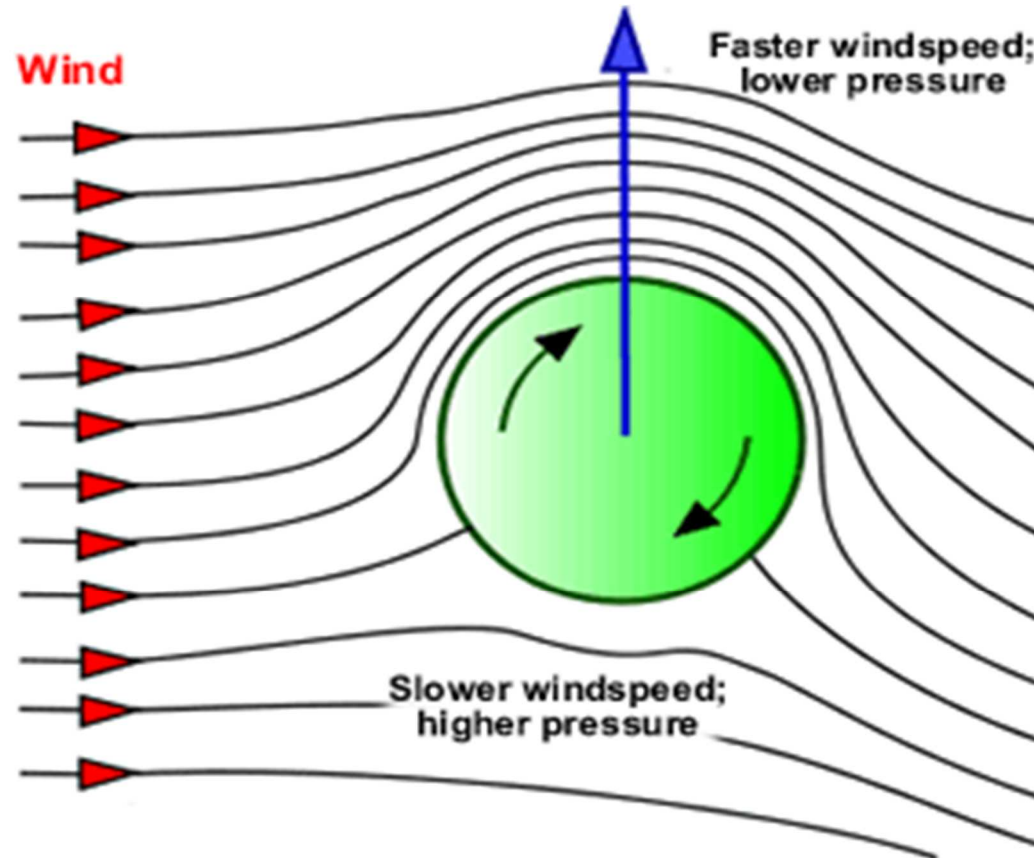
high angle of attack: boundary layer separation & stall

Airfoil performance



$$C_L = 2\pi \sin \alpha \rightarrow dC_L/d\alpha = 2\pi \cos \alpha$$
$$C_D = C_{D,0} + B\alpha^2 \rightarrow dC_D/d\alpha = 2B\alpha$$

Magnus effect



[5]

[Movie: Flow around cylinder](#) [6]

[Movie: Magnus effect](#) [7]

Source

1. Tacoma Narrows Bridge Collapse "Gallop'n' Gertie", <http://youtu.be/j-zczJXSxnw>,
2. New fast iceskating suit, photo courtesy of ANP
3. Frank M. White, *Fluid Mechanics*, McGraw-Hill Series in Mechanical Engineering
4. Testing an iceskating suit for less friction, photo courtesy of TU Delft, faculty of Aerospace Engineering
5. The Magnus effect, royalty free picture
6. Flow around cylinder, <http://www.youtube.com/watch?v=j6yB90vno1E>
7. Magnus effect, <http://www.youtube.com/watch?v=MUf5RwKXNQ0>