

Fig I

↑ see above Figure

$d = \underline{\text{colatitude angle}}$, which is $90^\circ - \text{latitude angle}$.
 The rotation of the earth is given by Ω .

1.167 an object is thrown vertically upward with a speed v_0 . Prove that when it returns it will be at a distance westward from its starting point equal to $(4\Omega v_0^3 \sin \lambda) / 3g^2$.

Note: For deriving this expression the terms relating to Ω^2 are neglected ($\Omega^2 \approx 0$).

In the non-inertial frame of reference x-y-z Newton's 2nd law is formulated as

$$m \cdot \bar{a}_{REL} = \bar{F} + \bar{F}_{fict} \quad (1)$$

with the fictitious force given by

$$\bar{F}_{fict} = -m \left(\bar{a}_{xyz} + \dot{\bar{\omega}}_{xyz} \times \bar{r}_{REL} + \bar{\omega}_{xyz} \times (\bar{\omega}_{xyz} \times \bar{r}_{REL}) + 2 \bar{\omega}_{xyz} \times \bar{v}_{REL} \right) \quad (2)$$

In this expression,

$$\bar{a}_{xyz} = \bar{\omega} \times (\bar{\omega} \times \bar{r}_{xyz}) \quad (3)$$

with \bar{r}_{xyz} the distance from the centre of the earth to the origin of the rotating x-y-z frame of reference.

Further, $\bar{\omega}_{xyz}$ is related to the earth's rotation as

$$\bar{\omega}_{xyz} = \Omega (\sin \delta \bar{j} + \cos \delta \bar{k}) \quad (4)$$

$$\dot{\bar{\omega}}_{xyz} = \bar{0}, \text{ (since } \Omega \text{ is constant).} \quad (5)$$

$$\left. \begin{aligned} \bar{r}_{REL} &= x \bar{i} + y \bar{j} + z \bar{k} \\ \bar{v}_{REL} &= \dot{x} \bar{i} + \dot{y} \bar{j} + \dot{z} \bar{k} \\ \bar{a}_{REL} &= \ddot{x} \bar{i} + \ddot{y} \bar{j} + \ddot{z} \bar{k} \end{aligned} \right\} (6)$$

Substituting (4) into (3) gives

$$\begin{aligned} \bar{a}_{xyz} &= \Omega (\sin \delta \bar{j} + \cos \delta \bar{k}) \times \\ &\quad \left[\Omega (\sin \delta \bar{j} + \cos \delta \bar{k}) \times (x \bar{i} + y \bar{j} + z \bar{k}) \right] \\ &= \Omega^2 (\sin \delta \bar{j} + \cos \delta \bar{k}) \times \left[(\sin \delta \bar{j} + \cos \delta \bar{k}) \times (x \bar{i} + y \bar{j} + z \bar{k}) \right] \end{aligned}$$

Since this term is proportional to Ω^2 , it is ignored as stated by $\Omega^2 \approx 0$;

$$\bar{a}_{xyz} \approx \bar{0}. \quad (7)$$

Using the same argument, the term (3)

$\bar{\omega}_{xyz} \times (\bar{\omega}_{xyz} \times \bar{r}_{REL})$, which also is proportional to Ω^2 , is ignored.

Hence, Eq. (2) is reduced to an expression that only contains the Coriolis ACCELERATION:

$$\bar{F}_{fict} = -m \cdot 2 \bar{\omega}_{xyz} \times V_{REL}$$

$$= -2m\Omega (\sin\delta \bar{j} + \cos\delta \bar{k}) \times (\dot{x}\bar{i} + \dot{y}\bar{j} + \dot{z}\bar{k})$$

$$= -2m\Omega (-\dot{x} \sin\delta \bar{k} + \dot{z} \sin\delta \bar{i} + \dot{x} \cos\delta \bar{j} - \dot{y} \cos\delta \bar{i}) \quad (8)$$

Inserting (8), (6)₃ into (1), and using the fact that the external loading \bar{F} is defined as

$$\bar{F} = -m \cdot g \bar{k} \quad (9)$$

gives

$$m(\ddot{x}\bar{i} + \ddot{y}\bar{j} + \ddot{z}\bar{k}) = -mg\bar{k} - 2m\Omega \left[(\dot{z} \sin\delta - \dot{y} \cos\delta) \bar{i} + \dot{x} \cos\delta \bar{j} - \dot{x} \sin\delta \bar{k} \right] \quad (10)$$

Factorizing m out, and separating the equations of motion for the x , y and z -direction gives:

$$\ddot{x} + 2\mathcal{N} \sin \lambda \dot{z} - 2\mathcal{N} \cos \lambda \dot{y} = 0; \quad (11)$$

$$\ddot{y} + 2\mathcal{N} \cos \lambda \dot{x} = 0; \quad (12)$$

$$\ddot{z} = 2\mathcal{N} \sin \lambda \dot{x} - g; \quad (13)$$

Integrating the above expressions w.r.t. time gives, respectively:

$$\dot{x} + 2\mathcal{N} \sin \lambda z - 2\mathcal{N} \cos \lambda y = C_1 \quad (14)$$

$$\dot{y} + 2\mathcal{N} \cos \lambda x = C_2 \quad (15)$$

$$\dot{z} = 2\mathcal{N} \sin \lambda x - gt + C_3 \quad (16)$$

The integration constants C_1 , C_2 and C_3 follow from the initial conditions:

$$x(0) = y(0) = z(0) = 0; \quad \dot{x}(0) = 0; \quad \dot{y}(0) = 0; \quad \dot{z}(0) = v_0$$

After substituting these initial conditions into (14), (15) and (16), we obtain $C_1 = 0$; $C_2 = 0$;

$$C_3 = v_0, \text{ so}$$

$$\dot{x} + 2\mathcal{N} \sin \lambda z - 2\mathcal{N} \cos \lambda y = 0 \quad (17)$$

$$\dot{y} + 2\mathcal{N} \cos \lambda x = 0 \quad (18)$$

$$\dot{z} = 2\mathcal{N} \sin \lambda x - gt + v_0 \quad (19)$$

Inserting (17)-(19) into (11)-(13), where (5) the terms relating to v^2 are ignored gives the simplified equations of motion:

$$\ddot{x} + 2v \sin \lambda (-gt + v_0) = 0 \quad (20)$$

$$\ddot{y} = 0 \quad (21)$$

$$\ddot{z} = -g \quad (22)$$

Integrating the above expression twice w.r.t. time, again using the initial conditions

$$x(0) = y(0) = z(0) = 0 ;$$

$$\dot{x}(0) = 0 ; \dot{y}(0) = 0 ; \dot{z}(0) = v_0 ; \text{ leads to}$$

$$x(t) = \frac{1}{3} v \sin \lambda g t^3 - v \sin \lambda v_0 t^2 \quad (23)$$

$$y(t) = 0 \quad (24)$$

$$z(t) = v_0 t - \frac{1}{2} g t^2 \quad (25)$$

The time it takes for the object to come back to the earth ($z=0$) after being thrown up can be computed from Eq. (25):

$$0 = v_0 t - \frac{1}{2} g t^2$$

$$\rightarrow t(v_0 - \frac{1}{2} g t) = 0$$

$$\rightarrow t=0 \quad \vee \quad t = \frac{2v_0}{g}$$

Substituting $t = \frac{2V_0}{g}$ into (23) gives (6)

$$\begin{aligned} x\left(\frac{2V_0}{g}\right) &= \frac{1}{3} v \sin \alpha g \left(\frac{2V_0}{g}\right)^3 - v \sin \alpha V_0 \left(\frac{2V_0}{g}\right)^2 \\ &= -\frac{4}{3} v \sin \alpha \frac{V_0^3}{g^2} \end{aligned} \quad (26)$$

which means that it has indeed moved over a distance

$$\frac{4}{3} v \sin \alpha \frac{V_0^3}{g^2}$$

in the westward direction (in the negative x-direction, see Figure I)

1.16g

The solution to this problem essentially uses expressions derived for question 1.167.

The projectile now is not thrown vertically but under an angle α with x-axis in the west direction. So, the initial conditions are now:

$$x(0) = y(0) = z(0) = 0 \quad (27)$$

$$\dot{x}(0) = -V_0 \cos \alpha; \quad \dot{y}(0) = 0; \quad \dot{z}(0) = V_0 \sin \alpha$$

Substituting the boundary conditions (27) into (14) - (16) gives

$$-V_0 \cos \alpha = C_1$$

$$0 = C_2$$

$$V_0 \sin \alpha = C_3$$

This turns the expressions (14) - (16) into

$$\ddot{x} + 2\lambda \sin \lambda z - 2\lambda \cos \lambda y = -V_0 \cos \alpha \quad (28)$$

$$\ddot{y} + 2\lambda \cos \lambda x = 0 \quad (29)$$

$$\ddot{z} = 2\lambda \sin \lambda x - g + V_0 \sin \alpha \quad (30)$$

Inserting (28) - (30) into (11) - (13) and ignoring the terms related to λ^2 provides the simplified Eqs. of motion

$$\ddot{x} + 2\lambda \sin \lambda (-gt + V_0 \sin \alpha) = 0; \quad (31)$$

$$\ddot{y} + 2\lambda \cos \lambda (-V_0 \cos \alpha) = 0; \quad (32)$$

$$\ddot{z} = 2\lambda \sin \lambda (-V_0 \cos \alpha) - g \quad (33)$$

Integrating the above expressions once w.r.t. time gives

(P)

$$\dot{x} = \nu \sin \delta g t^2 - 2\nu \sin \delta V_0 \sin \alpha t + C_1 \quad (34)$$

$$\dot{y} = 2\nu \cos \delta V_0 \cos \alpha t + C_2 \quad (35)$$

$$\dot{z} = -2\nu \sin \delta \cos \alpha V_0 t - g t + C_3 \quad (36)$$

The integration constants C_1 , C_2 and C_3 follow from the initial conditions (27) as

$$C_1 = -V_0 \cos \alpha$$

$$C_2 = 0$$

$$C_3 = V_0 \sin \alpha$$

(37)

Integrating (34) - (36) once again w.r.t. time, and using (37) leads to

$$x = \frac{1}{3} \nu \sin \delta g t^3 - \nu \sin \delta V_0 \sin \alpha t^2 - V_0 \cos \alpha t$$

$$y = \nu \cos \delta V_0 \cos \alpha t^2 \quad (38)$$

$$z = -\nu \sin \delta \cos \alpha V_0 t^2 - \frac{1}{2} g t^2 + V_0 \sin \alpha t$$

where the integration constants are zero as a result of the initial conditions, Eq (27)

The projectile reaches the maximum height when $\dot{z}(t) = 0$.

From (36)₃ and (37)₃, this gives (9)

$$0 = -2v \sin \delta \cos \alpha v_0 t - gt + v_0 \sin \alpha$$

$$\Rightarrow t = \frac{v_0 \sin \alpha}{2 v_0 v \sin \delta \cos \alpha + g} \quad (39)$$

which can be further developed as

$$t = \frac{v_0 \sin \alpha}{2 v_0 v \sin \delta \cos \alpha + g} * \frac{-2 v_0 v \sin \delta \cos \alpha + g}{-2 v_0 v \sin \delta \cos \alpha + g}$$

$$\rightarrow t = \frac{v_0 \sin \alpha (g - 2 v_0 v \sin \delta \cos \alpha)}{g^2 - 4 v_0^2 v^2 \sin^2 \delta \cos^2 \alpha}$$

≈ 0 since $v^2 \ll 0$

$$\rightarrow t \approx \frac{v_0 \sin \alpha (g - 2 v_0 v \sin \delta \cos \alpha)}{g^2} \quad (40)$$

When $v = 0$, (40) turns into

$$t \approx \frac{v_0 \sin \alpha}{g}$$

(Simplification, assuming the earth does not rotate).

1.170 The maximum height can be computed (11) by substituting (40) into (30)₃:

$$z_{\max} = \left(-\frac{1}{2}g - \nu \sin \delta \cos \alpha v_0 \right) + \left[\frac{v_0 \sin \alpha (g - 2\nu \sin \delta \cos \alpha)}{g^2} \right. \\ \left. + v_0 \sin \alpha \left[\frac{v_0 \sin \alpha (g - 2\nu \sin \delta \cos \alpha)}{g^2} \right] \right]$$

Ignoring the terms related to ν^2 , this expression can be developed as

$$z_{\max} = \frac{-\frac{1}{2}g v_0^2 \sin^2 \alpha}{g^4} \\ - \nu \sin \delta \cos \alpha v_0 \cdot \frac{v_0^2 \sin^2 \alpha g^2}{g^4} \\ - \frac{4\nu \sin \delta \cos \alpha g v_0^2 \sin^2 \alpha}{g^4} * \left(-\frac{1}{2}g \right) \\ + \frac{v_0^2 \sin^2 \alpha g}{g^2} - \frac{2 v_0^3 \nu \sin^2 \alpha \sin \delta \cos \alpha}{g^2}$$

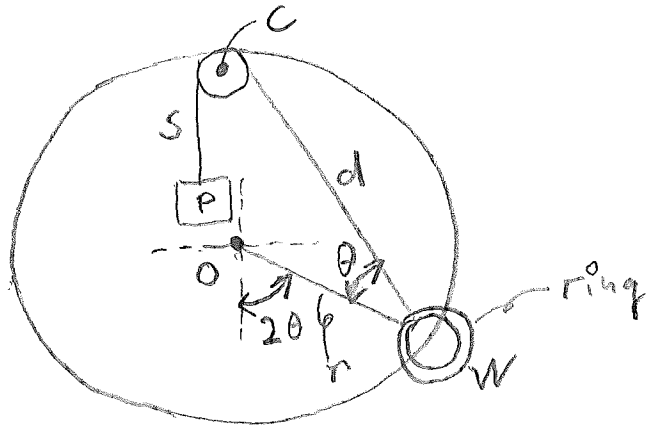
which finally leads to:

$$z_{\max} = \frac{v_0^2 \sin^2 \alpha}{2g} - \frac{v_0^3 \nu \sin^2 \alpha \sin \delta \cos \alpha}{g^2}$$

NOTE: The factor of 2 appearing in front of the second term on page 73 of Tóvák is wrong!

1.207

①



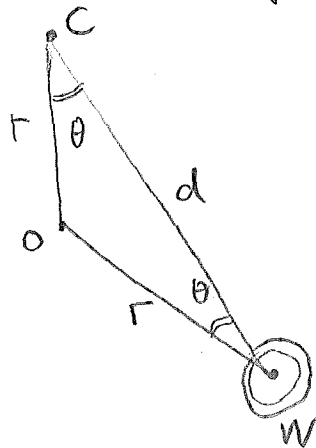
Let s be the length of the string attached to the block and let d be the length of the string between the pulley and the ring.

$$s + d = l (= \text{constant}) \quad (1) \quad \text{with } l \text{ the total length of the string.}$$

When writing the angle 2θ as $\phi = 2\theta$, and giving the ring a virtual displacement, the virtual work can be written as

$$\delta W = P \cdot \delta s - W \cdot r \sin \phi \delta \phi \quad (2)$$

The distance d follows, with the triangle below



as $d = 2r \cos \theta$, from which it follows that

$$\delta d = -2r \sin \theta \delta \theta \quad (3)$$

(2)

Further, from (1) it follows that

$$\delta s + \delta d = 0, \text{ so that } \delta s = -\delta d \quad (4)$$

In addition, since $\phi = 2\theta$, we have

$$\delta \phi = 2\delta \theta \quad (5)$$

Substituting (3)-(5) into (2) gives

$$\delta W = P \cdot 2r \sin \theta \delta \theta - 2Wr \sin 2\theta \delta \theta \quad (6)$$

For equilibrium, it is required that $\delta W = 0$,

so, from (6) it follows that

$$(P \cdot 2r \sin \theta - 2Wr \sin 2\theta) \delta \theta = 0 \quad (7)$$

which, for an arbitrary $\delta \theta$, leads to

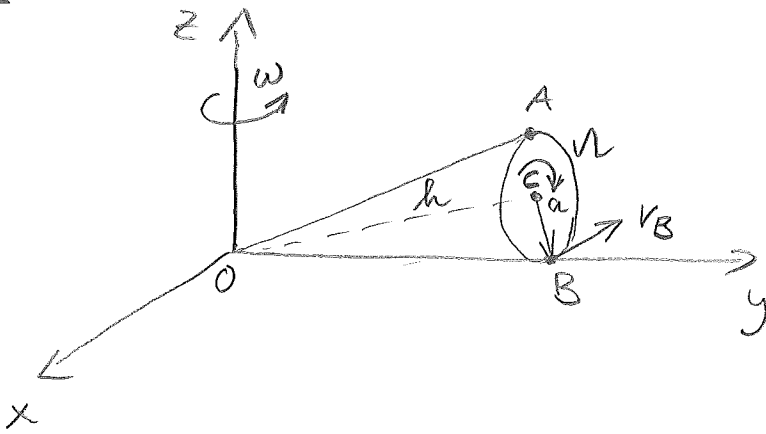
$$P \cdot 2r \sin \theta - 2Wr \sin 2\theta = 0$$

$$\rightarrow P \sin \theta - W \cdot 2 \sin \theta \cos \theta = 0$$

$$\rightarrow \boxed{P = 2W \cos \theta}$$

4.4.0

①



The contact point B of the line of contact OB has a velocity equal to

$$\begin{aligned}\vec{v}_B &= \vec{\omega} \times \vec{OB} \\ &= \omega \vec{k} \times \sqrt{h^2 + a^2} \cdot \vec{j} \\ &= -\omega \sqrt{h^2 + a^2} \cdot \vec{i} \quad \text{①}\end{aligned}$$

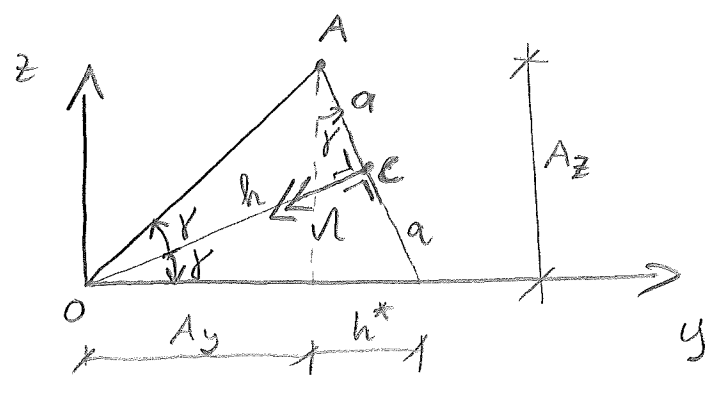
This velocity may be alternatively written in terms of the angular velocity ν of the cone as

$$\vec{v}_B = -\nu a \vec{i} \quad \text{②}$$

Equating ① and ② gives

$$\boxed{\nu = \frac{\omega \sqrt{h^2 + a^2}}{a}} \quad \text{③} \quad \left(= \text{holonomic constraint!} \right)$$

When denoting the centre point of the base of the cone as C (see Figure above), the total rotation of a point on the cone is determined by the rotation ω about the z-axis, and the rotation ν about the OC-axis.



In accordance with the above figure, the rotation $\bar{\nu}$ about the OC axis can be written as :

$$\begin{aligned} \bar{\nu} &= \nu_y \bar{j} + \nu_z \bar{k} \\ &= -\nu \cos \gamma \bar{j} - \nu \sin \gamma \bar{k} \\ &= -\nu \frac{h}{\sqrt{h^2+a^2}} \bar{j} - \nu \frac{a}{\sqrt{h^2+a^2}} \bar{k} \end{aligned}$$

The total rotation $\bar{\omega}$ then follows as

$$\begin{aligned} \bar{\omega} &= \bar{\nu} + \omega \bar{k} \\ &= -\nu \frac{h}{\sqrt{h^2+a^2}} \bar{j} + \left(\omega - \frac{\nu a}{\sqrt{h^2+a^2}} \right) \bar{k} \end{aligned} \tag{4}$$

The velocity of the highest point on the cone, point A, can now be computed as :

$$\vec{V}_A = \vec{\omega} \times \vec{OA} \tag{5}$$

where \vec{OA} follows from

$$\begin{aligned} \vec{OA} &= A_y \bar{j} + A_z \bar{k} \\ &= \sqrt{h^2+a^2} \cdot \cos \gamma \bar{j} + \sqrt{h^2+a^2} \cdot \sin \gamma \bar{k} \end{aligned}$$

HENCE \vec{OA} can be further elaborated as (3)

$$\vec{OA} = \sqrt{h^2 + a^2} \cdot (\cos^2 \gamma - \sin^2 \gamma) \vec{j} \\ + \sqrt{h^2 + a^2} \cdot 2 \sin \gamma \cdot \cos \gamma \vec{k}$$

$$\rightarrow \vec{OA} = \sqrt{h^2 + a^2} \left(\left[\left(\frac{h}{\sqrt{h^2 + a^2}} \right)^2 - \left(\frac{a}{\sqrt{h^2 + a^2}} \right)^2 \right] \vec{j} \right. \\ \left. + 2 \cdot \frac{h}{\sqrt{h^2 + a^2}} \cdot \frac{a}{\sqrt{h^2 + a^2}} \vec{k} \right)$$

$$\rightarrow \vec{OA} = \frac{h^2 - a^2}{\sqrt{h^2 + a^2}} \vec{j} + \frac{2ha}{\sqrt{h^2 + a^2}} \vec{k} \quad (6)$$

Now, substituting (6) and (4) into (5) gives:

$$\vec{V}_A = \left(-\Omega \frac{h}{\sqrt{h^2 + a^2}} \vec{j} + \left(\omega - \frac{\Omega a}{\sqrt{h^2 + a^2}} \right) \vec{k} \right) \times \\ \left(\frac{h^2 - a^2}{\sqrt{h^2 + a^2}} \vec{j} + \frac{2ha}{\sqrt{h^2 + a^2}} \vec{k} \right)$$

$$\rightarrow \vec{V}_A = -\Omega \frac{h}{\sqrt{h^2 + a^2}} \cdot \frac{2ha}{\sqrt{h^2 + a^2}} \cdot \vec{i} \\ - \left(\omega - \frac{\Omega a}{\sqrt{h^2 + a^2}} \right) \cdot \frac{(h^2 - a^2)}{\sqrt{h^2 + a^2}} \vec{i}$$

$$\rightarrow \vec{V}_A = \left[-\Omega \left\{ \frac{ha^2}{h^2 + a^2} + \frac{a^3}{h^2 + a^2} \right\} - \omega \frac{(h^2 - a^2)}{\sqrt{h^2 + a^2}} \right] \vec{i} \quad (7)$$

(4)

Inserting (3) into (7) gives

$$\vec{V}_A = \left[-\frac{\omega \sqrt{h^2 + a^2}}{a} \left\{ \frac{h^2 a}{h^2 + a^2} + \frac{a^3}{h^2 + a^2} \right\} - \omega \frac{(h^2 - a^2)}{\sqrt{h^2 + a^2}} \right] \vec{i}$$

$$\rightarrow \vec{V}_A = \frac{-2 \cdot h^2 \cdot \omega}{\sqrt{h^2 + a^2}} \vec{i}$$