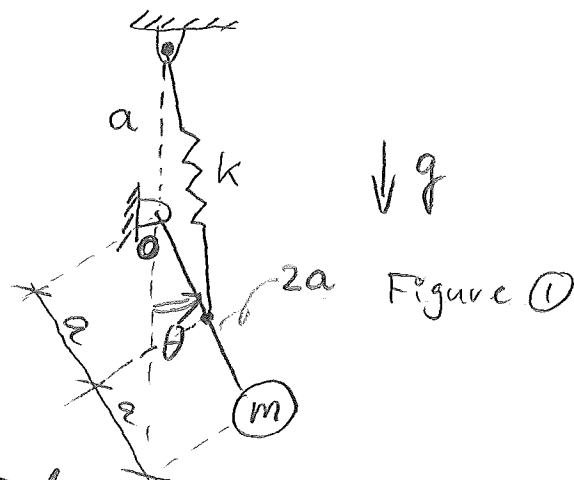


2.17

①

The kinetic energy of the system Figure ① is

$$\begin{aligned} T &= \frac{1}{2} J \dot{\theta}^2 \\ &= \frac{1}{2} \cdot m \cdot (2a)^2 \cdot \dot{\theta}^2 \\ &= 2ma^2 \dot{\theta}^2 \quad \text{①} \end{aligned}$$

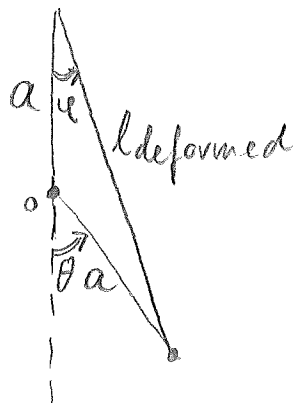


The potential energy of the system is

$$V = -mg \cdot 2a \cos \theta + \frac{1}{2} k \cdot \delta_{\text{spring}}^2 \quad \text{②}$$

$$\delta_{\text{spring}} = l_{\text{deformed}} - l \quad \text{③}$$

with l_{deformed} as given in the figure below



$$l_{\text{deformed}} = 2a \cos \phi \quad \text{④}$$

ϕ can be expressed in terms of θ from the relation:

$$a + a \cos \theta = l_{\text{deformed}} \cos \phi \quad \text{⑤}$$

Substituting (4) into (5) gives

$$a + a \cos \theta = 2a \cos^2 \varphi$$

$$\Rightarrow \cos \varphi = \sqrt{\frac{1}{2} + \frac{1}{2} \cos \theta} \quad (6)$$

Inserting (6) into (4) leads to

$$\begin{aligned} l_{\text{deformed}} &= 2a \sqrt{\frac{1}{2} + \frac{1}{2} \cos \theta} \\ &= a \sqrt{2 + 2 \cos \theta} \quad (7) \end{aligned}$$

With this expression, (3) becomes

$$l_{\text{spring}} = a \sqrt{2 + 2 \cos \theta} - l \quad (8)$$

Inserting (8) into (2) leads to

$$V = -2mg a \cos \theta + \frac{1}{2} k (a \sqrt{2 + 2 \cos \theta} - l)^2 \quad (9)$$

From (1) and (9), the Lagrangian $L = T - V$ becomes

$$L = 2m a^2 \dot{\theta}^2 + 2mg a \cos \theta - \frac{1}{2} k (a \sqrt{2 + 2 \cos \theta} - l)^2 \quad (10)$$

Substituting (10) into the Lagrange equations of motion

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}} \right) - \frac{\partial L}{\partial \theta} = 0$$

leads to

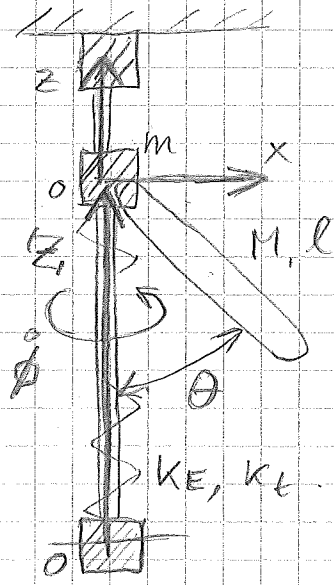
$$4m a^2 \ddot{\theta} + 2mga \sin \theta - k(a \sqrt{2 + 2 \cos \theta} - l) a \frac{\sin \theta}{\sqrt{2 + 2 \cos \theta}} = 0$$

which may be alternatively written as (using goniometry rules);

$$4m a^2 \ddot{\theta} + (2mga - k a^2) \sin \theta + k l a \cdot \sin \frac{1}{2} \theta = 0$$

2.53

(1)



z_1 = the vertical position of the collar.

The x-y-z-moving frame of reference rotates about the vertical axis. The rotation ω of the moving frame of reference is

$$\omega = \dot{\phi} \bar{k}$$

The velocity of the centre of mass of the bar, $v_{c, \text{bar}}$, is expressed as

$$\begin{aligned} \bar{v}_{c, \text{bar}} &= \bar{v}_{xyz} + \bar{\omega} \times \bar{r}_{\text{rel}} + \bar{v}_{\text{rel}} \\ &= \dot{z}_1 \bar{k} + \dot{\phi} \bar{k} \times \left(\frac{l}{2} \sin \theta \bar{i} - \frac{l}{2} \cos \theta \bar{k} \right) \\ &\quad + \dot{\theta} \frac{l}{2} \cos \theta \bar{i} + \dot{\theta} \frac{l}{2} \sin \theta \bar{k} \end{aligned}$$

$$\begin{aligned} \bar{v}_{c, \text{bar}} &= \dot{z}_1 \bar{k} + \dot{\phi} \frac{l}{2} \sin \theta \bar{j} \\ &\quad + \dot{\theta} \frac{l}{2} \cos \theta \bar{i} + \dot{\theta} \frac{l}{2} \sin \theta \bar{k} \end{aligned}$$

$$T = T_m + T_{\text{bar, trans}} + T_{\text{bar, rot}}$$

$$\begin{aligned} T_{\text{bar, rot}} &= \frac{1}{2} J_c (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) \\ &= \frac{1}{2} \frac{1}{12} M l^2 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) = \frac{1}{24} M l^2 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) \end{aligned}$$

$$T_{\text{bar, trans}} = \frac{1}{2} M \cdot \bar{v}_{c, \text{bar}} \cdot \bar{v}_{c, \text{bar}} \quad (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta)$$

$$T_m = \frac{1}{2} \cdot m \cdot \dot{z}_1^2$$

$$T_{C, Bar, trans} = \frac{1}{2} M \left(\dot{\theta}^2 \frac{l^2}{4} \cos^2 \theta + \dot{\phi}^2 \frac{l^2}{4} \sin^2 \theta + \left(\dot{\theta} \frac{l}{2} \sin \theta + \dot{z}_1 \right)^2 \right)$$

$$T = \frac{1}{2} m \dot{z}_1^2 + \frac{1}{2} M \left[\dot{\theta}^2 \frac{l^2}{4} \cos^2 \theta + \dot{\phi}^2 \frac{l^2}{4} \sin^2 \theta + \dot{\theta}^2 \frac{l^2}{4} \sin^2 \theta + 2 \dot{\theta} \frac{l}{2} \sin \theta \dot{z}_1 + \dot{z}_1^2 \right] + \frac{1}{24} M l^2 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta)$$

$$\Rightarrow T = \frac{1}{2} (m+M) \dot{z}_1^2 + \frac{1}{2} M \left[\frac{\dot{\theta}^2 l^2}{3} + \dot{\phi}^2 \frac{l^2}{3} \sin^2 \theta + \dot{\theta} \dot{z}_1 l \sin \theta \right]$$

$$V = \frac{1}{2} k_E \cdot \dot{z}_1^2 + \frac{1}{2} k_t \phi^2 + mg z_1 + Mg \left(z_1 - \frac{l}{2} \cos \theta \right)$$

$$L = T - V \quad (I)$$

Eqs. of motion :

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_k} \right) - \frac{\partial L}{\partial q_k} = 0$$

$$\frac{\partial L}{\partial \dot{z}_1} = (m+M) \dot{z}_1 + \frac{Ml}{2} \dot{\theta} \sin \theta$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{z}_1} \right) = (m+M) \ddot{z}_1 + \frac{Ml}{2} \ddot{\theta} \sin \theta + \frac{Ml}{2} \dot{\theta}^2 \cos \theta \quad (1)$$

$$\frac{\partial L}{\partial z} = -k_E z - (m+M)g \quad (2)$$

Combining (1) & (2) with (I), the first equation of motion becomes:

$$\left((m+M)\ddot{z}_1 + \frac{Ml}{2}(\ddot{\theta} \sin \theta + \dot{\theta}^2 \cos \theta) + k_E z = -(m+M)g \right) \quad (A)$$

Subsequently:

$$\frac{\partial L}{\partial \dot{\theta}} = \frac{Ml^2 \dot{\theta}}{3} + \dot{z}_1 l \sin \theta$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}} \right) = \frac{Ml^2 \ddot{\theta}}{3} + \ddot{z}_1 l \sin \theta + \dot{z}_1 l \cos \theta \dot{\theta} \quad (3)$$

$$\frac{\partial L}{\partial \theta} = \frac{Ml^2 \dot{\theta}^2 \sin \theta \cos \theta}{3} + \frac{\dot{\theta} \dot{z}_1 Ml \cos \theta}{2} - \frac{Mg l}{2} \sin \theta \quad (4)$$

Combining (3) & (4) with (I) gives:

$$\left. \begin{aligned} & \frac{Ml^2 \ddot{\theta}}{3} + \ddot{z}_1 l \sin \theta + \dot{z}_1 \dot{\theta} l \cos \theta \\ & - \frac{Ml^2 \dot{\theta}^2 \sin \theta \cos \theta}{3} - \frac{\dot{\theta} \dot{z}_1 Ml \cos \theta}{2} + \frac{Mg l}{2} \sin \theta \end{aligned} \right\} = 0 \quad (B)$$

Finally:
$$\frac{\partial L}{\partial \dot{\phi}} = \frac{Ml^2 \dot{\phi}}{3} \sin^2 \theta$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\phi}} \right) = \frac{Ml^2}{3} (\dot{\phi}^2 \sin^2 \theta + 2\dot{\phi} \sin \theta \cos \theta \dot{\theta}) \quad (5)$$

(4)

$$\frac{\partial L}{\partial \phi} = -k_t \phi \quad (6)$$

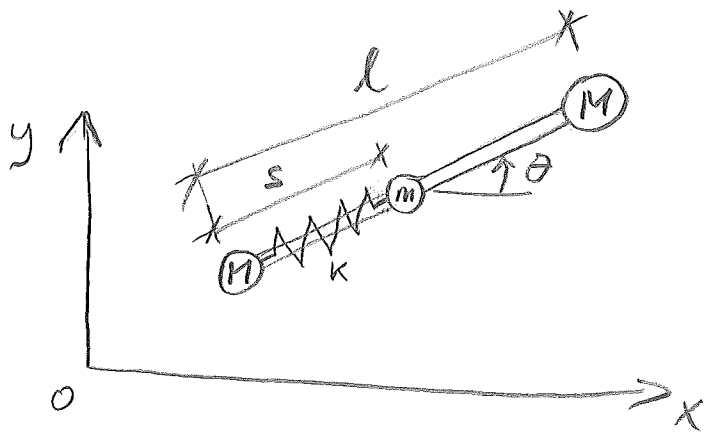
Combining (5) & (6) with (I) gives:

$$\left. \frac{Ml^2}{3} (\ddot{\phi} \sin^2 \theta + 2\dot{\phi} \sin \theta \cos \theta \dot{\theta}) + k_t \phi = 0 \right\} \quad (c)$$

So, the equations of motion of the system are given by (A), (B) & (C).

①

2.22

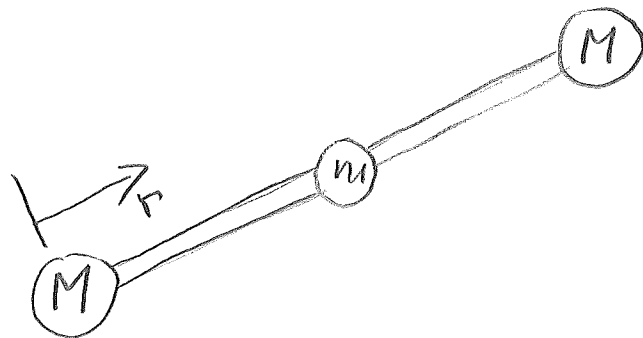


Two masses M with a mass m in between, which is connected to a spring k .

The x - y system represents an inertial frame of reference.

Compute the potential energy V and the kinetic energy T .

The energies are described using the coordinates x and y of the mass centre, together with the generalised coordinates s and θ .



With respect to a coordinate system in the axial direction r of the bar, with its origin at the left mass M , the centre of mass r_c can be computed as:

$$r_c = \frac{m \cdot s + M \cdot l + M \cdot 0}{2M + m} = \frac{m \cdot s + M \cdot l}{2M + m}$$

①

(2)

Subsequently, the relative distance of each mass w.r.t. the centre of mass C is given by (thus assuming a non-inertial frame of reference with its origin at C):

$$\begin{aligned}
 \underline{m}: \quad \Gamma_{rel, m} &= s - \frac{(ms + Ml)}{2M + m} \\
 &= \frac{s(2M + m)}{2M + m} - \frac{ms + Ml}{2M + m} \\
 &= \frac{M(2s - l)}{2M + m} \quad (2)
 \end{aligned}$$

$$\begin{aligned}
 \underline{M_{left}}: \quad \Gamma_{rel, M_{left}} &= 0 - \frac{(ms + Ml)}{2M + m} \\
 &= -\frac{(ms + Ml)}{2M + m} \quad (3)
 \end{aligned}$$

$$\begin{aligned}
 \underline{M_{right}}: \quad \Gamma_{rel, M_{right}} &= l - \frac{(ms + Ml)}{2M + m} \\
 &= \frac{l(2M + m)}{2M + m} - \frac{(ms + Ml)}{2M + m} \\
 &= \frac{Ml + m(l - s)}{2M + m} \quad (4)
 \end{aligned}$$

3

From (2) - (4), the corresponding relative velocities are calculated as

$$\underline{M}: \dot{T}_{rel, m} = \frac{2M \dot{s}}{2M + m} \quad (5)$$

$$\underline{M_{left}}: \dot{T}_{rel, M_{left}} = \frac{-m \dot{s}}{2M + m} \quad (6)$$

$$\underline{M_{right}}: \dot{T}_{rel, M_{right}} = \frac{-m \dot{s}}{2M + m} \quad (7)$$

The total kinetic energy T is composed of translational and rotational parts as

$$T = T_{trans} + T_{rot} \quad (7A)$$

The translational part consists of the kinetic energy associated to the centre of mass, $T_{trans}^{(1)}$, and the kinetic energy of the individual masses about the centre of mass, $T_{trans}^{(2)}$, see Török, pg. 36.

Since the position of the centre of mass is described by the coordinates x and y , the corresponding kinetic energy is:

$$T_{trans}^{(1)} = \frac{1}{2} (2M + m) \cdot (\dot{x}^2 + \dot{y}^2) \quad (8)$$

(4)

The kinetic energy of the individual masses w.r.t. the centre of mass can be computed using the corresponding relative velocities (5)-(7). i.e.,

$$T_{\text{trans}}^{(2)} = \frac{1}{2} m \cdot \frac{4M^2 \dot{s}^2}{(2M+m)^2} + \frac{1}{2} M \cdot \frac{m^2 \dot{s}^2}{(2M+m)^2} \times 2$$

$$\Rightarrow T_{\text{trans}}^{(2)} = \frac{2mM^2 \dot{s}^2 + Mm^2 \dot{s}^2}{(2M+m)^2} = \frac{mM \cdot \dot{s}^2}{2M+m} \quad (9)$$

From (8) and (9), the total translational kinetic energy becomes

$$T_{\text{trans}} = \frac{2M+m}{2} (\dot{x}^2 + \dot{y}^2) + \frac{mM \cdot \dot{s}^2}{2M+m} \quad (10)$$

The rotational kinetic energy follows from

$$T_{\text{rot}} = \frac{1}{2} I_c \cdot \dot{\theta}^2 \quad (11)$$

where I_c is the mass moment of inertia about the centre of mass.

(5)

Using the relative distances (2)-(4) of the individual masses w.r.t. the centre of mass C, the mass moment of inertia I_c can be computed as:

$$\begin{aligned}
 I_c = & m \cdot \left[\frac{M(2s-l)}{2M+m} \right]^2 \\
 & + M \cdot \left[\frac{-(ms+Ml)}{2M+m} \right]^2 \\
 & + M \cdot \left[\frac{Ml+m(l-s)}{2M+m} \right]^2 \quad (12)
 \end{aligned}$$

This expression can be further developed as

$$I_c = \frac{M}{(2M+m)^2} \left\{ \begin{aligned} & mM(2s-l)^2 \\ & + m^2s^2 + 2mMsL + M^2l^2 \\ & + M^2l^2 + 2Mml(l-s) + m^2(l-s)^2 \end{aligned} \right\}$$

Writing the first term between curly braces as (13)

$$\begin{aligned}
 mM(2s-l)^2 = & 2Mm(l-s)^2 - Mml^2 \\
 & + 2Mms^2 \quad (14)
 \end{aligned}$$

(6)

and inserting (14) into (13) gives

$$I_c = \frac{M}{(2M+m)^2} \left\{ (2M+m) (Ml^2 + m(l-s)^2 + ms^2) \right\}$$

$$= \frac{M}{2M+m} (Ml^2 + m(l-s)^2 + ms^2) \quad (15)$$

Substituting (15) into (11) gives

$$T_{rot} = \frac{M}{2(2M+m)} (Ml^2 + m(l-s)^2 + ms^2) \dot{\theta}^2 \quad (16)$$

Finally, inserting the rotational kinetic energy (16) and the translational kinetic energy (10) into (7^A), the total kinetic energy becomes

$$T = \frac{2M+m}{2} (\dot{x}^2 + \dot{y}^2) + \frac{mM}{2M+m} \dot{s}^2$$

$$+ \frac{M}{2(2M+m)} (Ml^2 + m(l-s)^2 + ms^2) \dot{\theta}^2 \quad (17)$$

The total potential energy is straightforwardly computed from the spring deformation, $\frac{l}{2} - s$, as

$$V = \frac{1}{2} k \left(\frac{l}{2} - s \right)^2 \quad (18)$$